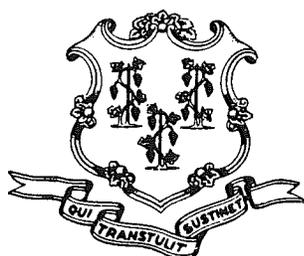


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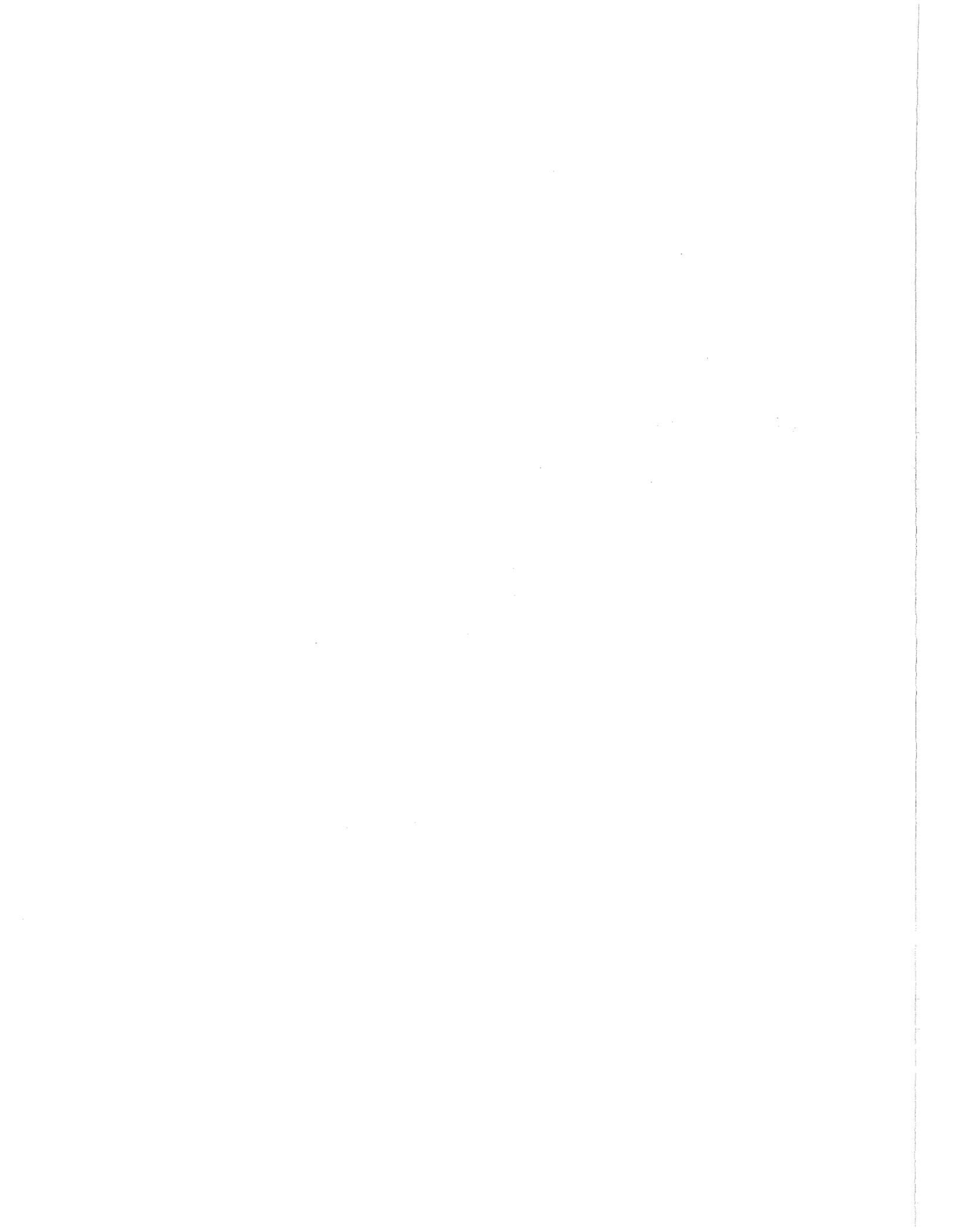
**STATE OF CONNECTICUT**

**ANNUAL AIR QUALITY SUMMARY**



**Lowell P. Weicker, Jr.**  
**Governor**

**Timothy R. E. Keeney**  
**Commissioner**



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## I. INTRODUCTION

The 1990 Air Quality Summary of ambient air quality in Connecticut is a compilation of all air pollutant measurements made at the Department of Environmental Protection (DEP) air monitoring network sites.

### A. OVERVIEW OF AIR POLLUTANT CONCENTRATIONS IN CONNECTICUT

The assessment of ambient air quality in Connecticut is made by comparing the measured concentrations of a pollutant to each of two Federal air quality standards. The first is the primary standard which is established to protect public health with an adequate margin of safety. The second is the secondary standard which is established to protect plants and animals and to prevent economic damage. The specific air quality standards are listed in Table 1-1 along with the time and data constraints imposed on each.

The following section briefly describes the status of Connecticut's air quality for the year 1990. More detailed discussions of each of the six pollutants are provided in subsequent sections of this Air Quality Summary.

#### 1. PARTICULATE MATTER (PM<sub>10</sub>)

**Revision of the Particulate Matter Standard** - In 1971, the federal Environmental Protection Agency (EPA) promulgated primary and secondary national ambient air quality standards for particulate matter, measured as total suspended particulates or "TSP." The primary standards were set at 260  $\mu\text{g}/\text{m}^3$ , 24-hour average not to be exceeded more than once per year, and 75  $\mu\text{g}/\text{m}^3$ , annual geometric mean. The secondary standard was set at 150  $\mu\text{g}/\text{m}^3$ , 24-hour average not to be exceeded more than once per year. These standards were adopted by the state of Connecticut in 1972.

In accordance with sections 108 and 109 of the Clean Air Act, EPA has reviewed and revised the health and welfare criteria upon which these primary and secondary particulate matter standards were based. EPA found that a size-specific indicator for primary standards representing small particles was warranted and that it should include particles of diameter less than or equal to a nominal 10 micrometers "cut point." Such a standard would place substantially greater emphasis on controlling small particles than does a TSP indicator, but would not completely exclude larger particles from all control.

On March 20, 1984, EPA proposed changes in the standards for particulate matter based on its review and revision of the health and welfare criteria. On July 1, 1987, EPA announced its final decisions regarding these changes. They include: (1) replacing TSP as the indicator for particulate matter for the ambient standards with a new indicator that includes only those particles with an aerodynamic diameter less than or equal to a nominal 10 micrometers (PM<sub>10</sub>); (2) replacing the 24-hour primary TSP standard with a 24-hour PM<sub>10</sub> standard of 150  $\mu\text{g}/\text{m}^3$  with no more than one expected exceedance per year; (3) replacing the annual primary TSP standard with a PM<sub>10</sub> standard of 50  $\mu\text{g}/\text{m}^3$ , expected annual arithmetic mean; and (4) replacing the secondary TSP standard with 24-hour and annual PM<sub>10</sub> standards that are identical in all respects to the primary standards. The state of Connecticut is in the process of adopting these standards.

**Compliance Assessment** - Measured PM<sub>10</sub> concentrations during 1990 did not exceed the 50 µg/m<sup>3</sup> level of the primary and secondary annual standards or the 150 µg/m<sup>3</sup> level of the primary and secondary 24-hour standards at any site. Furthermore, the 24-hour standards were not violated because the "expected number of exceedances" for the most recent 3 years at each site did not exceed one per year. The annual standards were also not violated because the "expected annual mean" for the most recent 3 years at each site did not exceed 50 µg/m<sup>3</sup>.

2. **SULFUR DIOXIDE (SO<sub>2</sub>)**

**Compliance Assessment** - None of the air quality standards for sulfur dioxide were exceeded in Connecticut in 1990. Measured concentrations were below the 80 µg/m<sup>3</sup> primary annual standard, the 365 µg/m<sup>3</sup> primary 24-hour standard, and the 1300 µg/m<sup>3</sup> secondary 3-hour standard at all monitoring sites.

3. **OZONE (O<sub>3</sub>)**

**National Ambient Air Quality Standard (NAAQS)** - On February 8, 1979, the U.S. Environmental Protection Agency (EPA) established an ambient air quality standard for ozone of 0.12 ppm for a one-hour average. That level is not to be exceeded more than once per year. Furthermore, in order to determine compliance with the 0.12 ppm ozone standard, EPA directs the states to record the number of daily exceedances of 0.12 ppm at a given monitoring site over a consecutive 3-year period and then calculate the average number of daily exceedances for this interval. If the resulting average value is less than or equal to 1.0, (that is, if the fourth highest daily value in a consecutive 3-year period is less than or equal to 0.12 ppm), the ozone standard is considered to be attained. The definition of the pollutant was also changed, along with the numerical value of the standard, partly because the instruments used to measure photochemical oxidants in the air really measure only ozone. Ozone is one of a group of chemicals which are formed photochemically in the air and are called photochemical oxidants. In the past, the two terms have often been used interchangeably. This Air Quality Summary uses the term "ozone" in conjunction with the new NAAQS to reflect the changes in both the numerical value of the NAAQS and the definition of the pollutant.

**Compliance Assessment** - The primary 1-hour ozone standard was frequently exceeded at nine of the ten DEP ozone monitoring sites in 1990 (see Table 1-2). Consequently, the standard was violated at those sites.

4. **NITROGEN DIOXIDE (NO<sub>2</sub>)**

**Compliance Assessment** - The annual average NO<sub>2</sub> standard of 100 µg/m<sup>3</sup> was not exceeded at any site in Connecticut in 1990.

5. **CARBON MONOXIDE (CO)**

**Compliance Assessment** - The primary eight-hour standard of 9 ppm was not exceeded at any of the five carbon monoxide monitoring sites in Connecticut during 1990. Since two exceedances at a particular site are required for the standard to be violated, this means that the eight-hour standard was not violated at any of the sites.

There were no exceedances and, therefore, no violations of the primary one-hour standard of 35 ppm at any carbon monoxide monitoring site in Connecticut in 1990.

#### 6. LEAD (Pb)

**Compliance Assessment** - The primary and secondary ambient air quality standard for lead is  $1.5 \mu\text{g}/\text{m}^3$ , maximum arithmetic mean averaged over three consecutive calendar months. As has been the case since 1980, the lead standard was not exceeded at any site in Connecticut during 1990.

### B. AIR MONITORING NETWORK

A computerized Air Monitoring Network consisting of an IBM System 7 computer and numerous telemetered monitoring sites has operated in Connecticut for several years. In 1985, this data acquisition system was modernized by installing new data loggers at the monitoring sites and replacing the dedicated IBM System 7 computer with a non-dedicated Data General Eclipse MV10000 computer, which was replaced in 1988 with a MV15000 model. This essentially improved both data accuracy and data capture. As many as 13 measurement parameters are transmitted from a site via telephone lines to the Data General unit located in the DEP Hartford office. The data are then compiled three times daily into 24-hour summaries. The telemetered sites are located in the towns of Bridgeport, Danbury, East Hartford, East Haven, Enfield, Greenwich, Groton, Hartford, Madison, Middletown, Milford, New Britain, New Haven, Stafford, Stamford, Stratford and Waterbury.

Continuously measured parameters include the pollutants sulfur dioxide, particulates (measured as  $\text{PM}_{10}$ ), carbon monoxide, nitrous oxide, total nitrogen oxides and ozone. Meteorological data consists of wind speed and direction, wind horizontal sigma, temperature, precipitation, barometric pressure and dew point.

The real-time capabilities of the telemetry network have enabled the Air Monitoring Unit to report the Pollutant Standards Index for a number of towns on a daily basis while continuously keeping a close watch for high pollution levels which may occur during adverse weather conditions.

The complete monitoring network used in 1990 consisted of the following:

- 43 Particulate matter ( $\text{PM}_{10}$ ) hi-vol samplers
- 4 Particulate matter ( $\text{PM}_{10}$ ) analyzers
- 5 Lead lo-vol samplers
- 16 Sulfur dioxide analyzers
- 10 Ozone analyzers
- 3 Nitrogen dioxide analyzers
- 5 Carbon monoxide analyzers

A complete description of all permanent air monitoring sites in Connecticut operated by DEP in 1990 is available from the Department of Environmental Protection, Bureau of Air Management, Monitoring and Radiation Division, State Office Building, Hartford, Connecticut, 06106.

### C. POLLUTANT STANDARDS INDEX

The Pollutant Standards Index (PSI) is a daily air quality index recommended for common use in state and local agencies by the U.S. Environmental Protection Agency. Starting on November 15, 1976, Connecticut began reporting the PSI on a 7-day basis, but is currently reporting the PSI on a 5-day basis

(i.e., with predictions for the weekends). The PSI incorporates three pollutants : sulfur dioxide, PM<sub>10</sub> and ozone. The index converts each air pollutant concentration into a normalized number where the National Ambient Air Quality Standard for each pollutant corresponds to PSI = 100 and the Significant Harm Level corresponds to PSI = 500.

Figure 1-1 shows the breakdown of index values for the commonly reported pollutants (PM<sub>10</sub>, SO<sub>2</sub>, and O<sub>3</sub>) in Connecticut. For the winter of 1990, Connecticut reported the PM<sub>10</sub> PSI for the towns of Ansonia, Bridgeport, Danbury, East Hartford, Greenwich, Groton, Hartford, Meriden, Milford, Naugatuck, New Britain, New Haven, Norwalk, Norwich, Putnam, Stamford, Torrington, Wallingford, Waterbury and Willimantic; and reported the sulfur dioxide PSI for the towns of Bridgeport, Danbury, East Hartford, East Haven, Enfield, Greenwich, Groton, Hartford, Milford, New Britain, New Haven, Stamford, and Waterbury. For the summer, the ozone PSI was reported for the towns of Bridgeport, Danbury, East Hartford, Greenwich, Groton, Madison, Middletown, New Haven, Stafford, and Stratford. Each day, the pollutant with the highest PSI value of all the pollutants being monitored is reported for each town, along with the dimensionless PSI number and a descriptor label to characterize the daily air quality. A descriptor label of each subsequent day's forecast is also included.

A telephone recording of the PSI is taped each afternoon at approximately 3 PM, five days a week, and can be heard by dialing 566-3449. Predictions for weekends are included on the Friday recordings. For answers to specific questions, you can call a DEP representative at 566-3310. The PSI information, as well as health effects information, is also available to the public during weekdays from the American Lung Association of Connecticut in East Hartford. The number there is 289-5401 or 1-800-992-2263.

#### **D. QUALITY ASSURANCE**

Quality Assurance requirements for State and Local Air Monitoring Stations (SLAMS) and the National Air Monitoring Stations (NAMS), as part of the (SLAMS) network, are specified by the code of Federal Regulations, Title 40, Part 58, Appendix A.

The regulations were enacted to provide a consistent approach to Quality Assurance activities across the country so that ambient data with a defined precision and accuracy is produced.

A Quality Assurance program was initiated in Connecticut with written procedures covering, but not limited to, the following:

- Equipment procurement
- Equipment installation
- Equipment calibration
- Equipment operation
- Sample analysis
- Maintenance checks
- Performance audits
- Data handling
- Data quality assessment

Quality assurance procedures for the above activities were fully operational on January 1, 1981 for all NAMS monitoring sites. On January 1, 1983 the above procedures were fully operational for all SLAMS monitoring sites.

Data precision and accuracy values are reported in the form of 95% probability limits as defined by equations found in Appendix A of the Federal regulations cited above.

## 1. PRECISION

Precision is a measure of data repeatability (grouping) and is determined as follows:

### a. Manual Samplers (PM<sub>10</sub>)

A second (co-located) PM<sub>10</sub> hi-vol sampler is placed alongside a regular PM<sub>10</sub> network sampler and operated concurrently. The concentration values from the co-located hi-vol sampler are compared to the network sampler and precision values are generated from the comparison.

### b. Manual Samplers (Lead)

A second (co-located) hi-vol sampler is placed alongside a regular network hi-vol sampler and operated concurrently. The concentration values from the co-located hi-vol sampler are compared to those from the network sampler, and precision values are generated from the comparison.

### c. Automated Analyzers (SO<sub>2</sub>, O<sub>3</sub>, CO and NO<sub>2</sub>)

All NAMS and SLAMS analyzers are challenged with a low level pollutant concentration a minimum of once every two weeks: 0.08 to 0.10 ppm for SO<sub>2</sub>, O<sub>3</sub> and NO<sub>2</sub>, and 8 to 10 ppm for CO. The comparison of analyzer response to input concentration is used to generate automated analyzer precision values.

## 2. ACCURACY

Accuracy is an estimate of the closeness of a measured value to a known value and is determined in the following manner:

### a. Manual Methods (PM<sub>10</sub>)

Accuracy for PM<sub>10</sub> is assessed by auditing the flow measurement phase of the sampling method. In Connecticut, this is accomplished by attaching a secondary standard calibrated orifice to the hi-vol inlet and comparing the flow rates. A minimum of 25% of the PM<sub>10</sub> network samplers is audited each quarter.

### b. Manual Methods (Lead)

Accuracy for lead is assessed by analyzing spiked samples and comparing the known spiked-sample concentrations with the measured concentrations. Accuracy measurements are obtained each quarter.

### c. Automated Analyzers (SO<sub>2</sub>, O<sub>3</sub>, CO and NO<sub>2</sub>)

Automated analyzer data accuracy is determined by challenging each analyzer with three predetermined concentration levels (four for NO<sub>2</sub>). Each quarter, accuracy values are calculated for approximately 25% of the analyzers in a pollutant sampling network, at each concentration level. The results for each concentration

of a particular pollutant are used to assess automated analyzer accuracy. The audit concentration levels are as follows:

| <b>SO<sub>2</sub>, O<sub>3</sub>, and NO<sub>2</sub> (PPM)</b> | <b>CO (PPM)</b> |
|--|-----------------|
| 0.03 to 0.08   | 3 to 8          |
| 0.15 to 0.20   | 15 to 20        |
| 0.35 to 0.45   | 35 to 45        |
| 0.80 to 0.90 (NO <sub>2</sub> only)                            |                 |

**TABLE 1-1**  
**ASSESSMENT OF AMBIENT AIR QUALITY**

| POLLUTANT                                     | SAMPLING PERIOD               | DATA REDUCTION    | STATISTICAL BASE                      | AMBIENT AIR QUALITY STANDARDS |                   |                   |                   |
|---|-------------------------------|-------------------|---------------------------------------|-------------------------------|-------------------|-------------------|-------------------|
|   |                               |                   |                                       | PRIMARY                       |                   | SECONDARY         |                   |
|   |                               |                   |                                       | µg/m <sup>3</sup>             | ppm               | µg/m <sup>3</sup> | ppm               |
| Particulates (PM <sub>10</sub> ) <sup>a</sup> | 24 Hours<br>(every sixth day) | 24-Hour Average   | Annual Arithmetic Mean <sup>b</sup>   |                               |                   | 50 <sup>c</sup>   |                   |
|   |                               |                   | 24-Hour Average                       |                               |                   | 150 <sup>d</sup>  |                   |
| Sulfur Oxides<br>(measured as sulfur dioxide) | Continuous                    | 1-Hour Average    | Annual Arithmetic Mean <sup>e</sup>   | 80                            | 0.03              |                   |                   |
|   |                               |                   | 24-Hour Average <sup>e</sup>          | 365 <sup>f</sup>              | 0.14 <sup>f</sup> |                   |                   |
|   |                               |                   | 3-Hour Average <sup>e</sup>           |                               |                   | 1300 <sup>f</sup> |                   |
| Nitrogen Dioxide                              | Continuous                    | 1-Hour Average    | Annual Arithmetic Mean <sup>e</sup>   | 100                           | 0.05              | 100               | 0.05              |
|   |                               |                   | 1-Hour Average                        | 235 <sup>g</sup>              | 0.12 <sup>g</sup> | 235 <sup>g</sup>  | 0.12 <sup>g</sup> |
| Lead  | 24 Hours<br>(every sixth day) | Monthly Composite | Weighted 3-Month Average <sup>h</sup> | 1.5                           |                   | 1.5               |                   |
|   |                               |                   | 8-Hour Average                        | 10 <sup>f,i</sup>             | 9 <sup>f</sup>    | 10 <sup>f,i</sup> | 9 <sup>f</sup>    |
| Carbon Monoxide                               | Continuous                    | 1-Hour Average    | 1-Hour Average                        | 40 <sup>f</sup>               | 35 <sup>f</sup>   | 40 <sup>f</sup>   | 35 <sup>f</sup>   |

<sup>a</sup> Particulate matter with an aerodynamic diameter not greater than a nominal 10 micrometers.  
<sup>b</sup> EPA assessment criteria require 4 calendar quarters of data per year and at least 75% of the scheduled samples per calendar quarter in each of the most recent 3 years.  
<sup>c</sup> The "expected annual mean" for the most recent 3 years.  
<sup>d</sup> The "expected number of exceedances" per calendar year should be less than or equal to one, for the most recent 3 years.  
<sup>e</sup> EPA assessment criteria require at least 75% of the possible data to compute a valid average.  
<sup>f</sup> Not to be exceeded more than once per year.  
<sup>g</sup> Not to be exceeded more than an average of once per year in three years.  
<sup>h</sup> State of Connecticut assessment criteria require at least 75% of the scheduled samples to compute a valid average.  
<sup>i</sup> Units are mg/m<sup>3</sup>, not µg/m<sup>3</sup>.

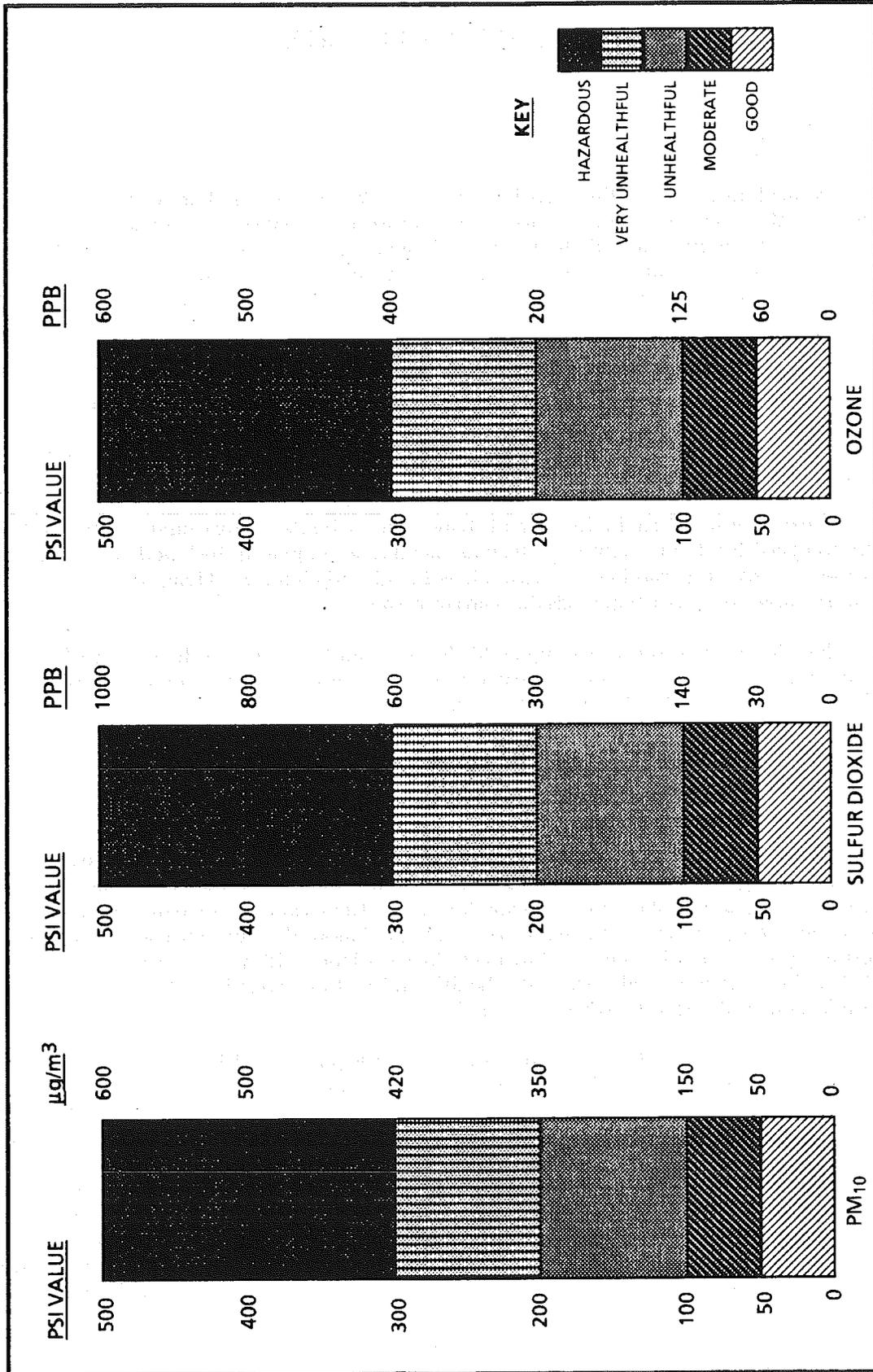
**TABLE 1-2**

**AIR QUALITY STANDARDS EXCEEDED IN CONNECTICUT IN 1990**  
**BASED ON MEASURED CONCENTRATIONS**

|  | <u>TOWN</u>   | <u>SITE</u> | <u>OZONE</u>                                   |   |
|--|---------------|-------------|--|---|
|  |               |             | <u>Level Exceeding<br/>1-Hour<br/>Standard</u> | <u>Highest<br/>Observed<br/>Level<br/>(ppm)</u> |
|  | Bridgeport    | 013         | 0.182  | 3   |
|  | Danbury       | 123         | 0.167  | 4   |
|  | East Hartford | 003         | 0.151  | 4   |
|  | Greenwich     | 017         | 0.146  | 7   |
|  | Groton        | 008         | 0.172  | 6   |
|  | Madison       | 002         | 0.197  | 7   |
|  | Middletown    | 007         | 0.158  | 3   |
|  | Stafford      | 001         | 0.153  | 5   |
|  | Stratford     | 007         | 0.126  | 4   |

# FIGURE 1-1

## POLLUTANT STANDARDS INDEX



## II. PARTICULATE MATTER

### HEALTH EFFECTS

Particulate matter is the generic term for a broad class of chemically and physically diverse substances that exist as discrete particles (liquid droplets or solids) over a wide range of sizes. Particles originate from a variety of stationary and mobile sources. They may be emitted directly or formed in the atmosphere by transformations of gaseous emissions such as sulfur oxides, nitrogen oxides, and volatile organic substances. The chemical and physical properties of particulate matter vary greatly with time, region, meteorology and source category.

The major effects associated with high exposures to particulate matter include reduced lung function; interference with respiratory mechanics; aggravation or potentiation of existing respiratory and cardiovascular disease, such as chronic bronchitis and emphysema; increased susceptibility to infection; interference with clearance and other host defense mechanisms; damage to lung tissues; carcinogenesis and mortality.

Harm may also occur in the form of changes in the human body caused by chemical reactions with pollution particles that pass through the lung membranes to poison the blood or be carried by the blood to other organs. This can happen with inhaled lead, cadmium, beryllium, and other metals, and with certain complex organic compounds that can cause cancer.

Population subgroups that appear likely to be most sensitive to the effects of particulate matter include individuals with chronic obstructive pulmonary or cardiovascular disease, individuals with influenza, asthmatics, the elderly, children, smokers, and mouth or oronasal breathers.

### REVISION OF THE PARTICULATE MATTER STANDARD

In 1971, the federal Environmental Protection Agency (EPA) promulgated primary and secondary national ambient air quality standards for particulate matter, measured as total suspended particulates or "TSP." The primary standards were set at 260  $\mu\text{g}/\text{m}^3$ , 24-hour average not to be exceeded more than once per year, and 75  $\mu\text{g}/\text{m}^3$ , annual geometric mean. The secondary standard, also measured as TSP, was set at 150  $\mu\text{g}/\text{m}^3$ , 24-hour average not to be exceeded more than once per year. These standards were adopted by the state of Connecticut in 1972. In accordance with sections 108 and 109 of the Clean Air Act, EPA has reviewed and revised the health and welfare criteria upon which these primary and secondary particulate matter standards were based.

The TSP standard directs control efforts towards particles of lower risk to health because of its inclusion of large particles which can dominate the measured mass concentration, but which are deposited only in the extrathoracic region. Smaller particles penetrate furthest in the respiratory tract, settling in the tracheobronchial region and in the deepest portion of the lung, the alveolar region. Available evidence demonstrates that the risk of adverse health effects associated with deposition of typical ambient fine and coarse particles in the thorax are markedly greater than those associated with deposition in the extrathoracic region. EPA found that a size-specific indicator for primary standards representing small particles was warranted and that it should include particles of diameter less than or equal to a nominal 10 micrometers "cut point." Such a standard would place substantially greater emphasis on controlling smaller particles than does a TSP indicator, but would not completely exclude larger particles from all control.

On March 20, 1984, EPA proposed changes in the standards for particulate matter based on its review and revision of the health and welfare criteria. On July 1, 1987, EPA announced its final decisions regarding these changes. They include: (1) replacing TSP as the indicator for particulate matter for the ambient standards with a new indicator that includes only those particles with an aerodynamic diameter less than or equal to a nominal 10 micrometers (PM<sub>10</sub>); (2) replacing the 24-hour primary TSP standard with a 24-hour PM<sub>10</sub> standard of 150 µg/m<sup>3</sup> with no more than one expected exceedance per year; (3) replacing the annual primary TSP standard with a PM<sub>10</sub> standard of 50 µg/m<sup>3</sup>, expected annual arithmetic mean; and (4) replacing the secondary TSP standard with 24-hour and annual PM<sub>10</sub> standards that are identical in all respects to the primary standards. The state of Connecticut is in the process of adopting these standards.

## **CONCLUSIONS**

Measured PM<sub>10</sub> concentrations during 1990 did not exceed the 50 µg/m<sup>3</sup> level of the primary and secondary annual standards or the 150 µg/m<sup>3</sup> level of the primary and secondary 24-hour standards at any site. Furthermore, the 24-hour standards were not violated because the "expected number of exceedances" for the most recent 3 years at each site did not exceed one per year. The annual standards were also not violated anywhere because the "expected annual mean" for the most recent 3 years at each site did not exceed 50 µg/m<sup>3</sup>.

## **SAMPLE COLLECTION AND ANALYSIS**

**PM<sub>10</sub> Sampler** - Before 1988, Connecticut's particulate sampling network was comprised of standard high-volume (hi-vol) samplers, whose function was to measure TSP. These hi-vols resemble vacuum cleaners in their operation, with an 8" X 10" piece of fiberglass filter paper replacing the vacuum bag. With the promulgation of a PM<sub>10</sub> standard, hi-vol samplers were needed that could screen out most particles larger than 10 microns. The samplers also had to be omnidirectional and have a constant inlet velocity so that wind direction and speed would not affect the amount of material collected.

In anticipation of a PM<sub>10</sub> standard being promulgated, Connecticut installed a small number of PM<sub>10</sub> samplers in 1985. The samplers, manufactured by Sierra-Andersen, were the first PM<sub>10</sub> samplers on the market. These early samplers were found to have relatively high maintenance requirements and to be biased towards particles larger than 10 microns. To remedy these problems, the samplers were physically modified after 1986. In 1987, PM<sub>10</sub> samplers by Wedding & Associates came on the market. These samplers replaced the Andersen samplers in the sampling network in 1988. The Wedding samplers have demonstrated lower maintenance requirements and greater precision (repeatability) and accuracy than the Andersen samplers they replaced.

The PM<sub>10</sub> samplers, like the standard hi-vol samplers, operate from midnight to midnight (standard time) at least every sixth day at all sites. However, PM<sub>10</sub> samplers use quartz fiber filters instead of fiberglass filters, in order to eliminate sulfate artifact formation. The matter collected on the filter is analyzed for weight. The air flow is recorded during sampling. The weight in micrograms (µg) divided by the volume of air in standard cubic meters (m<sup>3</sup>) yields the PM<sub>10</sub> concentration for the day in micrograms per cubic meter.

**Low Volume Sampler (Lo-vol)** - The low volume sampler is a 30-day continuous sampler. It is enclosed in a shelter similar to a hi-vol, uses the same fiberglass filter paper, but operates at an air sampling flow rate approximately one-tenth that used by a standard hi-vol (i.e., 4 cfm as opposed to 40-60 cfm). The air flow through the lo-vol is measured by a temperature compensating dry gas meter. The lo-vol measurement is essentially an average for the 30-day sampling interval.

The matter collected on the filters is analyzed for both weight and chemical composition. The chemical composition of the suspended particulate matter is determined at each lo-vol site as follows. Two standardized strips of every filter are cut out and prepared for two different analyses. In the first analysis, a sample is digested in acid and the resulting solution is analyzed for metals by means of an atomic absorption spectrophotometer. The results are reported for each individual metal in  $\mu\text{g}/\text{m}^3$ . In the second analysis, a sample is dissolved in water, filtered and the resulting solution is analyzed by means of wet chemistry techniques to determine the concentration of certain water soluble components. The results are reported for each individual constituent of the water soluble fraction in  $\mu\text{g}/\text{m}^3$ .

## DISCUSSION OF DATA

**Monitoring Network** - In 1990, 43  $\text{PM}_{10}$  samplers were operated in Connecticut (see Figure 2-1). It should be noted that this total includes one sampler for site New Haven 018 when, in fact, there are five samplers at the site, which are operated sequentially in order to facilitate a daily sampling schedule.

As part of the 1990 network for monitoring the airborne concentrations of lead, five lo-vol samplers were used to gather information on the chemical composition of TSP in the state. These samplers were Bridgeport 010, East Hartford 004, Hartford 016, New Haven 018 and Waterbury 123.

**Precision and Accuracy** - Precision checks were conducted at two  $\text{PM}_{10}$  sampling sites which had co-located samplers. On the basis of 110 precision checks, the 95% probability limits for precision ranged from -13% to +8%. Accuracy is based on air flow through the monitor. The 95% probability limits for accuracy, based on 43 audits conducted on the  $\text{PM}_{10}$  monitoring system network, ranged from -2% to +6%. (See section I.D. of this Air Quality Summary for a discussion of precision and accuracy.)

**Annual Averages** - The Federal EPA has established minimum sampling criteria (see Table 1-1) for use in determining compliance with the primary and secondary annual NAAQS for  $\text{PM}_{10}$ . A site must have 75% of the scheduled samples in each calendar quarter for the the most recent 3 years. Using the EPA criteria, one finds that a determination of attainment or nonattainment of the 50  $\mu\text{g}/\text{m}^3$  primary and secondary annual standards could be reached at only 3 of the 43  $\text{PM}_{10}$  monitoring sites in Connecticut in 1990. Attainment of the annual standards was demonstrated at the Hartford 015, New Haven 018 and Waterbury 123 sites. Whereas the "expected annual mean"  $\text{PM}_{10}$  concentration at New Haven 018 equaled the 50  $\mu\text{g}/\text{m}^3$  level of the standard in 1989 and exceeded the level of the standard by 5  $\mu\text{g}/\text{m}^3$  in 1988, it was well below the level of the standard at 44  $\mu\text{g}/\text{m}^3$  in 1990.

Of the 43 sampling sites in the network, the above 3 sites were the only ones that could satisfy the minimum sampling criteria for the most recent 3 years. The reason for this is that a major part of the network was installed after the first calendar quarter of 1988.

A summary of annual average  $\text{PM}_{10}$  data for 1988 -1990 is presented in Table 2-1. This table also includes an indication of whether the aforementioned EPA minimum sampling criteria were met at each site for each year. If the sampling was insufficient to meet the EPA criteria, an asterisk appears next to the number of samples.

**Statistical Projections** - The statistical projections presented in Table 2-1 are prepared by a DEP computer program which analyzes data from all sites operated by DEP. Input to the program includes the site location, the year, the number of samples (usually a maximum of 61), the annual arithmetic and geometric mean concentrations, and the arithmetic and geometric standard deviations. For each site, the program lists the input, calculates the 95% confidence limits about the annual arithmetic mean, and predicts the number of days in each year that the level of the primary and secondary 24-hour standards (150  $\mu\text{g}/\text{m}^3$ ) would have been exceeded if sampling had been conducted every day. For comparison, Table 2-1 also shows the number of days at each site when the level of the primary and secondary 24-hour standards was actually exceeded, as demonstrated by actual measurements at the site.

The statistical predictions of the number of days that would have seen an exceedance of the level of the 24-hour standards are based on the assumption of a lognormal distribution of the data. They indicate that more frequent PM<sub>10</sub> sampling in 1988 and 1989 at New Haven 018 might have resulted in measured violations (i.e., four or more exceedances in three years) of the 24-hour standards.

Because manpower and economic limitations dictate that PM<sub>10</sub> sampling for particulate matter cannot be conducted every day, a degree of uncertainty is introduced as to whether the air quality at a site has either met or exceeded the level of the annual standards. This uncertainty can be expressed by means of a statistic called a confidence limit. Assuming a normal distribution of the pollutant data, 95% confidence limits were calculated about the annual arithmetic mean at each site. For example (see Table 2-1), at Bridgeport 014 in 1989, 59 samples were analyzed and an arithmetic mean of 36.5 µg/m<sup>3</sup> was then calculated. The columns labeled "95-PCT-LIMITS" show the lower and upper limits of the 95% confidence interval to be 33.0 and 40.0 µg/m<sup>3</sup>, respectively. This means that there is a 95% chance that the true arithmetic mean would fall between these limits. Since the upper 95% limit is less than 50 µg/m<sup>3</sup>, one can be confident that the level of the annual standards was not exceeded at the site. However, if the upper 95% limit were greater, and the lower limit less, than 50 µg/m<sup>3</sup>, then one could not be confident that the standard was not exceeded at the site. And if both the upper and lower 95% limits were greater than 50 µg/m<sup>3</sup>, then one could assume that the level of the standards was indeed exceeded sometime during the year. These three possibilities are illustrated in Figure 2-2.

Table 2-2 summarizes the statistical predictions from Table 2-1 regarding compliance with the level of the annual air quality standards, using the 95% confidence limit criteria. The table shows that the level of the primary and secondary annual standards was probably achieved at the 39 sites that met the minimum sampling criteria in 1990. The results for the years 1988 and 1989 are also tabulated.

It should be noted that the above discussion of statistics does not affect the actual determination of attainment or nonattainment of the PM<sub>10</sub> standards. The promulgated regulations specify the requirements for making an attainment determination. Those requirements, mentioned in a limited way in Table 1-1, address the projection of exceedances and the calculation and use of arithmetic means in ways that are different from the foregoing discussion.

**24-Hour Averages** - Figure 2-3 presents the maximum 24-hour concentrations recorded at each site. There were no PM<sub>10</sub> concentrations at any site that exceeded the 150 µg/m<sup>3</sup> level of the primary and secondary 24-hour standards in 1990.

Table 2-3 summarizes the statistical predictions from Table 2-1 regarding the number of sites that would have seen PM<sub>10</sub> concentrations exceeding the level of the 24-hour standards, if sampling had been conducted every day. In 1990, there would have been no such site. The results for 1988 and 1989 are also given. In all cases, results are presented only for those sites that met the minimum sampling criteria for the year.

A determination of actual compliance with the primary and secondary 24-hour standards can be made for a site only when the minimum sampling criteria are met in each calendar quarter for the most recent 3 years. Based on these criteria, compliance was achieved at Hartford 015, New Haven 018 and Waterbury 123 in 1990. This was the first year that the 24-hour standards were not violated at New Haven 018, where the "expected number of exceedances" of the 150 µg/m<sup>3</sup> level of the 24-hour standards was determined to be less than one per year.

**Lo-vol Averages** - Monthly and annual averages of the chemical components from the lo-vol TSP monitors have been computed for 1990 and are presented in Table 2-4.

**10 High Days with Wind Data** - Table 2-5 lists the 10 highest 24-hour average PM<sub>10</sub> readings with the dates of occurrence for each PM<sub>10</sub> hi-vol site in Connecticut which complied with EPA's minimum

sampling criteria during 1990. This table also shows the average wind conditions which occurred on each of these dates. The resultant wind direction (DIR, in compass degrees clockwise from true north) and velocity (VEL, in mph), the average wind speed (SPD, in mph), and the ratio between the velocity and the speed are presented for each of four National Weather Service stations located in or near Connecticut. The resultant wind direction and velocity are vector quantities and are computed from the individual wind direction and speed readings in each day. The closer the wind speed ratio is to 1.000, the more persistent the wind. It should be noted that the Connecticut stations have local influences which change the speed and shift the direction of the near-surface air flow (e.g., the Bradley Field air flow is channeled north-south by the Connecticut River Valley and the Bridgeport air flow is frequently subject to sea breezes).

On a statewide basis, this table shows that approximately 33% of the high PM<sub>10</sub> days occur with winds out of the southwest quadrant and most of those days have relatively persistent winds. This relationship between southwest winds and high particulate levels has historically been more prevalent in southwestern Connecticut. However, many of the maximum levels at some urban sites do not occur with southwest winds, indicating that these sites are possibly influenced by local sources or transport from different out-of-state sources. As noted above, a large scale southwesterly air flow is often diverted into a southerly flow up the Connecticut River Valley. At sites in the Connecticut River Valley, many of the highest PM<sub>10</sub> days occur when the winds at Bradley Airport are from the south.

**Trends** - Any attempt to assess statewide trends in air pollution levels must account for the tendency of local changes to obscure the statewide pattern. In order to reach some statistically valid conclusions concerning trends in pollutant levels in Connecticut, the DEP has applied a statistical test called a paired *t* test (referred to hereafter as the *t* test) to the annual average data for PM<sub>10</sub>.

The *t* test is a parametric test which can ascertain a statistically significant change in the statewide annual average pollutant concentration in Connecticut. The *t* test makes it possible to overcome the trend analysis problems which arise due to the changes in the number and location of monitoring sites from year-to-year, as well as problems associated with making equitable comparisons among sites. The annual mean pollutant concentrations for consecutive years are compared at each site, and the difference is noted. There is no inter-site comparison. The mean and the standard deviation of the differences are used to calculate a *t* statistic, which is employed to determine the statistical significance of the apparent statewide change in pollutant level. For example, if a high proportion of sites experience an increase and/or if the magnitude of the increases at several sites is of much greater importance than the magnitude of the decreases at other sites, the *t* test will show that the increase was statistically significant for those two years.

The results of the *t* test for PM<sub>10</sub> are presented in Table 2-6. The analyses were performed only on data computed for sites at which the EPA's minimum sampling criteria were met. The first three columns of Table 2-6 show the years of data that were paired, the number of sites, and the average of the geometric mean pollutant concentrations at the sites in each year. The remaining columns show the average and standard deviation of the differences of the paired year means at each site, as well as the statistical significance of any change in the statewide pollutant average. The significance of a change is indicated by an arrow for each confidence limit, and is also given numerically as the number of chances in 10,000 that the change in the statewide PM<sub>10</sub> level was not significant. For example, the statewide annual average for PM<sub>10</sub> decreased between 1986 and 1987 from 37.7 to 34.0. This change represented a significant decrease at the 95% confidence level, but it did not represent a significant change at the 99% confidence level. The "probability that change is not significant" is given as 0.0148, meaning that there are only 148 chances in 10,000 that the apparent decrease in PM<sub>10</sub> levels between 1986 and 1987 did not occur. The results of the *t* test show that the year-to-year PM<sub>10</sub> levels in Connecticut apparently remained unchanged from 1985 to 1989, except for a decrease at the 95% confidence level from 1986 to 1987. However, there was a significant decrease in statewide PM<sub>10</sub> levels from 1989 to 1990. The reader is advised that the results should be interpreted with caution when the number of paired sites is small, as is the case with the 1985-1989 data.

These trend analyses do not account for the uncertainty associated with the individual annual mean computed for each PM<sub>10</sub> site. Most particulate sampling is conducted only every sixth day, producing a maximum possible total of 61 samples per year. Therefore, the t test really compares averages of the sampled concentrations, not actual annual averages. However, the every-sixth-day sampling schedule is believed to be sufficient to produce representative annual averages. The every-sixth-day schedule for particulate sampling began in 1971.

Significant changes in annual PM<sub>10</sub> levels can be caused by a number of things. Among these are simple changes of weather, particularly the wind; changes in annual fuel use associated with conservation efforts or heating demand; the frequency of precipitation events, which wash out particulates from the atmosphere; changes in average wind speed, since higher winds result in greater dilution of emissions; and a change in the frequency of southwesterly winds, which affect the amount of particulate matter transported into Connecticut from the New York City metropolitan area and from other sources of emissions located to the southwest.



TABLE 2-1  
1988-1990 PM10 ANNUAL AVERAGES AND STATISTICAL PROJECTIONS

| TOWN NAME  | SITE | YEAR | SAMPLES | ARITHMETIC MEAN | 95-PCT-LIMITS<br>LOWER | UPPER | STANDARD DEVIATION | PREDICTED DAYS OVER 150 UG/M3 | MEASURED DAYS OVER 150 UG/M3 |
|------------|------|------|---------|-----------------|------------------------|-------|--------------------|-------------------------------|------------------------------|
| ANSONIA    | 004  | 1988 | 37*     | 26.0            | 21.1                   | 31.0  | 15.720             |                               |                              |
|            | 004  | 1989 | 58      | 25.3            | 22.5                   | 28.1  | 11.597             |                               |                              |
|            | 004  | 1990 | 30*     | 21.1            | 16.6                   | 25.7  | 12.780             |                               |                              |
| BERLIN     | 002  | 1989 | 59      | 22.4            | 19.9                   | 24.9  | 10.325             |                               |                              |
|            | 002  | 1990 | 55      | 18.8            | 16.3                   | 21.2  | 9.800              |                               |                              |
| BRIDGEPORT | 010  | 1988 | 53*     | 28.6            | 24.8                   | 32.4  | 14.904             |                               |                              |
|            | 010  | 1989 | 57      | 27.3            | 24.2                   | 30.4  | 12.843             |                               |                              |
|            | 010  | 1990 | 59      | 25.0            | 21.6                   | 28.4  | 14.198             |                               |                              |
| BRIDGEPORT | 013  | 1988 | 33*     | 27.5            | 22.4                   | 32.6  | 15.032             |                               |                              |
|            | 013  | 1989 | 57      | 26.9            | 23.6                   | 30.1  | 13.412             |                               |                              |
|            | 013  | 1990 | 58      | 24.6            | 21.3                   | 27.8  | 13.451             |                               |                              |
| BRIDGEPORT | 014  | 1988 | 10*     | 33.1            | 27.4                   | 38.8  | 8.031              |                               |                              |
|            | 014  | 1989 | 59      | 36.5            | 33.0                   | 40.0  | 14.737             |                               |                              |
|            | 014  | 1990 | 59      | 32.6            | 29.1                   | 36.2  | 14.881             |                               |                              |
| BRISTOL    | 001  | 1988 | 29*     | 22.9            | 18.7                   | 27.2  | 11.730             |                               |                              |
|            | 001  | 1989 | 60      | 22.9            | 20.5                   | 25.2  | 9.936              |                               |                              |
|            | 001  | 1990 | 60      | 20.1            | 17.7                   | 22.5  | 10.058             |                               |                              |
| BURLINGTON | 001  | 1988 | 44*     | 17.7            | 13.6                   | 21.8  | 14.312             |                               |                              |
|            | 001  | 1989 | 59      | 15.2            | 13.5                   | 16.9  | 7.171              |                               |                              |
|            | 001  | 1990 | 59      | 14.8            | 12.7                   | 16.8  | 8.573              |                               |                              |
| CORNWALL   | 005  | 1988 | 17*     | 10.8            | 7.4                    | 14.2  | 6.723              |                               |                              |
|            | 005  | 1989 | 60      | 15.1            | 13.1                   | 17.1  | 8.587              |                               |                              |
|            | 005  | 1990 | 58      | 16.0            | 13.4                   | 18.7  | 10.949             |                               |                              |
| DANBURY    | 123  | 1988 | 36*     | 25.8            | 21.2                   | 30.4  | 14.363             |                               |                              |
|            | 123  | 1989 | 57      | 25.4            | 22.6                   | 28.3  | 11.743             |                               |                              |
|            | 123  | 1990 | 60      | 22.1            | 19.4                   | 24.7  | 11.272             |                               |                              |

\* THE NUMBER OF SAMPLES FOR THE YEAR IS INSUFFICIENT TO COMPLY WITH THE MINIMUM SAMPLING CRITERIA.

TABLE 2-1, CONTINUED  
1988-1990 PM10 ANNUAL AVERAGES AND STATISTICAL PROJECTIONS

| TOWN NAME     | SITE | YEAR | SAMPLES | ARITHMETIC MEAN | 95-PCT-LIMITS<br>LOWER | UPPER | STANDARD DEVIATION | PREDICTED DAYS OVER 150 UG/M3 | MEASURED DAYS OVER 150 UG/M3 |
|---------------|------|------|---------|-----------------|------------------------|-------|--------------------|-------------------------------|------------------------------|
| DARIEN        | 001  | 1989 | 45*     | 28.7            | 25.0                   | 32.4  | 13.200             |                               |                              |
| DARIEN        | 001  | 1990 | 58      | 31.0            | 27.6                   | 34.3  | 13.869             |                               |                              |
| EAST HARTFORD | 004  | 1988 | 27*     | 24.6            | 20.0                   | 29.2  | 12.093             |                               |                              |
| EAST HARTFORD | 004  | 1989 | 59      | 25.8            | 22.9                   | 28.8  | 12.329             |                               |                              |
| EAST HARTFORD | 004  | 1990 | 59      | 21.8            | 18.9                   | 24.7  | 12.030             |                               |                              |
| ENFIELD       | 005  | 1988 | 27*     | 20.3            | 16.6                   | 24.1  | 9.832              |                               |                              |
| ENFIELD       | 005  | 1989 | 58      | 19.6            | 17.5                   | 21.8  | 8.784              |                               |                              |
| ENFIELD       | 005  | 1990 | 58      | 16.6            | 14.5                   | 18.7  | 8.763              |                               |                              |
| GREENWICH     | 017  | 1988 | 34*     | 24.9            | 19.4                   | 30.3  | 16.432             |                               |                              |
| GREENWICH     | 017  | 1989 | 56      | 21.4            | 18.7                   | 24.1  | 11.003             |                               |                              |
| GREENWICH     | 017  | 1990 | 57      | 20.4            | 17.5                   | 23.3  | 11.953             |                               |                              |
| GROTON        | 006  | 1988 | 28*     | 21.6            | 17.2                   | 26.1  | 11.860             |                               |                              |
| GROTON        | 006  | 1989 | 59      | 20.0            | 17.7                   | 22.3  | 9.689              |                               |                              |
| GROTON        | 006  | 1990 | 56      | 18.8            | 16.1                   | 21.4  | 10.730             |                               |                              |
| HADDAM        | 002  | 1988 | 26*     | 17.6            | 13.8                   | 21.4  | 9.688              |                               |                              |
| HADDAM        | 002  | 1989 | 59      | 18.5            | 16.4                   | 20.5  | 8.468              |                               |                              |
| HADDAM        | 002  | 1990 | 53*     | 16.6            | 14.3                   | 18.8  | 8.751              |                               |                              |
| HARTFORD      | 013  | 1988 | 38*     | 23.3            | 19.4                   | 27.3  | 12.724             |                               |                              |
| HARTFORD      | 013  | 1989 | 57      | 23.3            | 20.8                   | 25.8  | 10.299             |                               |                              |
| HARTFORD      | 013  | 1990 | 59      | 20.7            | 18.2                   | 23.2  | 10.526             |                               |                              |
| HARTFORD      | 014  | 1988 | 25*     | 21.6            | 18.1                   | 25.2  | 8.984              |                               |                              |
| HARTFORD      | 014  | 1989 | 58      | 24.4            | 21.4                   | 27.4  | 12.352             |                               |                              |
| HARTFORD      | 014  | 1990 | 55      | 21.6            | 18.8                   | 24.4  | 11.331             |                               |                              |
| HARTFORD      | 015  | 1988 | 54      | 29.9            | 26.1                   | 33.8  | 15.261             |                               |                              |
| HARTFORD      | 015  | 1989 | 59      | 29.5            | 26.6                   | 32.3  | 11.918             |                               |                              |
| HARTFORD      | 015  | 1990 | 58      | 24.9            | 22.0                   | 27.8  | 11.864             |                               |                              |

\* THE NUMBER OF SAMPLES FOR THE YEAR IS INSUFFICIENT TO COMPLY WITH THE MINIMUM SAMPLING CRITERIA.

TABLE 2-1, CONTINUED  
1988-1990 PM10 ANNUAL AVERAGES AND STATISTICAL PROJECTIONS

| TOWN NAME   | SITE | YEAR | SAMPLES | ARITHMETIC 95-PCT-LIMITS |             | STANDARD DEVIATION | PREDICTED DAYS OVER 150 UG/M3 | MEASURED DAYS OVER 150 UG/M3 |
|-------------|------|------|---------|--------------------------|-------------|--------------------|-------------------------------|------------------------------|
|             |      |      |         | MEAN                     | LOWER UPPER |                    |                               |                              |
| HARTFORD    | 018  | 1988 | 7*      | 25.7                     | 16.4 35.0   | 10.124             |                               |                              |
|             | 018  | 1989 | 60      | 28.0                     | 25.1 30.9   | 12.232             |                               |                              |
|             | 018  | 1990 | 60      | 24.1                     | 21.1 27.0   | 12.684             |                               |                              |
| MANCHESTER  | 001  | 1988 | 26*     | 19.6                     | 15.6 23.5   | 10.150             |                               |                              |
|             | 001  | 1989 | 58      | 21.2                     | 18.8 23.5   | 9.687              |                               |                              |
|             | 001  | 1990 | 55      | 19.1                     | 16.5 21.6   | 10.404             |                               |                              |
| MERIDEN     | 002  | 1988 | 25*     | 22.7                     | 18.7 26.7   | 10.027             |                               |                              |
|             | 002  | 1989 | 48*     | 24.3                     | 21.4 27.2   | 10.722             |                               |                              |
|             | 002  | 1990 | 37*     | 21.4                     | 18.0 24.8   | 10.792             |                               |                              |
| MIDDLETOWN  | 003  | 1988 | 26*     | 23.0                     | 18.7 27.3   | 11.019             |                               |                              |
|             | 003  | 1989 | 57      | 23.2                     | 20.4 25.9   | 11.154             |                               |                              |
|             | 003  | 1990 | 58      | 20.5                     | 18.0 23.0   | 10.360             |                               |                              |
| MILFORD     | 010  | 1988 | 9*      | 19.1                     | 14.6 23.6   | 5.934              |                               |                              |
|             | 010  | 1989 | 58      | 22.0                     | 19.6 24.4   | 9.861              |                               |                              |
|             | 010  | 1990 | 58      | 21.2                     | 18.5 23.9   | 11.180             |                               |                              |
| NAUGATUCK   | 001  | 1988 | 29*     | 25.8                     | 21.1 30.5   | 12.957             |                               |                              |
|             | 001  | 1989 | 60      | 26.4                     | 23.5 29.2   | 12.146             |                               |                              |
|             | 001  | 1990 | 56      | 23.4                     | 20.3 26.5   | 12.583             |                               |                              |
| NEW BRITAIN | 012  | 1988 | 22*     | 19.9                     | 16.7 23.1   | 7.397              |                               |                              |
|             | 012  | 1989 | 61      | 24.2                     | 21.5 26.9   | 11.676             |                               |                              |
|             | 012  | 1990 | 58      | 21.3                     | 18.6 24.0   | 11.223             |                               |                              |
| NEW HAVEN   | 013  | 1988 | 39*     | 26.2                     | 21.9 30.4   | 13.873             |                               |                              |
|             | 013  | 1989 | 57      | 24.9                     | 22.4 27.3   | 10.140             |                               |                              |
|             | 013  | 1990 | 60      | 23.7                     | 20.8 26.5   | 12.172             |                               |                              |
| NEW HAVEN   | 018  | 1988 | 300     | 45.6                     | 44.5 46.6   | 21.269             | 1                             |                              |
|             | 018  | 1989 | 351     | 44.1                     | 43.7 44.5   | 20.213             | 1                             |                              |
|             | 018  | 1990 | 349     | 40.6                     | 40.2 41.1   | 19.749             |                               |                              |

\* THE NUMBER OF SAMPLES FOR THE YEAR IS INSUFFICIENT TO COMPLY WITH THE MINIMUM SAMPLING CRITERIA.

TABLE 2-1, CONTINUED  
1988-1990 PM10 ANNUAL AVERAGES AND STATISTICAL PROJECTIONS

| TOWN NAME    | SITE | YEAR | SAMPLES | ARITHMETIC 95-PCT-LIMITS |             | STANDARD DEVIATION | PREDICTED DAYS OVER 150 UG/M3 | MEASURED DAYS OVER 150 UG/M3 |
|--------------|------|------|---------|--------------------------|-------------|--------------------|-------------------------------|------------------------------|
|              |      |      |         | MEAN                     | LOWER UPPER |                    |                               |                              |
| NEW HAVEN    | 020  | 1988 | 31*     | 30.0                     | 25.4 34.5   | 12.933             |                               |                              |
|              | 020  | 1989 | 59      | 28.8                     | 26.0 31.6   | 11.659             |                               |                              |
|              | 020  | 1990 | 60      | 26.5                     | 23.6 29.4   | 12.392             |                               |                              |
| NEW HAVEN    | 123  | 1988 | 37*     | 28.5                     | 24.0 32.9   | 14.069             |                               |                              |
|              | 123  | 1989 | 59      | 27.9                     | 25.1 30.6   | 11.561             |                               |                              |
|              | 123  | 1990 | 55      | 26.7                     | 23.3 30.1   | 13.549             |                               |                              |
| NEW LONDON   | 004  | 1989 | 42*     | 21.7                     | 18.6 24.8   | 10.615             |                               |                              |
|              | 004  | 1990 | 58      | 20.6                     | 18.1 23.0   | 10.210             |                               |                              |
| NORWALK      | 014  | 1988 | 13*     | 33.9                     | 29.2 38.6   | 7.956              |                               |                              |
|              | 014  | 1989 | 57      | 37.4                     | 33.7 41.0   | 14.853             |                               |                              |
|              | 014  | 1990 | 59      | 38.7                     | 34.7 42.6   | 16.628             |                               |                              |
| NORWICH      | 002  | 1988 | 29*     | 24.4                     | 19.9 28.8   | 12.138             |                               |                              |
|              | 002  | 1989 | 60      | 23.5                     | 21.0 25.9   | 10.509             |                               |                              |
|              | 002  | 1990 | 59      | 20.7                     | 18.2 23.2   | 10.378             |                               |                              |
| OLD SAYBROOK | 005  | 1988 | 24*     | 21.3                     | 17.9 24.6   | 8.278              |                               |                              |
|              | 005  | 1989 | 59      | 23.2                     | 20.6 25.8   | 10.856             |                               |                              |
| PUTNAM       | 002  | 1988 | 27*     | 18.8                     | 15.3 22.4   | 9.298              |                               |                              |
|              | 002  | 1989 | 59      | 20.2                     | 18.0 22.4   | 9.224              |                               |                              |
|              | 002  | 1990 | 49*     | 19.2                     | 16.6 21.8   | 9.623              |                               |                              |
| STAMFORD     | 001  | 1988 | 25*     | 24.2                     | 18.5 29.9   | 14.319             |                               |                              |
|              | 001  | 1989 | 59      | 26.0                     | 23.0 29.0   | 12.567             |                               |                              |
|              | 001  | 1990 | 59      | 24.0                     | 20.8 27.2   | 13.461             |                               |                              |
| STAMFORD     | 026  | 1988 | 11*     | 26.3                     | 16.7 35.8   | 14.461             |                               |                              |
| STRATFORD    | 005  | 1988 | 26*     | 24.1                     | 19.4 28.8   | 12.071             |                               |                              |
|              | 005  | 1989 | 60      | 25.0                     | 22.4 27.7   | 11.300             |                               |                              |
|              | 005  | 1990 | 55      | 24.3                     | 20.8 27.7   | 13.678             |                               |                              |

\* THE NUMBER OF SAMPLES FOR THE YEAR IS INSUFFICIENT TO COMPLY WITH THE MINIMUM SAMPLING CRITERIA.

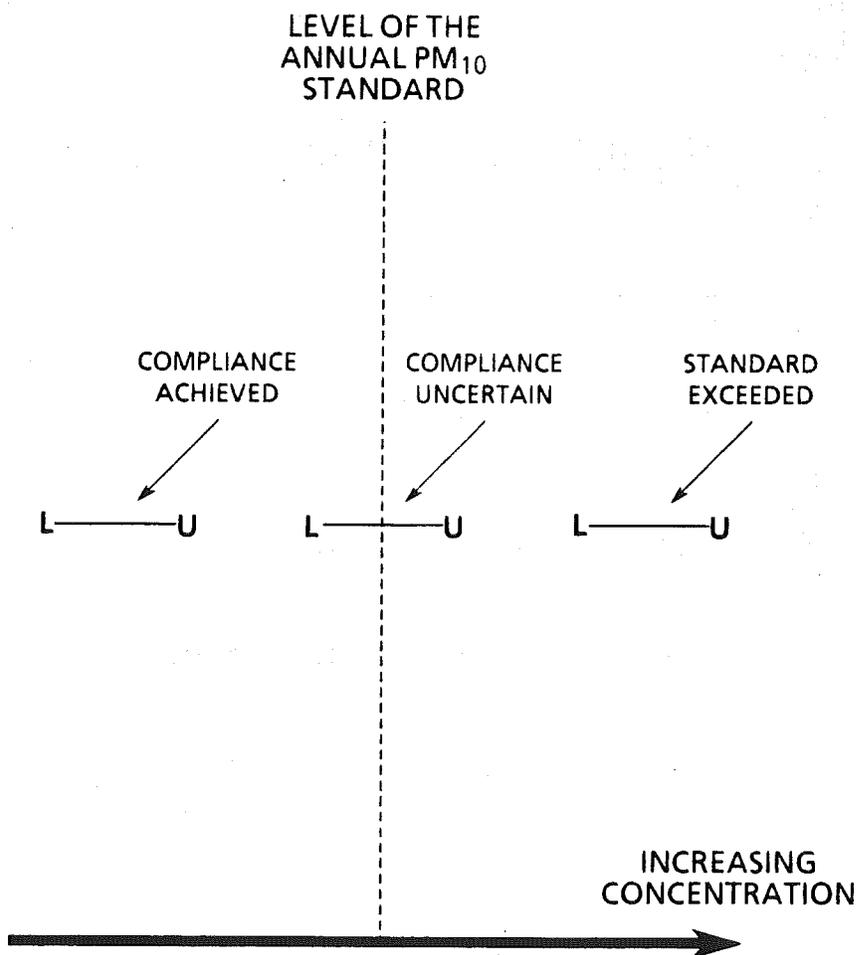
TABLE 2-1, CONTINUED  
 1988-1990 PM10 ANNUAL AVERAGES AND STATISTICAL PROJECTIONS

| TOWN NAME   | SITE | YEAR | SAMPLES | ARITHMETIC 95-PCT-LIMITS |       |        | STANDARD DEVIATION | PREDICTED DAYS OVER 150 UG/M3 | MEASURED DAYS OVER 150 UG/M3 |
|-------------|------|------|---------|--------------------------|-------|--------|--------------------|-------------------------------|------------------------------|
|             |      |      | MEAN    | LOWER                    | UPPER |        |                    |                               |                              |
| TORRINGTON  | 001  | 1988 | 21.5    | 17.5                     | 25.5  | 10.675 |                    |                               |                              |
| TORRINGTON  | 001  | 1989 | 22.9    | 20.4                     | 25.4  | 10.474 |                    |                               |                              |
| TORRINGTON  | 001  | 1990 | 19.5    | 16.9                     | 22.1  | 10.923 |                    |                               |                              |
| VOLUNTOWN   | 001  | 1988 | 16.7    | 13.2                     | 20.2  | 11.457 |                    |                               |                              |
| VOLUNTOWN   | 001  | 1989 | 15.3    | 13.4                     | 17.3  | 7.947  |                    |                               |                              |
| VOLUNTOWN   | 001  | 1990 | 14.3    | 12.4                     | 16.3  | 8.292  |                    |                               |                              |
| WALLINGFORD | 006  | 1988 | 24.3    | 17.9                     | 30.7  | 8.446  |                    |                               |                              |
| WALLINGFORD | 006  | 1989 | 22.2    | 19.9                     | 24.5  | 9.510  |                    |                               |                              |
| WALLINGFORD | 006  | 1990 | 19.5    | 16.8                     | 22.1  | 10.291 |                    |                               |                              |
| WATERBURY   | 007  | 1988 | 27.2    | 22.6                     | 31.9  | 12.792 |                    |                               |                              |
| WATERBURY   | 007  | 1989 | 28.3    | 24.8                     | 31.7  | 14.142 |                    |                               |                              |
| WATERBURY   | 007  | 1990 | 25.6    | 22.1                     | 29.1  | 14.752 |                    |                               |                              |
| WATERBURY   | 123  | 1988 | 32.9    | 28.5                     | 37.4  | 18.257 |                    |                               |                              |
| WATERBURY   | 123  | 1989 | 33.0    | 29.1                     | 36.9  | 16.235 |                    |                               |                              |
| WATERBURY   | 123  | 1990 | 32.4    | 28.4                     | 36.4  | 16.652 |                    |                               |                              |
| WATERFORD   | 001  | 1988 | 20.9    | 15.9                     | 25.8  | 13.255 |                    |                               |                              |
| WATERFORD   | 001  | 1989 | 17.5    | 15.5                     | 19.5  | 8.309  |                    |                               |                              |
| WATERFORD   | 001  | 1990 | 18.4    | 15.7                     | 21.0  | 10.669 |                    |                               |                              |
| WEST HAVEN  | 003  | 1988 | 27.6    | 23.9                     | 31.3  | 12.572 |                    |                               |                              |
| WEST HAVEN  | 003  | 1989 | 27.9    | 25.3                     | 30.5  | 11.109 |                    |                               |                              |
| WEST HAVEN  | 003  | 1990 | 26.8    | 24.0                     | 29.6  | 11.570 |                    |                               |                              |
| WILLIMANTIC | 002  | 1988 | 20.5    | 17.2                     | 23.7  | 8.736  |                    |                               |                              |
| WILLIMANTIC | 002  | 1989 | 21.0    | 18.8                     | 23.2  | 9.174  |                    |                               |                              |
| WILLIMANTIC | 002  | 1990 | 18.5    | 16.3                     | 20.7  | 9.318  |                    |                               |                              |

\* THE NUMBER OF SAMPLES FOR THE YEAR IS INSUFFICIENT TO COMPLY WITH THE MINIMUM SAMPLING CRITERIA.

**FIGURE 2-2**

**COMPLIANCE WITH THE LEVEL OF THE ANNUAL PM<sub>10</sub> STANDARDS**  
**USING 95% CONFIDENCE LIMITS ABOUT**  
**THE ANNUAL ARITHMETIC MEAN CONCENTRATION**



L = The lower limit of the 95% confidence interval about the annual arithmetic mean concentration.

U = The upper limit of the 95% confidence interval about the annual arithmetic mean concentration.

**TABLE 2-2**

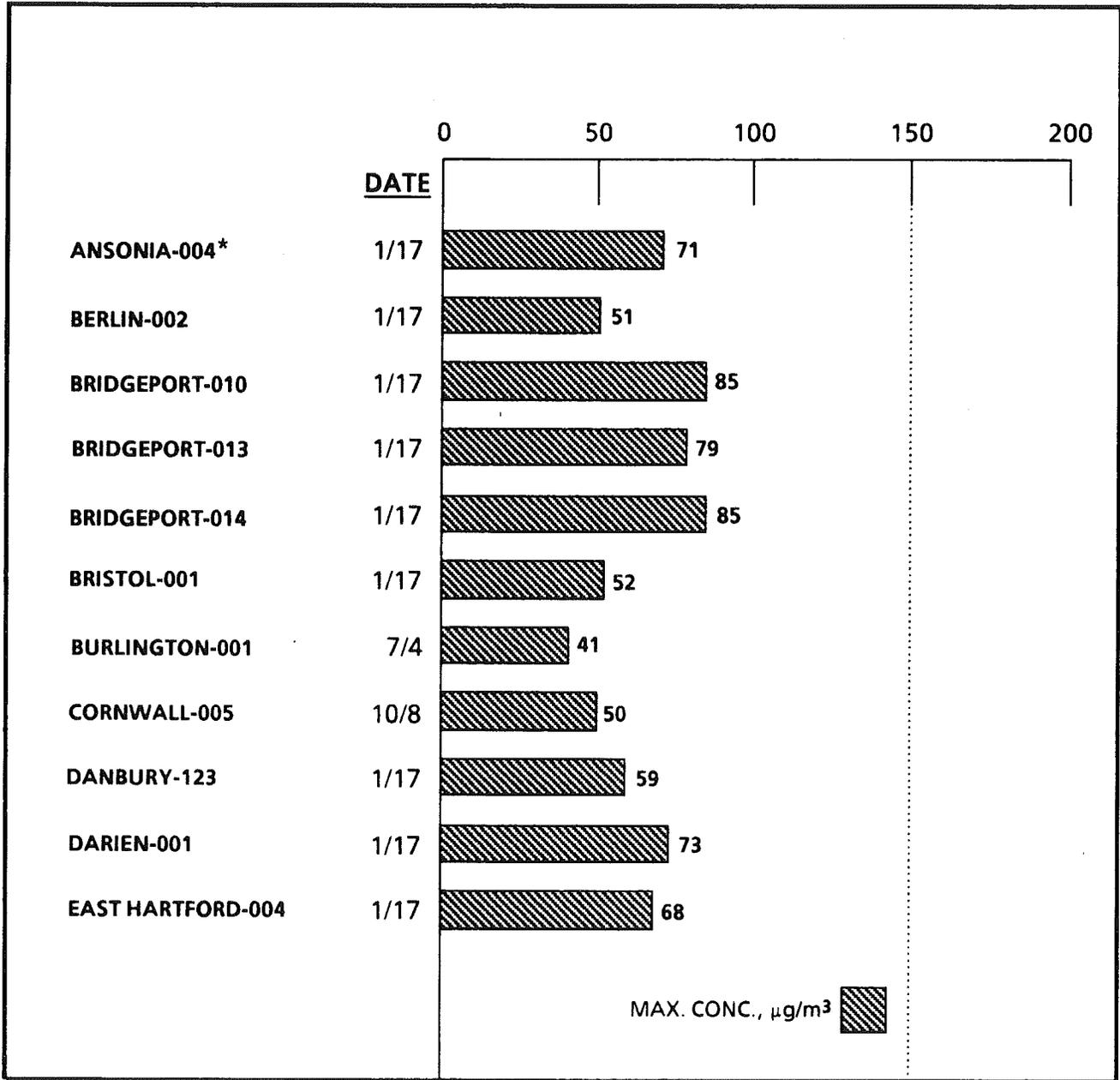
**STATISTICALLY PREDICTED NUMBER OF SITES**  
**IN COMPLIANCE WITH THE LEVEL OF THE**  
**ANNUAL PM10 STANDARDS \***

|      | <b>COMPLIANCE<br/>ACHIEVED</b> | <b>COMPLIANCE<br/>UNCERTAIN</b> | <b>STANDARD<br/>EXCEEDED</b> |
|------|--------------------------------|---------------------------------|------------------------------|
| 1985 | 2                              | 0                               | 0                            |
| 1986 | 4                              | 0                               | 1                            |
| 1987 | 4                              | 0                               | 1                            |
| 1988 | 3                              | 0                               | 0                            |
| 1989 | 40                             | 0                               | 0                            |
| 1990 | 39                             | 0                               | 0                            |

\* Using 95% confidence limits about the arithmetic mean concentration at only those sites which had sufficient data to satisfy the minimum sampling criteria for the year.

## FIGURE 2-3

### 1990 MAXIMUM 24-HOUR PM10 CONCENTRATIONS

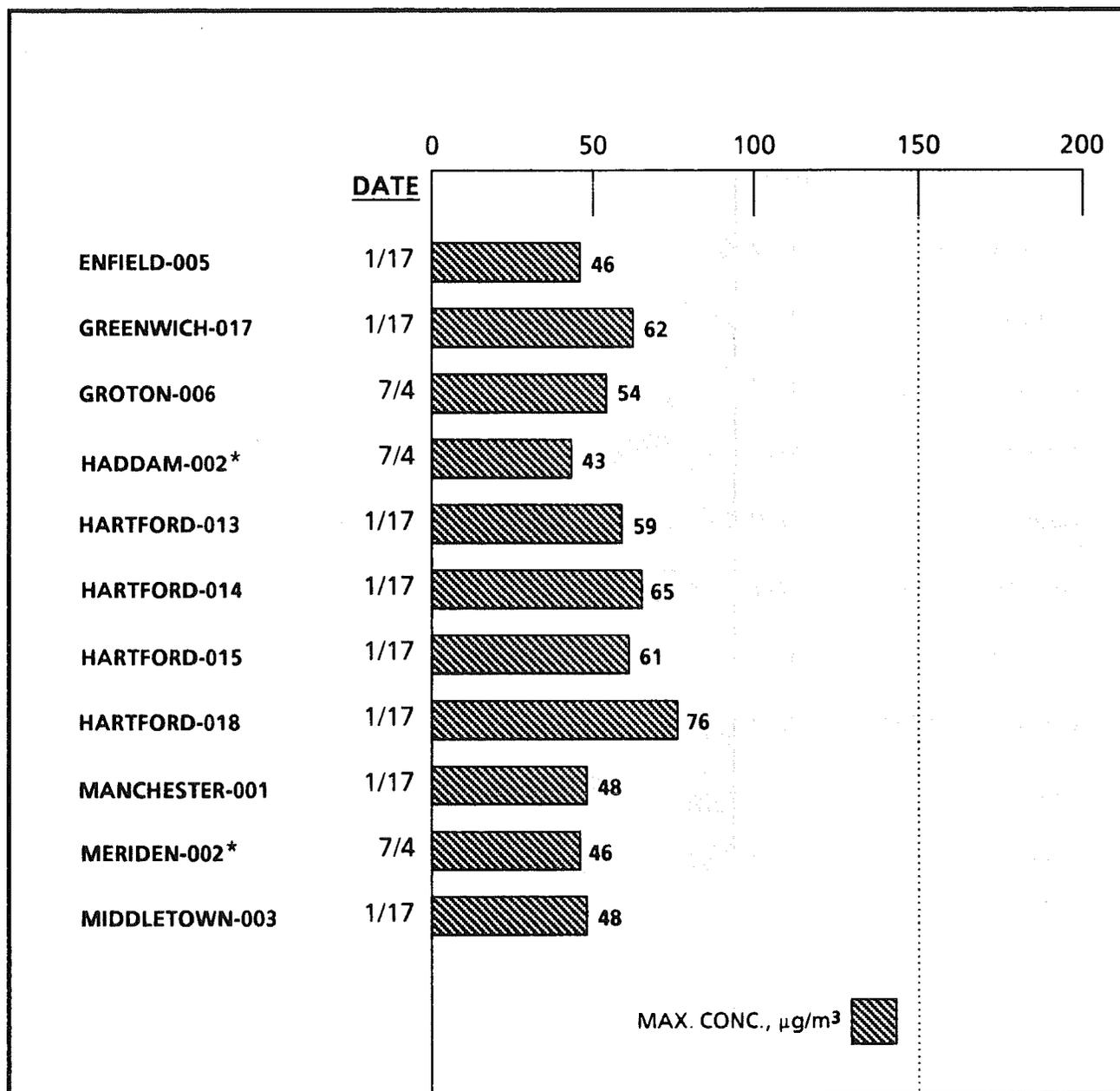


150  $\mu\text{g}/\text{m}^3$   
24 - HOUR  
STANDARD

\* The site has insufficient data to satisfy the minimum sampling criteria.

## FIGURE 2-3, continued

### 1990 MAXIMUM 24-HOUR PM10 CONCENTRATIONS

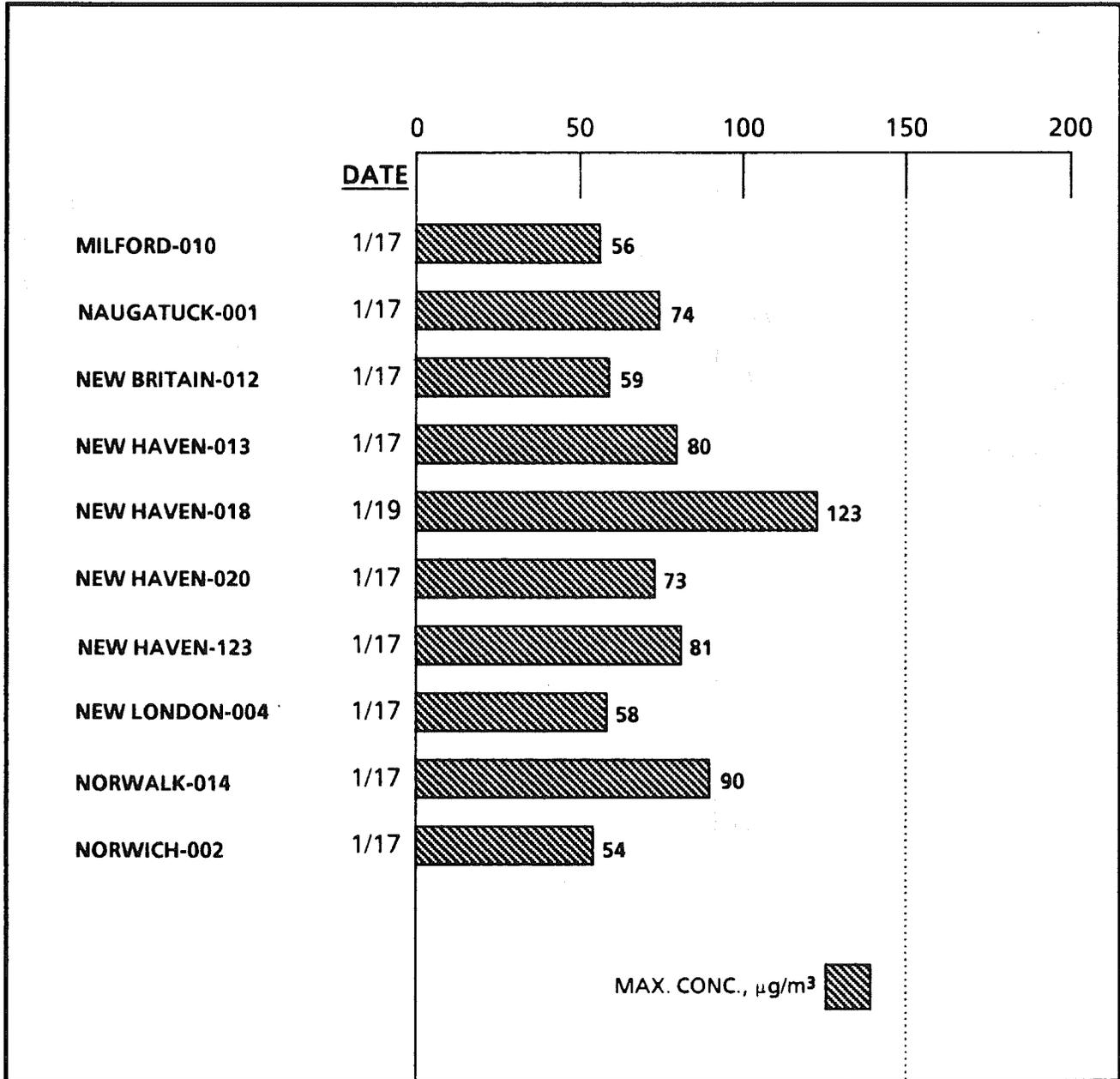


150 µg/m<sup>3</sup>  
 24 - HOUR  
 STANDARD

\* The site has insufficient data to satisfy the minimum sampling criteria.

**FIGURE 2-3, continued**

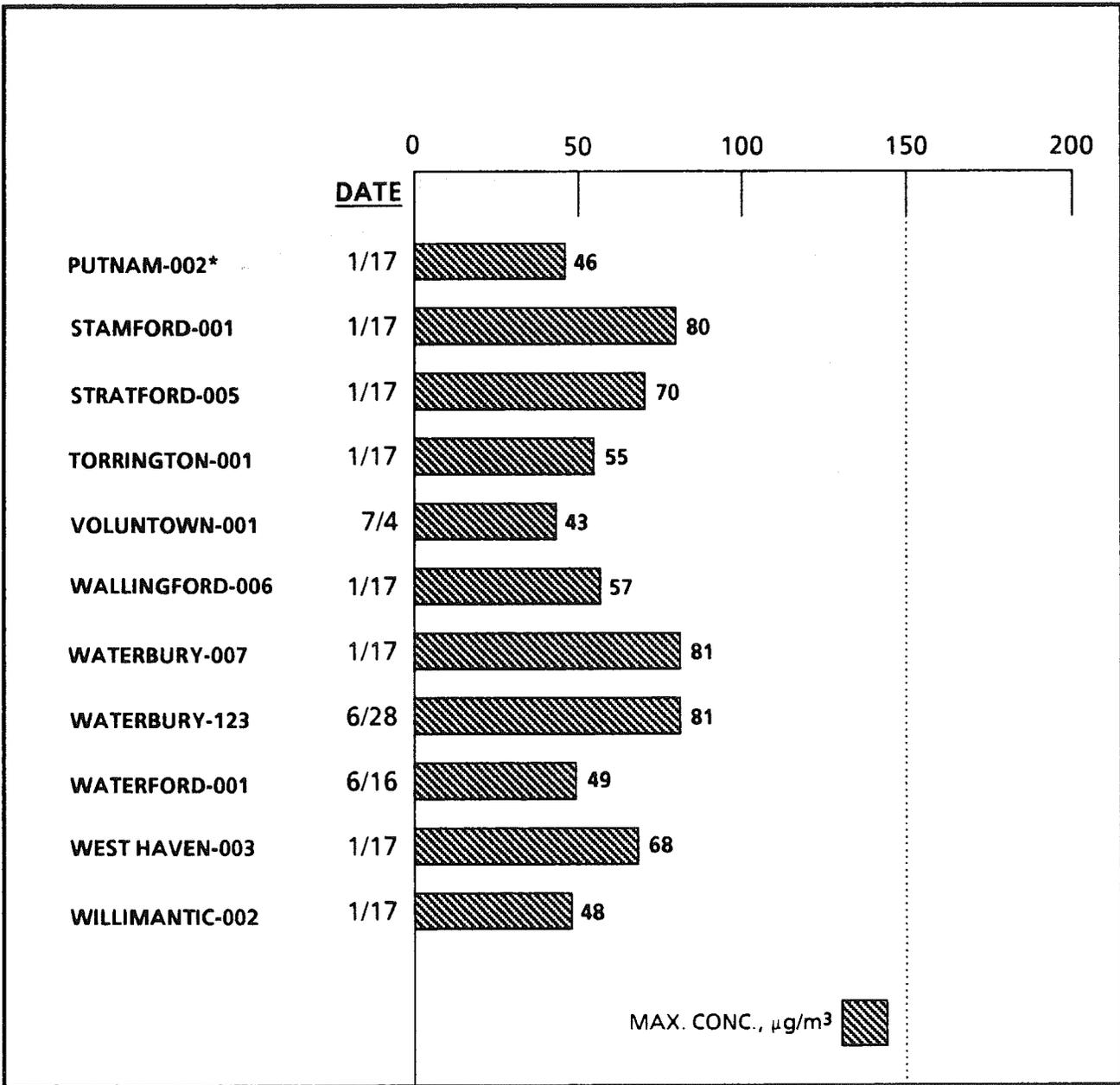
**1990 MAXIMUM 24-HOUR PM10 CONCENTRATIONS**



150  $\mu\text{g}/\text{m}^3$   
24 - HOUR  
STANDARD

FIGURE 2-3, continued

1990 MAXIMUM 24-HOUR PM10 CONCENTRATIONS



150  $\mu\text{g}/\text{m}^3$   
24 - HOUR  
STANDARD

\* The site has insufficient data to satisfy the minimum sampling criteria.

## TABLE 2-3

### SUMMARY OF THE STATISTICALLY PREDICTED NUMBER OF PM10 SITES EXCEEDING THE LEVEL OF THE 24-HOUR STANDARDS

| <u>YEAR</u> | <u>NO. OF SITES<sup>1</sup></u> | <u>SITES WITH <math>\geq</math> 1 DAY<br/>EXCEEDING 150 <math>\mu\text{g}/\text{m}^3</math></u> |                                    |
|-------------|---------------------------------|---|------------------------------------|
|             |                                 | <u>No. of Sites</u>   | <u>Percentage<br/>of All Sites</u> |
| 1985        | 2                               | 0   | 0%                                 |
| 1986        | 5                               | 2   | 40%                                |
| 1987        | 5                               | 1   | 20%                                |
| 1988        | 3                               | 1   | 33%                                |
| 1989        | 40                              | 1   | 3%                                 |
| 1990        | 39                              | 0   | 0%                                 |

<sup>1</sup> Only those sites are used which had sufficient data to satisfy the minimum sampling criteria.

TABLE 2-4

MONTHLY CHEMICAL CHARACTERIZATION OF 1990 LO-VOL TSP

|  | MONTHLY AVERAGE |      |      |      |      |      |      |      |      |      |      |      | ANNUAL AVG |      |
|--|-----------------|------|------|------|------|------|------|------|------|------|------|------|------------|------|
|  | JAN             | FEB  | MAR  | APR  | MAY  | JUN  | JUL  | AUG  | SEP  | OCT  | NOV  | DEC  |            |      |
| TOWN<br>Bridgeport                       |                 |      |      |      |      |      |      |      |      |      |      |      |            |      |
| AREA<br>0060                             |                 |      |      |      |      |      |      |      |      |      |      |      |            |      |
| SITE<br>010                              |                 |      |      |      |      |      |      |      |      |      |      |      |            |      |
| <u>METALS (ng/m<sup>3</sup>)</u>         |                 |      |      |      |      |      |      |      |      |      |      |      |            |      |
| BERYLLIUM                                | <0.1            | <0.1 | <0.1 | <0.1 | <0.1 | <0.1 | <0.1 | <0.1 | <0.1 | <0.1 | <0.1 | <0.1 | <0.1       | <0.1 |
| CADMIUM                                  | 1.3             | 1.4  | 1.1  | 1.2  | 0.8  | 0.6  | 1.8  | 0.9  | 0.8  | 1.6  | 1.2  | 1.2  | 1.2        | 1.2  |
| CHROMIUM                                 | 15              | 8    | 6    | 6    | 4    | 4    | 3    | 3    | 6    | 6    | 4    | 4    | 6          | 6    |
| COPPER                                   | 30              | 30   | 30   | 20   | 20   | 20   | 10   | 10   | 10   | 10   | 20   | 20   | 20         | 20   |
| IRON                                     | 2030            | 1070 | 1920 | 1540 | 1110 | 1190 | 1060 | 960  | 550  | 410  | 480  | 480  | 1120       | 1120 |
| LEAD                                     | 50              | 30   | 40   | 40   | 30   | 30   | 30   | 10   | 10   | 30   | 10   | 10   | 30         | 30   |
| MANGANESE                                | 20              | 14   | 20   | 16   | 14   | 14   | 12   | 13   | 11   | 16   | 9    | 9    | 14         | 14   |
| NICKEL                                   | 26              | 18   | 19   | 13   | 9    | 8    | 8    | 6    | 7    | 12   | 11   | 11   | 12         | 12   |
| VANADIUM                                 | 40              | 30   | 30   | 20   | 10   | 10   | 10   | 10   | 20   | 20   | 20   | 20   | 20         | 20   |
| ZINC                                     | 110             | 110  | 110  | 60   | 50   | 80   | 80   | 80   | 40   | 30   | 60   | 60   | 70         | 70   |
| <u>WATER SOLUBLES (ng/m<sup>3</sup>)</u> |                 |      |      |      |      |      |      |      |      |      |      |      |            |      |
| NITRATE                                  | 4240            | 3270 | 4580 | 3000 | 3700 | 4160 | 3290 | 3430 | 2530 | 2540 | 2250 | 2250 | 3360       | 3360 |
| SULFATE                                  | 8090            | 8570 | 7540 | 8310 | 8290 | 9080 | 9540 | 6780 | 5470 | 7360 | 6270 | 6270 | 7750       | 7750 |
| AMMONIUM                                 | 1180            | 310  | 410  | 100  | 10   | 20   | 190  | 50   | 60   | 220  | 420  | 420  | 270        | 270  |
| TSP (µg/m <sup>3</sup> )                 | 90              | 58   | 87   | 55   | 53   | 51   | 50   | 44   | 36   | 46   | 38   | 38   | 55         | 55   |

**TABLE 2-4, continued**

**MONTHLY CHEMICAL CHARACTERIZATION OF 1990 LO-VOL TSP**

|  | JAN  | FEB  | MAR  | APR  | MAY  | MONTHLY AVERAGE       |              |             |      |      |      |      |      |      |      |  |  | ANNUAL AVG |
|--|------|------|------|------|------|-----------------------|--------------|-------------|------|------|------|------|------|------|------|--|--|------------|
|  |      |      |      |      |      | TOWN<br>East Hartford | AREA<br>0220 | SITE<br>004 | JUN  | JUL  | AUG  | SEP  | OCT  | NOV  | DEC  |  |  |            |
| <u>METALS (ng/m<sup>3</sup>)</u>         |      |      |      |      |      |                       |              |             |      |      |      |      |      |      |      |  |  |            |
| BERYLLIUM                                | <0.1 | <0.1 | <0.1 | <0.1 | <0.1 | <0.1                  | <0.1         | <0.1        | <0.1 | <0.1 | <0.1 | <0.1 | <0.1 | <0.1 | <0.1 |  |  |            |
| CADMIUM                                  | 1.1  | 1.3  | 2.1  | 2.1  | 0.7  | 0.7                   | 0.2          | 0.8         | 0.8  | 0.7  | 0.7  | 0.8  | 0.8  | 0.5  | 0.5  |  |  |            |
| CHROMIUM                                 | 6    | 5    | 2    | 2    | 3    | 3                     | 0            | 1           | 3    | 3    | 4    | 4    | 2    | 2    | 2    |  |  |            |
| COPPER                                   | 40   | 30   | 10   | 10   | 10   | 10                    | 0            | 5           | 10   | 10   | 10   | 10   | 10   | 10   | 10   |  |  |            |
| IRON                                     | 1160 | 920  | 800  | 1110 | 300  | 550                   | 730          | 850         | 320  | 30   | 30   | 30   | 30   | 30   | 30   |  |  |            |
| LEAD                                     | 40   | 30   | 20   | 20   | 4    | 10                    | 20           | 30          | 30   | 30   | 30   | 30   | 30   | 30   | 30   |  |  |            |
| MANGANESE                                | 14   | 14   | 12   | 17   | 4    | 7                     | 8            | 11          | 5    | 5    | 5    | 5    | 5    | 5    | 5    |  |  |            |
| NICKEL                                   | 18   | 12   | 6    | 11   | 1    | 6                     | 7            | 9           | 3    | 3    | 3    | 3    | 3    | 3    | 3    |  |  |            |
| VANADIUM                                 | 30   | 20   | 10   | 10   | 1    | 4                     | 4            | 10          | 4    | 4    | 4    | 10   | 4    | 4    | 4    |  |  |            |
| ZINC                                     | 100  | 80   | 40   | 50   | 10   | 70                    | 100          | 170         | 80   | 80   | 80   | 80   | 80   | 80   | 80   |  |  |            |
| <u>WATER SOLUBLES (ng/m<sup>3</sup>)</u> |      |      |      |      |      |                       |              |             |      |      |      |      |      |      |      |  |  |            |
| NITRATE                                  | 2900 | 2770 | 2510 | 3670 | 1030 | 2470                  | 2450         | 2580        | 1210 | 1210 | 1210 | 1210 | 1210 | 1210 | 1210 |  |  |            |
| SULFATE                                  | 7070 | 8440 | 8970 | 8690 | 3780 | 6530                  | 5760         | 5650        | 3680 | 3680 | 3680 | 3680 | 3680 | 3680 | 3680 |  |  |            |
| AMMONIUM                                 | 470  | 30   | 10   | 70   | 10   | 10                    | 60           | 50          | 260  | 260  | 260  | 260  | 260  | 260  | 260  |  |  |            |
| <u>TSP (µg/m<sup>3</sup>)</u>            | 68   | 57   | 44   | 55   | 17   | 32                    | 33           | 41          | 19   | 19   | 19   | 19   | 19   | 19   | 19   |  |  |            |

TABLE 2-4, continued

MONTHLY CHEMICAL CHARACTERIZATION OF 1990 LO-VOL TSP

|  | MONTHLY AVERAGE |      |      |      |      |      |        |      |      |      |      |      | ANNUAL AVG |      |
|--|-----------------|------|------|------|------|------|--------|------|------|------|------|------|------------|------|
|  | JAN             | FEB  | MAR  | APR  | MAY  | JUN  | JUL    | AUG  | SEP  | OCT  | NOV  | DEC  |            |      |
|  |                 |      |      |      |      |      |        |      |      |      |      |      | TOWN       | SITE |
|  |                 |      |      |      |      |      |        |      |      |      |      |      | Hartford   | 016  |
|  |                 |      |      |      |      |      |        |      |      |      |      |      | AREA       |      |
|  |                 |      |      |      |      |      |        |      |      |      |      |      | 0420       |      |
| <u>METALS (ng/m<sup>3</sup>)</u>         |                 |      |      |      |      |      |        |      |      |      |      |      |            |      |
| BERYLLIUM                                | <0.1            | <0.1 | <0.1 | <0.1 | <0.1 | <0.1 | <0.1   | <0.1 | <0.1 | <0.1 | <0.1 | <0.1 | <0.1       |      |
| CADMIUM                                  | 1.3             | 1.1  | 1.0  | 0.7  | 0.6  | 1.5  | 1.0    | 0.8  | 0.6  |      |      |      |            |      |
| CHROMIUM                                 | 7               | 7    | 6    | 4    | 4    | 5    | 3      | 3    | 4    |      |      |      |            |      |
| COPPER                                   | 20              | 20   | 20   | 20   | 20   | 20   | 10     | 10   | 10   |      |      |      |            |      |
| IRON                                     | 1720            | 2120 | 2580 | 1530 | 1840 | 1920 | 1160   | 1000 | 1010 |      |      |      |            |      |
| LEAD                                     | 40              | 50   | 50   | 30   | 50   | 40   | 30     | 20   | 20   |      |      |      |            |      |
| MANGANESE                                | 18              | 24   | 26   | 18   | 23   | 24   | 14     | 12   | 13   |      |      |      |            |      |
| NICKEL                                   | 18              | 17   | 15   | 8    | 6    | 11   | 6      | 6    | 6    |      |      |      |            |      |
| VANADIUM                                 | 30              | 30   | 20   | 10   | 10   | 10   | 10     | 10   | 10   |      |      |      |            |      |
| ZINC                                     | 100             | 130  | 120  | 70   | 70   | 110  | 80     | 80   | 80   |      |      |      |            |      |
| <u>WATER SOLUBLES (ng/m<sup>3</sup>)</u> |                 |      |      |      |      |      |        |      |      |      |      |      |            |      |
| NITRATE                                  | 2610            | 3170 | 3390 | 2480 | 2460 | 2430 | 1230   | 1760 | 3120 |      |      |      |            |      |
| SULFATE                                  | 5890            | 9070 | 7760 | 7630 | 8470 | 9140 | 10,040 | 9000 | 8060 |      |      |      |            |      |
| AMMONIUM                                 | 680             | 350  | 220  | 20   | 4    | 110  | 210    | 50   | 40   |      |      |      |            |      |
| TSP (µg/m <sup>3</sup> )                 | 80              | 103  | 113  | 67   | 65   | 81   | 50     | 47   | 46   |      |      |      |            |      |

**TABLE 2-4, continued**

**MONTHLY CHEMICAL CHARACTERIZATION OF 1990 LO-VOL TSP**

|  | MONTHLY AVERAGE |        |      |      |      |      |      |      |      |      |      |      | ANNUAL AVG |      |
|--|-----------------|--------|------|------|------|------|------|------|------|------|------|------|------------|------|
|  | JAN             | FEB    | MAR  | APR  | MAY  | JUN  | JUL  | AUG  | SEP  | OCT  | NOV  | DEC  |            |      |
| <u>TOWN</u><br>New Haven                 |                 |        |      |      |      |      |      |      |      |      |      |      |            |      |
| <u>AREA</u><br>0700                      |                 |        |      |      |      |      |      |      |      |      |      |      |            |      |
| <u>SITE</u><br>018                       |                 |        |      |      |      |      |      |      |      |      |      |      |            |      |
| <u>METALS (ng/m<sup>3</sup>)</u>         |                 |        |      |      |      |      |      |      |      |      |      |      |            |      |
| BERYLLIUM                                | <0.1            | <0.1   | <0.1 | <0.1 | <0.1 | <0.1 | <0.1 | <0.1 | <0.1 | <0.1 | <0.1 | <0.1 | <0.1       | <0.1 |
| CADMIUM                                  | 2.1             | 1.9    | 2.4  | 2.1  | 1.5  | 1.4  | 2.1  | 2.8  | 1.2  | 1.5  | 2.0  | 1.0  | 1.8        | 1.8  |
| CHROMIUM                                 | 10              | 10     | 7    | 11   | 4    | 6    | 8    | 4    | 5    | 7    | 10   | 8    | 8          | 8    |
| COPPER                                   | 90              | 100    | 60   | 70   | 40   | 60   | 60   | 60   | 70   | 60   | 60   | 50   | 70         | 70   |
| IRON                                     | 4600            | 5120   | 6090 | 7330 | 3450 | 4650 | 6850 | 3590 | 4810 | 4400 | 7520 | 4720 | 5260       | 5260 |
| LEAD                                     | 100             | 80     | 70   | 80   | 40   | 60   | 80   | 50   | 70   | 80   | 90   | 100  | 80         | 80   |
| MANGANESE                                | 40              | 43     | 50   | 78   | 32   | 41   | 63   | 30   | 37   | 48   | 99   | 37   | 50         | 50   |
| NICKEL                                   | 30              | 24     | 20   | 8    | 8    | 12   | 17   | 11   | 11   | 14   | 15   | 16   | 16         | 16   |
| VANADIUM                                 | 60              | 50     | 40   | 40   | 10   | 20   | 20   | 10   | 20   | 20   | 30   | 30   | 30         | 30   |
| ZINC                                     | 210             | 200    | 180  | 180  | 80   | 120  | 230  | 120  | 170  | 160  | 220  | 150  | 170        | 170  |
| <u>WATER SOLUBLES (ng/m<sup>3</sup>)</u> |                 |        |      |      |      |      |      |      |      |      |      |      |            |      |
| NITRATE                                  | 3340            | 2980   | 3280 | 3040 | 1350 | 2720 | 3530 | 2570 | 3170 | 2420 | 1250 | 920  | 2550       | 2550 |
| SULFATE                                  | 7690            | 10,190 | 7410 | 8770 | 7490 | 7650 | 8540 | 7180 | 7060 | 4460 | 4380 | 2220 | 6920       | 6920 |
| AMMONIUM                                 | 750             | 240    | 130  | 70   | 2    | 40   | 330  | 90   | 100  | 140  | 90   | 200  | 180        | 180  |
| <u>TSP (µg/m<sup>3</sup>)</u>            | 129             | 149    | 157  | 163  | 79   | 144  | 121  | 90   | 104  | 117  | 132  | 112  | 125        | 125  |

TABLE 2-4, continued

MONTHLY CHEMICAL CHARACTERIZATION OF 1990 LO-VOL TSP

|  | MONTHLY AVERAGE |      |      |      |        |        |        |      |      |      |      |      | ANNUAL AVG |
|--|-----------------|------|------|------|--------|--------|--------|------|------|------|------|------|------------|
|  | JAN             | FEB  | MAR  | APR  | MAY    | JUN    | JUL    | AUG  | SEP  | OCT  | NOV  | DEC  |            |
|  | TOWN            |      |      |      |        |        |        |      |      |      |      |      |            |
|  | Waterbury       |      |      |      |        |        |        |      |      |      |      |      |            |
|  | AREA            |      |      |      |        |        |        |      |      |      |      |      |            |
|  | 1240            |      |      |      |        |        |        |      |      |      |      |      |            |
|  | SITE            |      |      |      |        |        |        |      |      |      |      |      |            |
|  | 123             |      |      |      |        |        |        |      |      |      |      |      |            |
| <u>METALS (ng/m<sup>3</sup>)</u>         |                 |      |      |      |        |        |        |      |      |      |      |      |            |
| BERYLLIUM                                | <0.1            | <0.1 | <0.1 | <0.1 | <0.1   | <0.1   | <0.1   | <0.1 | <0.1 | <0.1 | <0.1 | <0.1 | <0.1       |
| CADMIUM                                  | 1.7             | 1.6  | 2.1  | 2.2  | 2.3    | 1.2    | 1.7    | 1.3  | 1.4  | 1.1  | 1.1  | 1.7  | 1.7        |
| CHROMIUM                                 | 17              | 20   | 20   | 6    | 23     | 17     | 7      | 20   | 20   | 18   | 18   | 17   | 17         |
| COPPER                                   | 60              | 50   | 120  | 40   | 50     | 50     | 70     | 60   | 80   | 50   | 50   | 60   | 60         |
| IRON                                     | 2990            | 4300 | 5050 | 2540 | 6760   | 4950   | 2290   | 2660 | 2630 | 1790 | 1790 | 3600 | 3600       |
| LEAD                                     | 50              | 60   | 50   | 40   | 560    | 230    | 70     | 50   | 70   | 60   | 60   | 120  | 120        |
| MANGANESE                                | 38              | 62   | 71   | 43   | 96     | 81     | 35     | 41   | 36   | 29   | 29   | 53   | 53         |
| NICKEL                                   | 22              | 20   | 21   | 12   | 13     | 9      | 7      | 7    | 8    | 8    | 8    | 13   | 13         |
| VANADIUM                                 | 50              | 40   | 50   | 20   | 30     | 10     | 10     | 10   | 10   | 10   | 10   | 20   | 20         |
| ZINC                                     | 200             | 230  | 210  | 90   | 310    | 200    | 330    | 360  | 300  | 310  | 310  | 220  | 220        |
| <u>WATER SOLUBLES (ng/m<sup>3</sup>)</u> |                 |      |      |      |        |        |        |      |      |      |      |      |            |
| NITRATE                                  | 3270            | 2880 | 3550 | 2760 | 3190   | 3080   | 2660   | 3020 | 2330 | 2200 | 2200 | 2900 | 2900       |
| SULFATE                                  | 7120            | 9480 | 8500 | 9540 | 11,610 | 11,610 | 10,070 | 9430 | 7650 | 7020 | 7020 | 9200 | 9200       |
| AMMONIUM                                 | 1550            | 400  | 320  | 10   | 5      | 10     | 10     | 10   | 70   | 10   | 10   | 240  | 240        |
| <u>TSP (µg/m<sup>3</sup>)</u>            | 109             | 144  | 165  | 97   | 171    | 134    | 104    | 103  | 85   | 80   | 80   | 119  | 119        |

TABLE 2-5

1990 TEN HIGHEST 24-HOUR AVERAGE PM10 DAYS WITH WIND DATA

UNITS : MICROGRAMS PER CUBIC METER

| TOWN-SITE (SAMPLES)   | RANK      | 1       | 2       | 3        | 4        | 5        | 6        | 7        | 8       | 9        | 10       |
|-----------------------|-----------|---------|---------|----------|----------|----------|----------|----------|---------|----------|----------|
| BERLIN-002 (0055)     |           |         |         |          |          |          |          |          |         |          |          |
| PM10                  |           | 51      | 42      | 40       | 38       | 34       | 32       | 30       | 28      | 27       | 27       |
| DATE                  |           | 1/17/90 | 7/ 4/90 | 9/ 2/90  | 8/27/90  | 11/ 1/90 | 12/ 7/90 | 12/13/90 | 6/22/90 | 10/ 8/90 | 9/14/90  |
| METEOROLOGICAL SITE   | DIR (DEG) | 190     | 230     | 280      | 340      | 200      | 330      | 280      | 200     | 170      | 140      |
| NEWARK                | VEL (MPH) | 5.8     | 14.0    | 4.8      | 5.0      | 2.7      | 1.7      | 9.0      | 6.4     | 2.8      | 6.6      |
|                       | SPD (MPH) | 6.3     | 16.2    | 7.2      | 7.2      | 5.5      | 5.0      | 11.9     | 8.3     | 5.0      | 7.5      |
|                       | RATIO     | 0.912   | 0.861   | 0.670    | 0.694    | 0.501    | 0.334    | 0.750    | 0.773   | 0.560    | 0.881    |
| METEOROLOGICAL SITE   | DIR (DEG) | 180     | 220     | 240      | 320      | 80       | 330      | 280      | 210     | 190      | 160      |
| BRADLEY               | VEL (MPH) | 6.2     | 8.0     | 1.4      | 4.8      | .6       | 1.6      | 5.1      | 6.9     | 4.9      | 5.5      |
|                       | SPD (MPH) | 8.1     | 10.2    | 4.9      | 6.6      | 3.3      | 4.3      | 9.3      | 8.5     | 7.0      | 8.1      |
|                       | RATIO     | 0.772   | 0.781   | 0.279    | 0.727    | 0.183    | 0.375    | 0.541    | 0.819   | 0.701    | 0.681    |
| METEOROLOGICAL SITE   | DIR (DEG) | 170     | 260     | 250      | 300      | 260      | 100      | 290      | 230     | 210      | 160      |
| BRIDGEPORT            | VEL (MPH) | 1.4     | 8.2     | 6.7      | 3.5      | 1.9      | 1.3      | 7.1      | 5.5     | 1.3      | 6.1      |
|                       | SPD (MPH) | 4.6     | 8.3     | 6.9      | 5.8      | 3.9      | 2.7      | 8.1      | 5.6     | 2.9      | 6.6      |
|                       | RATIO     | 0.306   | 0.979   | 0.967    | 0.602    | 0.489    | 0.466    | 0.876    | 0.974   | 0.460    | 0.922    |
| METEOROLOGICAL SITE   | DIR (DEG) | 210     | 260     | 280      | 300      | 280      | 260      | 270      | 260     | 240      | 170      |
| WORCESTER             | VEL (MPH) | 5.0     | 9.3     | 6.6      | 4.0      | 5.9      | 3.4      | 8.9      | 6.3     | 2.5      | 4.3      |
|                       | SPD (MPH) | 5.8     | 9.3     | 7.0      | 4.2      | 6.2      | 4.3      | 10.4     | 6.8     | 5.5      | 4.3      |
|                       | RATIO     | 0.864   | 0.997   | 0.932    | 0.957    | 0.960    | 0.794    | 0.858    | 0.934   | 0.458    | 0.989    |
| BRIDGEPORT-010 (0059) |           |         |         |          |          |          |          |          |         |          |          |
| PM10                  |           | 85      | 52      | 52       | 50       | 49       | 41       | 41       | 41      | 39       | 38       |
| DATE                  |           | 1/17/90 | 7/ 4/90 | 11/ 1/90 | 9/ 2/90  | 12/13/90 | 6/22/90  | 3/12/90  | 8/27/90 | 7/22/90  | 12/ 7/90 |
| METEOROLOGICAL SITE   | DIR (DEG) | 190     | 230     | 200      | 280      | 280      | 200      | 90       | 340     | 110      | 330      |
| NEWARK                | VEL (MPH) | 5.8     | 14.0    | 2.7      | 4.8      | 9.0      | 6.4      | 3.5      | 5.0     | 2.4      | 1.7      |
|                       | SPD (MPH) | 6.3     | 16.2    | 5.5      | 7.2      | 11.9     | 8.3      | 4.7      | 7.2     | 5.0      | 5.0      |
|                       | RATIO     | 0.912   | 0.861   | 0.501    | 0.670    | 0.750    | 0.773    | 0.734    | 0.694   | 0.486    | 0.334    |
| METEOROLOGICAL SITE   | DIR (DEG) | 180     | 220     | 80       | 240      | 280      | 210      | 360      | 320     | 130      | 330      |
| BRADLEY               | VEL (MPH) | 6.2     | 8.0     | .6       | 1.4      | 5.1      | 6.9      | 4.3      | 4.8     | 3.0      | 1.6      |
|                       | SPD (MPH) | 8.1     | 10.2    | 3.3      | 4.9      | 9.3      | 8.5      | 4.3      | 6.6     | 6.5      | 4.3      |
|                       | RATIO     | 0.772   | 0.781   | 0.183    | 0.279    | 0.541    | 0.819    | 0.992    | 0.727   | 0.468    | 0.375    |
| METEOROLOGICAL SITE   | DIR (DEG) | 170     | 260     | 260      | 250      | 290      | 230      | 100      | 300     | 110      | 100      |
| BRIDGEPORT            | VEL (MPH) | 1.4     | 8.2     | 1.9      | 6.7      | 7.1      | 5.5      | 6.8      | 3.5     | 5.4      | 1.3      |
|                       | SPD (MPH) | 4.6     | 8.3     | 3.9      | 6.9      | 8.1      | 5.6      | 6.9      | 5.8     | 5.5      | 2.7      |
|                       | RATIO     | 0.306   | 0.979   | 0.489    | 0.967    | 0.876    | 0.974    | 0.983    | 0.602   | 0.987    | 0.466    |
| METEOROLOGICAL SITE   | DIR (DEG) | 210     | 260     | 280      | 280      | 270      | 260      | 130      | 300     | 140      | 260      |
| WORCESTER             | VEL (MPH) | 5.0     | 9.3     | 5.9      | 6.6      | 8.9      | 6.3      | 1.8      | 4.0     | 3.6      | 3.4      |
|                       | SPD (MPH) | 5.8     | 9.3     | 6.2      | 7.0      | 10.4     | 6.8      | 2.0      | 4.2     | 3.6      | 4.3      |
|                       | RATIO     | 0.864   | 0.997   | 0.960    | 0.932    | 0.858    | 0.934    | 0.889    | 0.957   | 0.992    | 0.794    |
| BRIDGEPORT-013 (0058) |           |         |         |          |          |          |          |          |         |          |          |
| PM10                  |           | 79      | 49      | 47       | 46       | 46       | 45       | 43       | 39      | 39       | 38       |
| DATE                  |           | 1/17/90 | 7/ 4/90 | 11/ 1/90 | 12/13/90 | 9/ 2/90  | 6/22/90  | 8/27/90  | 7/22/90 | 6/28/90  | 1/23/90  |
| METEOROLOGICAL SITE   | DIR (DEG) | 190     | 230     | 200      | 280      | 280      | 200      | 340      | 110     | 260      | 270      |
| NEWARK                | VEL (MPH) | 5.8     | 14.0    | 2.7      | 9.0      | 4.8      | 6.4      | 5.0      | 2.4     | 2.4      | 4.8      |
|                       | SPD (MPH) | 6.3     | 16.2    | 5.5      | 11.9     | 7.2      | 8.3      | 7.2      | 5.0     | 5.2      | 8.9      |
|                       | RATIO     | 0.912   | 0.861   | 0.501    | 0.750    | 0.670    | 0.773    | 0.694    | 0.486   | 0.464    | 0.538    |
| METEOROLOGICAL SITE   | DIR (DEG) | 180     | 220     | 80       | 240      | 240      | 210      | 320      | 130     | 320      | 220      |
| BRADLEY               | VEL (MPH) | 6.2     | 8.0     | .6       | 1.4      | 1.4      | 6.9      | 4.8      | 3.0     | 6.9      | 2.4      |
|                       | SPD (MPH) | 8.1     | 10.2    | 3.3      | 9.3      | 4.9      | 8.5      | 6.6      | 6.5     | 7.5      | 4.5      |
|                       | RATIO     | 0.772   | 0.781   | 0.183    | 0.279    | 0.541    | 0.819    | 0.727    | 0.468   | 0.926    | 0.541    |

TABLE 2-5, CONTINUED

1990 TEN HIGHEST 24-HOUR AVERAGE PM10 DAYS WITH WIND DATA

| TOWN-SITE (SAMPLES)               | RANK      | UNITS : MICROGRAMS PER CUBIC METER |          |         |         |         |          |         |         |         |         |
|-----------------------------------|-----------|------------------------------------|----------|---------|---------|---------|----------|---------|---------|---------|---------|
|                                   |           | 1                                  | 2        | 3       | 4       | 5       | 6        | 7       | 8       | 9       | 10      |
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG) | 170                                | 260      | 260     | 290     | 250     | 230      | 300     | 110     | 260     | 280     |
|                                   | VEL (MPH) | 1.4                                | 8.2      | 1.9     | 7.1     | 6.7     | 5.5      | 3.5     | 5.4     | 5.2     | 3.6     |
|                                   | SPD (MPH) | 4.6                                | 8.3      | 3.9     | 8.1     | 6.9     | 5.6      | 5.8     | 5.5     | 5.9     | 6.0     |
|                                   | RATIO     | 0.306                              | 0.979    | 0.489   | 0.876   | 0.967   | 0.974    | 0.602   | 0.987   | 0.883   | 0.603   |
|                                   | DIR (DEG) | 210                                | 260      | 280     | 270     | 280     | 260      | 300     | 140     | 300     | 280     |
| METEOROLOGICAL SITE<br>WORCESTER  | VEL (MPH) | 5.0                                | 9.3      | 5.9     | 8.9     | 6.6     | 6.3      | 4.0     | 3.6     | 7.0     | 4.9     |
|                                   | SPD (MPH) | 5.8                                | 9.3      | 6.2     | 10.4    | 7.0     | 6.8      | 4.2     | 3.6     | 7.5     | 5.3     |
|                                   | RATIO     | 0.864                              | 0.997    | 0.960   | 0.858   | 0.932   | 0.934    | 0.957   | 0.992   | 0.934   | 0.922   |
|                                   | PM10      | 85                                 | 60       | 57      | 56      | 54      | 54       | 53      | 52      | 51      | 51      |
|                                   | DATE      | 1/17/90                            | 12/13/90 | 8/27/90 | 11/1/90 | 9/2/90  | 6/22/90  | 7/4/90  | 6/28/90 | 3/12/90 | 1/23/90 |
| METEOROLOGICAL SITE<br>NEWARK     | DIR (DEG) | 190                                | 280      | 340     | 200     | 280     | 200      | 230     | 260     | 90      | 270     |
|                                   | VEL (MPH) | 5.8                                | 9.0      | 5.0     | 2.7     | 4.8     | 6.4      | 14.0    | 2.4     | 3.5     | 4.8     |
|                                   | SPD (MPH) | 6.3                                | 11.9     | 7.2     | 5.5     | 7.2     | 8.3      | 16.2    | 5.2     | 4.7     | 8.9     |
|                                   | RATIO     | 0.912                              | 0.750    | 0.694   | 0.501   | 0.670   | 0.773    | 0.861   | 0.464   | 0.734   | 0.538   |
|                                   | DIR (DEG) | 180                                | 280      | 320     | 80      | 240     | 210      | 220     | 320     | 360     | 220     |
| METEOROLOGICAL SITE<br>BRADLEY    | VEL (MPH) | 6.2                                | 5.1      | 4.8     | 6       | 1.4     | 6.9      | 8.0     | 6.9     | 4.3     | 2.4     |
|                                   | SPD (MPH) | 8.1                                | 9.3      | 6.6     | 3.3     | 4.9     | 8.5      | 10.2    | 7.5     | 4.3     | 4.5     |
|                                   | RATIO     | 0.772                              | 0.541    | 0.727   | 0.183   | 0.279   | 0.819    | 0.781   | 0.926   | 0.992   | 0.541   |
|                                   | DIR (DEG) | 170                                | 290      | 300     | 260     | 250     | 230      | 260     | 260     | 100     | 280     |
|                                   | VEL (MPH) | 1.4                                | 7.1      | 3.5     | 1.9     | 6.7     | 5.5      | 8.2     | 5.2     | 6.8     | 3.6     |
| METEOROLOGICAL SITE<br>BRIDGEPORT | SPD (MPH) | 4.6                                | 8.1      | 5.8     | 3.9     | 6.9     | 5.6      | 8.3     | 5.9     | 6.9     | 6.0     |
|                                   | RATIO     | 0.306                              | 0.876    | 0.602   | 0.489   | 0.967   | 0.974    | 0.979   | 0.883   | 0.983   | 0.603   |
|                                   | DIR (DEG) | 210                                | 270      | 300     | 280     | 280     | 260      | 260     | 300     | 130     | 280     |
|                                   | VEL (MPH) | 5.0                                | 8.9      | 4.0     | 7.0     | 6.6     | 6.8      | 9.3     | 7.0     | 1.8     | 4.9     |
|                                   | SPD (MPH) | 5.8                                | 10.4     | 4.2     | 6.2     | 7.0     | 6.8      | 9.3     | 7.5     | 2.0     | 5.3     |
| RATIO                             | 0.864     | 0.858                              | 0.957    | 0.960   | 0.932   | 0.934   | 0.997    | 0.934   | 0.889   | 0.922   |         |
| BRISTOL-001 (0060)                | PM10      | 52                                 | 44       | 43      | 39      | 36      | 36       | 34      | 32      | 32      | 31      |
|                                   | DATE      | 1/17/90                            | 7/4/90   | 9/2/90  | 8/27/90 | 11/1/90 | 12/13/90 | 9/14/90 | 10/8/90 | 7/22/90 | 6/22/90 |
|                                   | DIR (DEG) | 190                                | 230      | 280     | 340     | 200     | 280      | 140     | 170     | 110     | 200     |
|                                   | VEL (MPH) | 5.8                                | 14.0     | 4.8     | 5.0     | 2.7     | 9.0      | 6.6     | 2.8     | 2.4     | 6.4     |
|                                   | SPD (MPH) | 6.3                                | 16.2     | 7.2     | 7.2     | 5.5     | 11.9     | 7.5     | 5.0     | 5.0     | 8.3     |
| METEOROLOGICAL SITE<br>BRADLEY    | RATIO     | 0.912                              | 0.861    | 0.670   | 0.694   | 0.501   | 0.750    | 0.881   | 0.560   | 0.486   | 0.773   |
|                                   | DIR (DEG) | 180                                | 220      | 240     | 320     | 80      | 280      | 160     | 190     | 130     | 210     |
|                                   | VEL (MPH) | 6.2                                | 8.0      | 1.4     | 4.8     | 6       | 5.1      | 5.5     | 4.9     | 3.0     | 6.9     |
|                                   | SPD (MPH) | 8.1                                | 10.2     | 4.9     | 6.6     | 3.3     | 9.3      | 8.1     | 7.0     | 6.5     | 8.5     |
|                                   | RATIO     | 0.772                              | 0.781    | 0.279   | 0.727   | 0.183   | 0.541    | 0.681   | 0.701   | 0.468   | 0.819   |
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG) | 170                                | 260      | 250     | 300     | 260     | 290      | 160     | 210     | 110     | 230     |
|                                   | VEL (MPH) | 1.4                                | 8.2      | 6.7     | 3.5     | 1.9     | 7.1      | 6.1     | 1.3     | 5.4     | 5.5     |
|                                   | SPD (MPH) | 4.6                                | 8.3      | 6.9     | 5.8     | 3.9     | 8.1      | 6.6     | 2.9     | 5.5     | 5.6     |
|                                   | RATIO     | 0.306                              | 0.979    | 0.967   | 0.602   | 0.489   | 0.876    | 0.922   | 0.460   | 0.987   | 0.974   |
|                                   | DIR (DEG) | 210                                | 280      | 280     | 300     | 280     | 270      | 170     | 240     | 140     | 260     |
| METEOROLOGICAL SITE<br>WORCESTER  | VEL (MPH) | 5.0                                | 9.3      | 6.6     | 4.0     | 5.9     | 8.9      | 4.3     | 2.5     | 3.6     | 6.3     |
|                                   | SPD (MPH) | 5.8                                | 9.3      | 7.0     | 4.2     | 6.2     | 10.4     | 4.3     | 5.5     | 3.6     | 6.8     |
|                                   | RATIO     | 0.864                              | 0.997    | 0.932   | 0.957   | 0.960   | 0.858    | 0.989   | 0.458   | 0.992   | 0.934   |

TABLE 2-5, CONTINUED

1990 TEN HIGHEST 24-HOUR AVERAGE PM10 DAYS WITH WIND DATA

UNITS : MICROGRAMS PER CUBIC METER

| TOWN-SITE (SAMPLES)          | RANK      | 1        | 2        | 3       | 4       | 5       | 6        | 7        | 8        | 9        | 10      |
|------------------------------|-----------|----------|----------|---------|---------|---------|----------|----------|----------|----------|---------|
| <b>BURLINGTON-001 (0059)</b> |           | 41       | 39       | 36      | 33      | 30      | 30       | 30       | 24       | 23       | 21      |
| METEOROLOGICAL SITE          | DATE      | 7/ 4/90  | 9/ 2/90  | 8/27/90 | 1/17/90 | 9/14/90 | 10/ 8/90 | 7/22/90  | 6/22/90  | 12/13/90 | 8/ 9/90 |
| NEWARK                       | DIR (DEG) | 230      | 280      | 340     | 190     | 140     | 170      | 110      | 200      | 280      | 20      |
|                              | VEL (MPH) | 14.0     | 4.8      | 5.0     | 5.8     | 6.6     | 2.8      | 2.4      | 6.4      | 9.0      | 5.8     |
|                              | SPD (MPH) | 16.2     | 7.2      | 7.2     | 6.3     | 7.5     | 5.0      | 5.0      | 8.3      | 11.9     | 7.8     |
|                              | RATIO     | 0.861    | 0.670    | 0.694   | 0.912   | 0.881   | 0.560    | 0.486    | 0.773    | 0.750    | 0.744   |
| METEOROLOGICAL SITE          | DIR (DEG) | 220      | 240      | 320     | 180     | 160     | 190      | 130      | 210      | 280      | 10      |
| BRADLEY                      | VEL (MPH) | 8.0      | 1.4      | 4.8     | 6.2     | 5.5     | 4.9      | 3.0      | 6.9      | 5.1      | 3.8     |
|                              | SPD (MPH) | 10.2     | 4.9      | 6.6     | 8.1     | 8.1     | 7.0      | 6.5      | 8.5      | 9.3      | 6.0     |
|                              | RATIO     | 0.781    | 0.279    | 0.727   | 0.772   | 0.681   | 0.701    | 0.468    | 0.819    | 0.541    | 0.637   |
| METEOROLOGICAL SITE          | DIR (DEG) | 260      | 250      | 300     | 170     | 160     | 210      | 110      | 230      | 290      | 50      |
| BRIDGEPORT                   | VEL (MPH) | 8.2      | 6.7      | 3.5     | 4.6     | 6.1     | 1.3      | 5.4      | 5.5      | 7.1      | 1.2     |
|                              | SPD (MPH) | 8.3      | 6.9      | 5.8     | 4.6     | 6.6     | 2.9      | 5.5      | 5.6      | 8.1      | 5.2     |
|                              | RATIO     | 0.979    | 0.967    | 0.602   | 0.366   | 0.922   | 0.460    | 0.987    | 0.974    | 0.876    | 0.230   |
| METEOROLOGICAL SITE          | DIR (DEG) | 260      | 280      | 300     | 210     | 170     | 240      | 140      | 260      | 270      | 80      |
| WORCESTER                    | VEL (MPH) | 9.3      | 6.6      | 4.0     | 5.0     | 4.3     | 2.5      | 3.6      | 6.3      | 8.9      | 2.8     |
|                              | SPD (MPH) | 9.3      | 7.0      | 4.2     | 5.8     | 4.3     | 5.5      | 3.6      | 6.8      | 10.4     | 4.6     |
|                              | RATIO     | 0.997    | 0.932    | 0.957   | 0.864   | 0.989   | 0.458    | 0.992    | 0.934    | 0.858    | 0.600   |
| <b>CORNWALL-005 (0058)</b>   |           | 50       | 47       | 43      | 40      | 38      | 36       | 27       | 26       | 26       | 25      |
| METEOROLOGICAL SITE          | DATE      | 10/ 8/90 | 2/22/90  | 9/ 2/90 | 7/ 4/90 | 8/27/90 | 1/17/90  | 11/ 1/90 | 7/16/90  | 9/14/90  | 7/22/90 |
| NEWARK                       | DIR (DEG) | 170      | 210      | 280     | 230     | 340     | 190      | 200      | 260      | 140      | 110     |
|                              | VEL (MPH) | 2.8      | 8.0      | 4.8     | 14.0    | 5.0     | 5.8      | 2.7      | 7.2      | 6.6      | 2.4     |
|                              | SPD (MPH) | 5.0      | 10.8     | 7.2     | 16.2    | 7.2     | 6.3      | 5.5      | 9.2      | 7.5      | 5.0     |
|                              | RATIO     | 0.560    | 0.738    | 0.670   | 0.861   | 0.694   | 0.912    | 0.501    | 0.788    | 0.881    | 0.486   |
| METEOROLOGICAL SITE          | DIR (DEG) | 190      | 190      | 240     | 220     | 320     | 180      | 80       | 280      | 160      | 130     |
| BRADLEY                      | VEL (MPH) | 4.9      | 10.0     | 1.4     | 8.0     | 4.8     | 6.2      | .6       | 6.6      | 5.5      | 3.0     |
|                              | SPD (MPH) | 7.0      | 13.8     | 4.9     | 10.2    | 6.6     | 8.1      | 3.3      | 9.9      | 8.1      | 6.5     |
|                              | RATIO     | 0.701    | 0.727    | 0.279   | 0.781   | 0.727   | 0.772    | 0.183    | 0.663    | 0.681    | 0.468   |
| METEOROLOGICAL SITE          | DIR (DEG) | 210      | 240      | 250     | 260     | 300     | 170      | 260      | 270      | 160      | 110     |
| BRIDGEPORT                   | VEL (MPH) | 1.3      | 8.1      | 6.7     | 8.2     | 3.5     | 1.4      | 1.9      | 7.7      | 6.1      | 5.4     |
|                              | SPD (MPH) | 2.9      | 8.2      | 6.9     | 8.3     | 5.8     | 4.6      | 3.9      | 8.1      | 6.6      | 5.5     |
|                              | RATIO     | 0.460    | 0.986    | 0.967   | 0.979   | 0.602   | 0.306    | 0.489    | 0.954    | 0.922    | 0.987   |
| METEOROLOGICAL SITE          | DIR (DEG) | 240      | 240      | 280     | 260     | 300     | 210      | 280      | 270      | 170      | 140     |
| WORCESTER                    | VEL (MPH) | 2.5      | 14.1     | 6.6     | 9.3     | 4.0     | 5.0      | 5.9      | 7.2      | 4.3      | 3.6     |
|                              | SPD (MPH) | 5.5      | 14.2     | 7.0     | 9.3     | 4.2     | 5.8      | 6.2      | 7.8      | 4.3      | 3.6     |
|                              | RATIO     | 0.458    | 0.991    | 0.932   | 0.997   | 0.957   | 0.864    | 0.960    | 0.929    | 0.989    | 0.992   |
| <b>DANBURY-123 (0060)</b>    |           | 59       | 44       | 44      | 43      | 39      | 38       | 38       | 37       | 37       | 34      |
| METEOROLOGICAL SITE          | DATE      | 1/17/90  | 11/ 1/90 | 7/ 4/90 | 8/27/90 | 7/22/90 | 1/ 5/90  | 9/ 2/90  | 10/ 8/90 | 12/13/90 | 6/28/90 |
| NEWARK                       | DIR (DEG) | 190      | 200      | 230     | 340     | 110     | 320      | 280      | 170      | 280      | 260     |
|                              | VEL (MPH) | 5.8      | 2.7      | 14.0    | 5.0     | 2.4     | 7.2      | 4.8      | 2.8      | 9.0      | 2.4     |
|                              | SPD (MPH) | 6.3      | 5.5      | 16.2    | 7.2     | 5.0     | 9.8      | 7.2      | 5.0      | 11.9     | 5.2     |
|                              | RATIO     | 0.912    | 0.501    | 0.861   | 0.694   | 0.486   | 0.733    | 0.670    | 0.560    | 0.750    | 0.464   |
| METEOROLOGICAL SITE          | DIR (DEG) | 180      | 80       | 220     | 320     | 130     | 320      | 240      | 190      | 280      | 320     |
| BRADLEY                      | VEL (MPH) | 6.2      | .6       | 8.0     | 6.8     | 3.0     | 8.1      | 1.4      | 4.9      | 5.1      | 6.9     |
|                              | SPD (MPH) | 8.1      | 3.3      | 10.2    | 6.6     | 6.5     | 8.8      | 4.9      | 7.0      | 9.3      | 7.5     |
|                              | RATIO     | 0.772    | 0.183    | 0.781   | 0.727   | 0.468   | 0.920    | 0.279    | 0.701    | 0.541    | 0.926   |

TABLE 2-5, CONTINUED

1990 TEN HIGHEST 24-HOUR AVERAGE PM10 DAYS WITH WIND DATA

UNITS : MICROGRAMS PER CUBIC METER

| TOWN-SITE (SAMPLES)               | RANK | 1         | 2         | 3         | 4         | 5         | 6         | 7         | 8         | 9         | 10        |
|-----------------------------------|------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| METEOROLOGICAL SITE<br>BRIDGEPORT |      | 170       | 260       | 260       | 300       | 110       | 300       | 250       | 210       | 290       | 260       |
|                                   |      | DIR (DEG) |
|                                   |      | 1.4       | 1.9       | 8.2       | 3.5       | 5.4       | 3.2       | 6.7       | 1.3       | 7.1       | 5.2       |
|                                   |      | VEL (MPH) |
|                                   |      | 4.6       | 3.9       | 8.3       | 5.8       | 5.5       | 4.0       | 6.9       | 2.9       | 8.1       | 5.9       |
|                                   |      | RATIO     |
|                                   |      | 0.306     | 0.489     | 0.979     | 0.602     | 0.987     | 0.785     | 0.967     | 0.460     | 0.876     | 0.883     |
| METEOROLOGICAL SITE<br>WORCESTER  |      | 210       | 280       | 260       | 300       | 140       | 290       | 280       | 240       | 270       | 300       |
|                                   |      | DIR (DEG) |
|                                   |      | 5.0       | 5.9       | 9.3       | 4.0       | 3.6       | 6.3       | 6.6       | 2.5       | 8.9       | 7.0       |
|                                   |      | VEL (MPH) |
|                                   |      | 5.8       | 6.2       | 9.3       | 4.2       | 3.6       | 6.6       | 7.0       | 5.5       | 10.4      | 7.5       |
|                                   |      | RATIO     |
|                                   |      | 0.864     | 0.960     | 0.997     | 0.957     | 0.992     | 0.954     | 0.932     | 0.458     | 0.858     | 0.934     |
| DARLEN-001 (0058)                 |      | 73        | 65        | 55        | 54        | 52        | 51        | 49        | 48        | 47        | 44        |
|                                   |      | PM10      |
|                                   |      | DATE      |
|                                   |      | 1/17/90   | 8/27/90   | 12/13/90  | 4/23/90   | 11/1/90   | 7/4/90    | 6/28/90   | 9/2/90    | 5/11/90   | 8/15/90   |
| METEOROLOGICAL SITE<br>NEWARK     |      | 190       | 340       | 280       | 360       | 200       | 230       | 260       | 280       | 280       | 270       |
|                                   |      | DIR (DEG) |
|                                   |      | 5.8       | 5.0       | 9.0       | 6.2       | 2.7       | 14.0      | 2.4       | 4.8       | 11.9      | 4.5       |
|                                   |      | VEL (MPH) |
|                                   |      | 6.3       | 7.2       | 11.9      | 7.9       | 5.5       | 16.2      | 5.2       | 7.2       | 16.2      | 7.6       |
|                                   |      | RATIO     |
|                                   |      | 0.912     | 0.694     | 0.750     | 0.786     | 0.501     | 0.861     | 0.464     | 0.670     | 0.734     | 0.590     |
| METEOROLOGICAL SITE<br>BRADLEY    |      | 180       | 320       | 280       | 10        | 80        | 220       | 320       | 240       | 280       | 290       |
|                                   |      | DIR (DEG) |
|                                   |      | 6.2       | 4.8       | 5.1       | 6.9       | .6        | 2.0       | 6.9       | 1.4       | 13.7      | 4.8       |
|                                   |      | VEL (MPH) |
|                                   |      | 8.1       | 6.6       | 9.3       | 8.8       | 3.3       | 10.2      | 7.5       | 4.9       | 15.4      | 5.6       |
|                                   |      | RATIO     |
|                                   |      | 0.772     | 0.727     | 0.541     | 0.784     | 0.183     | 0.781     | 0.926     | 0.279     | 0.888     | 0.863     |
| METEOROLOGICAL SITE<br>BRIDGEPORT |      | 170       | 300       | 290       | 10        | 260       | 260       | 260       | 250       | 280       | 250       |
|                                   |      | DIR (DEG) |
|                                   |      | 1.4       | 3.5       | 7.1       | 7.2       | 1.9       | 8.2       | 5.2       | 6.7       | 9.8       | 2.7       |
|                                   |      | VEL (MPH) |
|                                   |      | 4.6       | 5.8       | 8.1       | 8.1       | 3.9       | 8.3       | 5.9       | 6.9       | 10.5      | 4.0       |
|                                   |      | RATIO     |
|                                   |      | 0.306     | 0.602     | 0.876     | 0.890     | 0.489     | 0.979     | 0.883     | 0.967     | 0.932     | 0.664     |
| METEOROLOGICAL SITE<br>WORCESTER  |      | 210       | 300       | 270       | 360       | 280       | 260       | 300       | 280       | 280       | 280       |
|                                   |      | DIR (DEG) |
|                                   |      | 5.0       | 4.0       | 8.9       | 6.4       | 5.9       | 9.3       | 7.0       | 6.6       | 11.1      | 5.5       |
|                                   |      | VEL (MPH) |
|                                   |      | 5.8       | 4.2       | 10.4      | 8.2       | 6.2       | 9.3       | 7.5       | 7.0       | 11.4      | 5.8       |
|                                   |      | RATIO     |
|                                   |      | 0.864     | 0.957     | 0.858     | 0.785     | 0.960     | 0.997     | 0.934     | 0.932     | 0.980     | 0.958     |
| EAST HARTFORD-004 (0059)          |      | 68        | 50        | 43        | 41        | 40        | 36        | 35        | 35        | 35        | 34        |
|                                   |      | PM10      |
|                                   |      | DATE      |
|                                   |      | 1/17/90   | 11/1/90   | 7/4/90    | 8/27/90   | 9/2/90    | 7/22/90   | 1/23/90   | 12/7/90   | 2/16/90   | 6/22/90   |
| METEOROLOGICAL SITE<br>NEWARK     |      | 190       | 200       | 230       | 340       | 280       | 110       | 270       | 330       | 50        | 200       |
|                                   |      | DIR (DEG) |
|                                   |      | 5.8       | 2.7       | 14.0      | 5.0       | 4.8       | 2.4       | 4.8       | 1.7       | 3.1       | 6.4       |
|                                   |      | VEL (MPH) |
|                                   |      | 6.3       | 5.5       | 16.2      | 7.2       | 7.2       | 5.0       | 8.9       | 5.0       | 5.3       | 8.3       |
|                                   |      | RATIO     |
|                                   |      | 0.912     | 0.501     | 0.861     | 0.694     | 0.670     | 0.486     | 0.538     | 0.334     | 0.578     | 0.773     |
| METEOROLOGICAL SITE<br>BRADLEY    |      | 180       | 80        | 220       | 320       | 240       | 130       | 220       | 330       | 20        | 210       |
|                                   |      | DIR (DEG) |
|                                   |      | 6.2       | .6        | 8.0       | 4.8       | 1.4       | 3.0       | 2.4       | 1.6       | 1.2       | 6.9       |
|                                   |      | VEL (MPH) |
|                                   |      | 8.1       | 3.3       | 10.2      | 6.6       | 4.9       | 6.5       | 4.5       | 4.3       | 3.2       | 8.5       |
|                                   |      | RATIO     |
|                                   |      | 0.772     | 0.183     | 0.781     | 0.727     | 0.279     | 0.468     | 0.541     | 0.375     | 0.377     | 0.819     |
| METEOROLOGICAL SITE<br>BRIDGEPORT |      | 170       | 280       | 260       | 300       | 250       | 110       | 280       | 100       | 140       | 230       |
|                                   |      | DIR (DEG) |
|                                   |      | 1.4       | 1.9       | 8.2       | 3.5       | 6.7       | 5.4       | 3.6       | 1.3       | 1.0       | 5.5       |
|                                   |      | VEL (MPH) |
|                                   |      | 4.6       | 3.9       | 8.3       | 5.8       | 6.9       | 5.5       | 6.0       | 2.7       | 2.7       | 5.6       |
|                                   |      | RATIO     |
|                                   |      | 0.306     | 0.489     | 0.979     | 0.602     | 0.967     | 0.987     | 0.603     | 0.466     | 0.383     | 0.974     |
| METEOROLOGICAL SITE<br>WORCESTER  |      | 210       | 280       | 260       | 300       | 280       | 140       | 280       | 260       | 10        | 260       |
|                                   |      | DIR (DEG) |
|                                   |      | 5.0       | 5.9       | 9.3       | 4.0       | 6.6       | 3.6       | 4.9       | 3.4       | 1.9       | 6.3       |
|                                   |      | VEL (MPH) |
|                                   |      | 5.8       | 6.2       | 9.3       | 4.2       | 7.0       | 3.6       | 5.3       | 4.3       | 2.4       | 6.8       |
|                                   |      | RATIO     |
|                                   |      | 0.864     | 0.960     | 0.997     | 0.957     | 0.932     | 0.992     | 0.922     | 0.794     | 0.779     | 0.934     |

TABLE 2-5. CONTINUED

1990 TEN HIGHEST 24-HOUR AVERAGE PM10 DAYS WITH WIND DATA

UNITS : MICROGRAMS PER CUBIC METER

| TOWN-SITE (SAMPLES)  | RANK      | 1       | 2       | 3       | 4        | 5       | 6       | 7        | 8       | 9       | 10      |
|----------------------|-----------|---------|---------|---------|----------|---------|---------|----------|---------|---------|---------|
| ENFIELD-005 (0058)   | PM10      | 46      | 43      | 37      | 30       | 29      | 28      | 27       | 26      | 25      | 25      |
|                      | DATE      | 1/17/90 | 7/4/90  | 7/22/90 | 8/27/90  | 6/22/90 | 10/8/90 | 12/13/90 | 7/16/90 | 8/9/90  | 11/1/90 |
| METEOROLOGICAL SITE  | DIR (DEG) | 190     | 230     | 110     | 340      | 200     | 170     | 280      | 260     | 20      | 200     |
| NEWARK               | VEL (MPH) | 5.8     | 14.0    | 2.4     | 5.0      | 6.4     | 2.8     | 9.0      | 7.2     | 5.8     | 2.7     |
|                      | SPD (MPH) | 6.3     | 16.2    | 5.0     | 7.2      | 8.3     | 5.0     | 11.9     | 9.2     | 7.8     | 5.5     |
|                      | RATIO     | 0.912   | 0.861   | 0.486   | 0.694    | 0.773   | 0.560   | 0.750    | 0.788   | 0.744   | 0.501   |
| METEOROLOGICAL SITE  | DIR (DEG) | 180     | 220     | 130     | 320      | 210     | 190     | 280      | 280     | 10      | 80      |
| BRADLEY              | VEL (MPH) | 6.2     | 8.0     | 3.0     | 4.8      | 6.9     | 4.9     | 5.1      | 6.6     | 3.8     | 6       |
|                      | SPD (MPH) | 8.1     | 10.2    | 6.5     | 6.6      | 8.5     | 7.0     | 9.3      | 9.9     | 6.0     | 3.3     |
|                      | RATIO     | 0.772   | 0.781   | 0.468   | 0.727    | 0.819   | 0.701   | 0.541    | 0.663   | 0.637   | 0.183   |
| METEOROLOGICAL SITE  | DIR (DEG) | 170     | 260     | 110     | 300      | 230     | 210     | 290      | 270     | 50      | 260     |
| BRIDGEPORT           | VEL (MPH) | 1.4     | 8.2     | 5.4     | 3.5      | 5.5     | 1.3     | 7.1      | 7.7     | 1.2     | 1.9     |
|                      | SPD (MPH) | 4.6     | 8.3     | 5.5     | 5.8      | 5.6     | 2.9     | 8.1      | 8.1     | 5.2     | 3.9     |
|                      | RATIO     | 0.306   | 0.979   | 0.987   | 0.602    | 0.974   | 0.460   | 0.876    | 0.954   | 0.230   | 0.489   |
| METEOROLOGICAL SITE  | DIR (DEG) | 210     | 260     | 140     | 300      | 260     | 240     | 270      | 270     | 80      | 280     |
| WORCESTER            | VEL (MPH) | 5.0     | 9.3     | 3.6     | 4.0      | 6.3     | 2.5     | 8.9      | 7.2     | 2.8     | 5.9     |
|                      | SPD (MPH) | 5.8     | 9.3     | 3.6     | 4.2      | 6.8     | 5.5     | 10.4     | 7.8     | 4.6     | 6.2     |
|                      | RATIO     | 0.864   | 0.997   | 0.992   | 0.957    | 0.934   | 0.458   | 0.858    | 0.929   | 0.600   | 0.960   |
| GREENWICH-017 (0057) | PM10      | 62      | 53      | 48      | 42       | 39      | 37      | 35       | 34      | 32      | 32      |
|                      | DATE      | 1/17/90 | 7/4/90  | 9/2/90  | 12/13/90 | 6/28/90 | 6/22/90 | 7/22/90  | 8/27/90 | 7/16/90 | 10/8/90 |
| METEOROLOGICAL SITE  | DIR (DEG) | 190     | 230     | 280     | 280      | 260     | 200     | 110      | 340     | 260     | 170     |
| NEWARK               | VEL (MPH) | 5.8     | 14.0    | 4.8     | 9.0      | 2.4     | 6.4     | 2.4      | 5.0     | 7.2     | 2.8     |
|                      | SPD (MPH) | 6.3     | 16.2    | 7.2     | 11.9     | 5.2     | 8.3     | 5.0      | 7.2     | 9.2     | 5.0     |
|                      | RATIO     | 0.912   | 0.861   | 0.670   | 0.750    | 0.464   | 0.773   | 0.486    | 0.694   | 0.788   | 0.560   |
| METEOROLOGICAL SITE  | DIR (DEG) | 180     | 220     | 240     | 280      | 320     | 210     | 130      | 320     | 280     | 190     |
| BRADLEY              | VEL (MPH) | 6.2     | 8.0     | 1.4     | 5.1      | 6.9     | 6.9     | 3.0      | 4.8     | 6.6     | 4.9     |
|                      | SPD (MPH) | 8.1     | 10.2    | 4.9     | 9.3      | 7.5     | 8.5     | 6.5      | 6.6     | 9.9     | 7.0     |
|                      | RATIO     | 0.772   | 0.781   | 0.279   | 0.541    | 0.926   | 0.819   | 0.468    | 0.727   | 0.663   | 0.701   |
| METEOROLOGICAL SITE  | DIR (DEG) | 170     | 260     | 250     | 290      | 260     | 230     | 110      | 300     | 270     | 210     |
| BRIDGEPORT           | VEL (MPH) | 1.4     | 8.2     | 6.7     | 7.1      | 5.2     | 5.5     | 5.4      | 3.5     | 7.7     | 1.3     |
|                      | SPD (MPH) | 4.6     | 8.3     | 6.9     | 8.1      | 5.9     | 5.6     | 5.5      | 5.8     | 8.1     | 2.9     |
|                      | RATIO     | 0.306   | 0.979   | 0.967   | 0.876    | 0.883   | 0.974   | 0.987    | 0.602   | 0.954   | 0.460   |
| METEOROLOGICAL SITE  | DIR (DEG) | 210     | 260     | 280     | 270      | 300     | 260     | 140      | 300     | 270     | 240     |
| WORCESTER            | VEL (MPH) | 5.0     | 9.3     | 6.6     | 8.9      | 7.0     | 6.3     | 3.6      | 4.0     | 7.2     | 2.5     |
|                      | SPD (MPH) | 5.8     | 9.3     | 7.0     | 10.4     | 7.5     | 6.8     | 3.6      | 4.2     | 7.8     | 5.5     |
|                      | RATIO     | 0.864   | 0.997   | 0.932   | 0.858    | 0.934   | 0.934   | 0.992    | 0.957   | 0.929   | 0.458   |
| GROTON-006 (0056)    | PM10      | 54      | 48      | 40      | 39       | 39      | 38      | 30       | 29      | 28      | 27      |
|                      | DATE      | 7/4/90  | 1/17/90 | 9/2/90  | 6/22/90  | 7/16/90 | 8/27/90 | 6/28/90  | 8/15/90 | 8/3/90  | 4/23/90 |
| METEOROLOGICAL SITE  | DIR (DEG) | 230     | 190     | 280     | 200      | 260     | 340     | 260      | 270     | 170     | 360     |
| NEWARK               | VEL (MPH) | 14.0    | 5.8     | 4.8     | 6.4      | 7.2     | 5.0     | 2.4      | 4.5     | 1.0     | 6.2     |
|                      | SPD (MPH) | 16.2    | 6.3     | 7.2     | 8.3      | 9.2     | 7.2     | 5.2      | 7.6     | 4.2     | 7.9     |
|                      | RATIO     | 0.861   | 0.912   | 0.670   | 0.773    | 0.788   | 0.694   | 0.464    | 0.590   | 0.233   | 0.786   |
| METEOROLOGICAL SITE  | DIR (DEG) | 220     | 180     | 240     | 210      | 280     | 320     | 320      | 290     | 290     | 10      |
| BRADLEY              | VEL (MPH) | 8.0     | 6.2     | 1.4     | 6.9      | 6.6     | 4.8     | 6.9      | 4.8     | 2.5     | 6.9     |
|                      | SPD (MPH) | 10.2    | 8.1     | 4.9     | 8.5      | 9.9     | 6.6     | 7.5      | 5.6     | 5.0     | 8.8     |
|                      | RATIO     | 0.781   | 0.772   | 0.279   | 0.819    | 0.663   | 0.727   | 0.926    | 0.863   | 0.492   | 0.784   |

TABLE 2-5, CONTINUED

1990 TEN HIGHEST 24-HOUR AVERAGE PM10 DAYS WITH WIND DATA

UNITS : MICROGRAMS PER CUBIC METER

| TOWN-SITE (SAMPLES)               | RANK         | 1             | 2             | 3            | 4            | 5             | 6             | 7             | 8             | 9             | 10             |
|-----------------------------------|--------------|---------------|---------------|--------------|--------------|---------------|---------------|---------------|---------------|---------------|----------------|
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG)    | 260           | 170           | 250          | 230          | 270           | 300           | 260           | 250           | 240           | 10             |
|                                   | VEL (MPH)    | 8.2           | 1.4           | 6.7          | 5.5          | 7.7           | 3.5           | 5.2           | 2.7           | 5.0           | 7.2            |
|                                   | SPD (MPH)    | 8.3           | 4.6           | 6.9          | 5.6          | 8.1           | 5.8           | 5.9           | 4.0           | 5.0           | 8.1            |
|                                   | RATIO        | 0.979         | 0.306         | 0.967        | 0.974        | 0.954         | 0.602         | 0.883         | 0.664         | 0.996         | 0.890          |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG)    | 260           | 210           | 280          | 260          | 270           | 300           | 300           | 280           | 300           | 360            |
|                                   | VEL (MPH)    | 9.3           | 5.0           | 6.6          | 6.3          | 7.2           | 4.0           | 7.0           | 5.5           | 5.6           | 6.4            |
|                                   | SPD (MPH)    | 9.3           | 5.8           | 7.0          | 6.8          | 7.8           | 4.2           | 7.5           | 5.8           | 5.9           | 8.2            |
|                                   | RATIO        | 0.997         | 0.864         | 0.932        | 0.934        | 0.929         | 0.957         | 0.934         | 0.958         | 0.944         | 0.785          |
| HARTFORD-013 (0059)               | PM10<br>DATE | 59<br>1/17/90 | 48<br>11/1/90 | 41<br>9/2/90 | 40<br>7/4/90 | 36<br>12/7/90 | 36<br>8/27/90 | 33<br>7/22/90 | 32<br>9/14/90 | 30<br>6/22/90 | 29<br>8/9/90   |
| METEOROLOGICAL SITE<br>NEWARK     | DIR (DEG)    | 190           | 200           | 280          | 230          | 330           | 340           | 110           | 140           | 200           | 20             |
|                                   | VEL (MPH)    | 5.8           | 2.7           | 4.8          | 14.0         | 1.7           | 5.0           | 2.4           | 6.6           | 6.4           | 5.8            |
|                                   | SPD (MPH)    | 6.3           | 5.5           | 7.2          | 16.2         | 5.0           | 7.2           | 5.0           | 7.5           | 8.3           | 7.8            |
|                                   | RATIO        | 0.912         | 0.501         | 0.670        | 0.861        | 0.334         | 0.694         | 0.486         | 0.881         | 0.773         | 0.744          |
| METEOROLOGICAL SITE<br>BRADLEY    | DIR (DEG)    | 180           | 80            | 240          | 220          | 330           | 320           | 130           | 160           | 210           | 10             |
|                                   | VEL (MPH)    | 6.2           | .6            | 1.4          | 8.0          | 1.6           | 4.8           | 3.0           | 5.5           | 6.9           | 3.8            |
|                                   | SPD (MPH)    | 8.1           | 3.3           | 4.9          | 10.2         | 4.3           | 6.6           | 6.5           | 8.1           | 8.5           | 6.0            |
|                                   | RATIO        | 0.772         | 0.183         | 0.279        | 0.781        | 0.375         | 0.727         | 0.468         | 0.681         | 0.819         | 0.637          |
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG)    | 170           | 260           | 250          | 260          | 100           | 300           | 110           | 160           | 230           | 50             |
|                                   | VEL (MPH)    | 1.4           | 1.9           | 6.7          | 8.2          | 1.3           | 3.5           | 5.4           | 6.1           | 5.5           | 1.2            |
|                                   | SPD (MPH)    | 4.6           | 3.9           | 6.9          | 8.3          | 2.7           | 5.8           | 5.5           | 6.6           | 5.6           | 5.2            |
|                                   | RATIO        | 0.306         | 0.489         | 0.967        | 0.979        | 0.466         | 0.602         | 0.987         | 0.922         | 0.974         | 0.230          |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG)    | 210           | 280           | 280          | 260          | 260           | 300           | 140           | 170           | 260           | 80             |
|                                   | VEL (MPH)    | 5.0           | 5.9           | 6.6          | 9.3          | 3.4           | 4.0           | 3.6           | 4.3           | 6.3           | 2.8            |
|                                   | SPD (MPH)    | 5.8           | 6.2           | 7.0          | 9.3          | 4.3           | 4.2           | 3.6           | 4.3           | 6.8           | 4.6            |
|                                   | RATIO        | 0.864         | 0.960         | 0.932        | 0.997        | 0.794         | 0.957         | 0.992         | 0.989         | 0.934         | 0.600          |
| HARTFORD-014 (0055)               | PM10<br>DATE | 65<br>1/17/90 | 51<br>11/1/90 | 42<br>7/4/90 | 41<br>9/2/90 | 38<br>8/27/90 | 36<br>7/22/90 | 34<br>12/7/90 | 32<br>2/16/90 | 32<br>9/14/90 | 31<br>12/13/90 |
| METEOROLOGICAL SITE<br>NEWARK     | DIR (DEG)    | 190           | 200           | 230          | 280          | 340           | 110           | 330           | 50            | 140           | 280            |
|                                   | VEL (MPH)    | 5.8           | 2.7           | 14.0         | 4.8          | 5.0           | 2.4           | 1.7           | 3.1           | 6.6           | 9.0            |
|                                   | SPD (MPH)    | 6.3           | 5.5           | 16.2         | 7.2          | 7.2           | 5.0           | 5.0           | 5.3           | 7.5           | 11.9           |
|                                   | RATIO        | 0.912         | 0.501         | 0.861        | 0.670        | 0.694         | 0.486         | 0.334         | 0.578         | 0.881         | 0.750          |
| METEOROLOGICAL SITE<br>BRADLEY    | DIR (DEG)    | 180           | 80            | 220          | 240          | 320           | 130           | 330           | 20            | 160           | 280            |
|                                   | VEL (MPH)    | 6.2           | .6            | 8.0          | 1.4          | 4.8           | 3.0           | 1.6           | 1.2           | 5.5           | 5.1            |
|                                   | SPD (MPH)    | 8.1           | 3.3           | 10.2         | 4.9          | 6.6           | 6.5           | 4.3           | 3.2           | 8.1           | 9.3            |
|                                   | RATIO        | 0.772         | 0.183         | 0.781        | 0.279        | 0.727         | 0.468         | 0.375         | 0.377         | 0.681         | 0.541          |
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG)    | 170           | 260           | 260          | 250          | 300           | 110           | 100           | 140           | 160           | 290            |
|                                   | VEL (MPH)    | 1.4           | 1.9           | 8.2          | 6.7          | 3.5           | 5.4           | 1.3           | 1.0           | 6.1           | 7.1            |
|                                   | SPD (MPH)    | 4.6           | 3.9           | 8.3          | 6.9          | 5.8           | 5.5           | 2.7           | 2.7           | 6.6           | 8.1            |
|                                   | RATIO        | 0.306         | 0.489         | 0.979        | 0.967        | 0.602         | 0.987         | 0.466         | 0.383         | 0.922         | 0.876          |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG)    | 210           | 280           | 260          | 280          | 300           | 140           | 260           | 10            | 170           | 270            |
|                                   | VEL (MPH)    | 5.0           | 5.9           | 9.3          | 6.6          | 4.0           | 3.6           | 3.4           | 1.9           | 4.3           | 8.9            |
|                                   | SPD (MPH)    | 5.8           | 6.2           | 9.3          | 7.0          | 4.2           | 3.6           | 3.6           | 2.4           | 4.3           | 10.4           |
|                                   | RATIO        | 0.864         | 0.960         | 0.997        | 0.932        | 0.957         | 0.992         | 0.794         | 0.779         | 0.989         | 0.858          |

TABLE 2-5, CONTINUED

1990 TEN HIGHEST 24-HOUR AVERAGE PM10 DAYS WITH WIND DATA

UNITS : MICROGRAMS PER CUBIC METER

| TOWN-SITE (SAMPLES)          | RANK      | 1       | 2       | 3       | 4       | 5       | 6       | 7       | 8       | 9       | 10       |
|------------------------------|-----------|---------|---------|---------|---------|---------|---------|---------|---------|---------|----------|
| <b>HARTFORD-015 (0058)</b>   |           |         |         |         |         |         |         |         |         |         |          |
| METEOROLOGICAL SITE          | PM10      | 61      | 61      | 46      | 46      | 45      | 41      | 41      | 37      | 36      | 35       |
| NEWARK                       | DATE      | 1/17/90 | 11/1/90 | 12/7/90 | 8/27/90 | 2/16/90 | 3/12/90 | 9/2/90  | 8/9/90  | 9/14/90 | 3/6/90   |
|                              | DIR (DEG) | 190     | 200     | 330     | 340     | 50      | 90      | 280     | 20      | 140     | 10       |
|                              | VEL (MPH) | 5.8     | 2.7     | 1.7     | 5.0     | 3.1     | 3.5     | 4.8     | 5.8     | 6.6     | 11.3     |
|                              | SPD (MPH) | 6.3     | 5.5     | 5.0     | 7.2     | 5.3     | 4.7     | 7.2     | 7.8     | 7.5     | 11.5     |
|                              | RATIO     | 0.912   | 0.501   | 0.334   | 0.694   | 0.578   | 0.734   | 0.670   | 0.744   | 0.881   | 0.987    |
| METEOROLOGICAL SITE          | DIR (DEG) | 180     | 80      | 330     | 320     | 20      | 360     | 240     | 10      | 160     | 10       |
| BRADLEY                      | VEL (MPH) | 6.2     | .6      | 1.6     | 4.8     | 1.2     | 4.3     | 1.4     | 3.8     | 5.5     | 8.2      |
|                              | SPD (MPH) | 8.1     | 3.3     | 4.3     | 6.6     | 3.2     | 4.3     | 4.9     | 6.0     | 8.1     | 8.3      |
|                              | RATIO     | 0.772   | 0.183   | 0.375   | 0.727   | 0.377   | 0.992   | 0.279   | 0.637   | 0.681   | 0.979    |
| METEOROLOGICAL SITE          | DIR (DEG) | 170     | 260     | 100     | 300     | 140     | 100     | 250     | 50      | 160     | 30       |
| BRIDGEPORT                   | VEL (MPH) | 1.4     | 1.9     | 1.3     | 3.5     | 1.0     | 6.8     | 6.7     | 1.2     | 6.1     | 9.8      |
|                              | SPD (MPH) | 4.6     | 3.9     | 2.7     | 5.8     | 2.7     | 6.9     | 6.9     | 5.2     | 6.6     | 9.9      |
|                              | RATIO     | 0.306   | 0.489   | 0.466   | 0.602   | 0.383   | 0.983   | 0.967   | 0.230   | 0.922   | 0.993    |
| METEOROLOGICAL SITE          | DIR (DEG) | 210     | 280     | 260     | 300     | 10      | 130     | 280     | 80      | 170     | 50       |
| WORCESTER                    | VEL (MPH) | 5.0     | 5.9     | 3.4     | 4.0     | 1.9     | 1.8     | 6.6     | 2.8     | 4.3     | 3.7      |
|                              | SPD (MPH) | 5.8     | 6.2     | 4.3     | 4.2     | 2.4     | 2.0     | 7.0     | 4.6     | 4.3     | 3.7      |
|                              | RATIO     | 0.864   | 0.960   | 0.794   | 0.957   | 0.779   | 0.889   | 0.932   | 0.600   | 0.989   | 0.992    |
| <b>HARTFORD-018 (0060)</b>   |           |         |         |         |         |         |         |         |         |         |          |
| METEOROLOGICAL SITE          | PM10      | 76      | 56      | 44      | 43      | 41      | 40      | 40      | 36      | 36      | 35       |
| NEWARK                       | DATE      | 1/17/90 | 11/1/90 | 7/4/90  | 8/27/90 | 9/2/90  | 12/7/90 | 2/16/90 | 9/14/90 | 7/22/90 | 3/12/90  |
|                              | DIR (DEG) | 190     | 200     | 230     | 340     | 280     | 330     | 50      | 140     | 110     | 90       |
|                              | VEL (MPH) | 5.8     | 2.7     | 14.0    | 5.0     | 4.8     | 1.7     | 3.1     | 6.6     | 2.4     | 3.5      |
|                              | SPD (MPH) | 6.3     | 5.5     | 16.2    | 7.2     | 7.2     | 5.0     | 5.3     | 7.5     | 5.0     | 4.7      |
|                              | RATIO     | 0.912   | 0.501   | 0.861   | 0.694   | 0.670   | 0.334   | 0.578   | 0.881   | 0.486   | 0.734    |
| METEOROLOGICAL SITE          | DIR (DEG) | 180     | 80      | 220     | 320     | 240     | 330     | 20      | 160     | 130     | 360      |
| BRADLEY                      | VEL (MPH) | 6.2     | .6      | 8.0     | 4.8     | 1.4     | 1.6     | 1.2     | 5.5     | 3.0     | 4.3      |
|                              | SPD (MPH) | 8.1     | 3.3     | 10.2    | 6.6     | 4.9     | 4.3     | 3.2     | 8.1     | 6.5     | 4.3      |
|                              | RATIO     | 0.772   | 0.183   | 0.781   | 0.727   | 0.279   | 0.375   | 0.377   | 0.681   | 0.468   | 0.992    |
| METEOROLOGICAL SITE          | DIR (DEG) | 170     | 260     | 260     | 300     | 250     | 100     | 140     | 160     | 110     | 100      |
| BRIDGEPORT                   | VEL (MPH) | 1.4     | 1.9     | 8.2     | 3.5     | 6.7     | 1.3     | 1.0     | 6.1     | 5.4     | 6.8      |
|                              | SPD (MPH) | 4.6     | 3.9     | 8.3     | 5.8     | 6.9     | 2.7     | 2.7     | 6.6     | 5.5     | 6.9      |
|                              | RATIO     | 0.306   | 0.489   | 0.979   | 0.602   | 0.967   | 0.466   | 0.383   | 0.922   | 0.987   | 0.983    |
| METEOROLOGICAL SITE          | DIR (DEG) | 210     | 280     | 260     | 300     | 280     | 260     | 10      | 170     | 140     | 130      |
| WORCESTER                    | VEL (MPH) | 5.0     | 5.9     | 9.3     | 4.0     | 6.6     | 3.4     | 1.9     | 4.3     | 3.6     | 1.8      |
|                              | SPD (MPH) | 5.8     | 6.2     | 9.3     | 4.2     | 7.0     | 4.3     | 2.4     | 4.3     | 3.6     | 2.0      |
|                              | RATIO     | 0.864   | 0.960   | 0.997   | 0.957   | 0.932   | 0.794   | 0.779   | 0.989   | 0.992   | 0.889    |
| <b>MANCHESTER-001 (0055)</b> |           |         |         |         |         |         |         |         |         |         |          |
| METEOROLOGICAL SITE          | PM10      | 48      | 47      | 43      | 41      | 37      | 35      | 32      | 29      | 28      | 27       |
| NEWARK                       | DATE      | 1/17/90 | 8/27/90 | 7/4/90  | 9/2/90  | 7/22/90 | 11/1/90 | 9/14/90 | 12/7/90 | 6/22/90 | 12/13/90 |
|                              | DIR (DEG) | 190     | 340     | 230     | 280     | 110     | 200     | 140     | 330     | 200     | 280      |
|                              | VEL (MPH) | 5.8     | 5.0     | 14.0    | 4.8     | 2.4     | 5.5     | 6.6     | 1.7     | 6.4     | 9.0      |
|                              | SPD (MPH) | 6.3     | 7.2     | 16.2    | 7.2     | 5.0     | 7.2     | 7.5     | 5.0     | 8.3     | 11.9     |
|                              | RATIO     | 0.912   | 0.694   | 0.861   | 0.670   | 0.486   | 0.501   | 0.881   | 0.334   | 0.773   | 0.750    |
| METEOROLOGICAL SITE          | DIR (DEG) | 180     | 320     | 220     | 240     | 130     | 80      | 160     | 330     | 210     | 280      |
| BRADLEY                      | VEL (MPH) | 6.2     | 4.8     | 8.0     | 1.4     | 3.0     | .6      | 5.5     | 1.6     | 6.9     | 5.1      |
|                              | SPD (MPH) | 8.1     | 6.6     | 10.2    | 4.9     | 6.5     | 3.3     | 8.1     | 4.3     | 8.5     | 9.3      |
|                              | RATIO     | 0.772   | 0.727   | 0.781   | 0.279   | 0.468   | 0.183   | 0.681   | 0.375   | 0.819   | 0.541    |

TABLE 2-5, CONTINUED

1990 TEN HIGHEST 24-HOUR AVERAGE PM10 DAYS WITH WIND DATA

UNITS : MICROGRAMS PER CUBIC METER

| TOWN-SITE (SAMPLES)               | RANK         | 1             | 2             | 3             | 4              | 5             | 6              | 7             | 8             | 9             | 10             |
|-----------------------------------|--------------|---------------|---------------|---------------|----------------|---------------|----------------|---------------|---------------|---------------|----------------|
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG)    | 170           | 300           | 260           | 250            | 110           | 260            | 160           | 100           | 230           | 290            |
|                                   | VEL (MPH)    | 1.4           | 3.5           | 8.2           | 6.7            | 5.4           | 1.9            | 6.1           | 1.3           | 5.5           | 7.1            |
|                                   | SPD (MPH)    | 4.6           | 5.8           | 8.3           | 6.9            | 5.5           | 3.9            | 6.6           | 2.7           | 5.6           | 8.1            |
|                                   | RATIO        | 0.306         | 0.602         | 0.979         | 0.967          | 0.987         | 0.489          | 0.922         | 0.466         | 0.974         | 0.876          |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG)    | 210           | 300           | 260           | 280            | 140           | 280            | 170           | 260           | 260           | 270            |
|                                   | VEL (MPH)    | 5.0           | 4.0           | 9.3           | 6.6            | 3.6           | 5.9            | 4.3           | 3.4           | 6.3           | 8.9            |
|                                   | SPD (MPH)    | 5.8           | 4.2           | 9.3           | 7.0            | 3.6           | 6.2            | 4.3           | 4.3           | 6.8           | 10.4           |
|                                   | RATIO        | 0.864         | 0.957         | 0.997         | 0.932          | 0.992         | 0.960          | 0.989         | 0.794         | 0.934         | 0.858          |
| MIDDLETOWN-003 (0058)             | PM10<br>DATE | 48<br>1/17/90 | 44<br>7/ 4/90 | 43<br>9/ 2/90 | 39<br>8/27/90  | 37<br>1/ 5/90 | 37<br>7/22/90  | 37<br>6/28/90 | 33<br>6/22/90 | 30<br>2/16/90 | 30<br>12/ 7/90 |
| METEOROLOGICAL SITE<br>NEWARK     | DIR (DEG)    | 190           | 230           | 280           | 340            | 320           | 110            | 260           | 200           | 50            | 330            |
|                                   | VEL (MPH)    | 5.8           | 14.0          | 4.8           | 5.0            | 7.2           | 2.4            | 2.4           | 6.4           | 3.1           | 1.7            |
|                                   | SPD (MPH)    | 6.3           | 16.2          | 7.2           | 7.2            | 9.8           | 5.0            | 5.2           | 8.3           | 5.3           | 5.0            |
|                                   | RATIO        | 0.912         | 0.861         | 0.670         | 0.694          | 0.733         | 0.486          | 0.464         | 0.773         | 0.578         | 0.334          |
| METEOROLOGICAL SITE<br>BRADLEY    | DIR (DEG)    | 180           | 220           | 240           | 320            | 320           | 130            | 210           | 210           | 20            | 330            |
|                                   | VEL (MPH)    | 6.2           | 8.0           | 1.4           | 4.8            | 8.1           | 3.0            | 6.9           | 6.9           | 1.2           | 1.6            |
|                                   | SPD (MPH)    | 8.1           | 10.2          | 4.9           | 6.6            | 8.8           | 6.5            | 7.5           | 8.5           | 3.2           | 4.3            |
|                                   | RATIO        | 0.772         | 0.781         | 0.279         | 0.727          | 0.920         | 0.468          | 0.926         | 0.819         | 0.377         | 0.375          |
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG)    | 170           | 260           | 250           | 300            | 300           | 110            | 260           | 230           | 140           | 100            |
|                                   | VEL (MPH)    | 1.4           | 8.2           | 6.7           | 3.5            | 3.2           | 5.4            | 5.2           | 5.5           | 1.0           | 1.3            |
|                                   | SPD (MPH)    | 4.6           | 8.3           | 6.9           | 5.8            | 4.0           | 5.5            | 5.9           | 5.6           | 2.7           | 2.7            |
|                                   | RATIO        | 0.306         | 0.979         | 0.967         | 0.602          | 0.785         | 0.987          | 0.883         | 0.974         | 0.383         | 0.466          |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG)    | 210           | 260           | 280           | 300            | 290           | 140            | 260           | 260           | 10            | 260            |
|                                   | VEL (MPH)    | 5.0           | 9.3           | 6.6           | 4.0            | 6.3           | 3.6            | 7.0           | 6.3           | 1.9           | 3.4            |
|                                   | SPD (MPH)    | 5.8           | 9.3           | 7.0           | 4.2            | 6.6           | 3.6            | 7.5           | 6.8           | 2.4           | 4.3            |
|                                   | RATIO        | 0.864         | 0.997         | 0.932         | 0.957          | 0.954         | 0.992          | 0.934         | 0.934         | 0.779         | 0.794          |
| MILFORD-010 (0058)                | PM10<br>DATE | 56<br>1/17/90 | 51<br>7/ 4/90 | 44<br>8/27/90 | 41<br>12/13/90 | 41<br>9/ 2/90 | 39<br>11/ 1/90 | 35<br>7/22/90 | 35<br>6/28/90 | 34<br>6/22/90 | 31<br>7/16/90  |
| METEOROLOGICAL SITE<br>NEWARK     | DIR (DEG)    | 190           | 230           | 340           | 280            | 280           | 200            | 110           | 260           | 200           | 260            |
|                                   | VEL (MPH)    | 5.8           | 14.0          | 5.0           | 9.0            | 4.8           | 2.7            | 2.4           | 2.4           | 6.4           | 7.2            |
|                                   | SPD (MPH)    | 6.3           | 16.2          | 7.2           | 11.9           | 7.2           | 5.5            | 5.0           | 5.2           | 8.3           | 9.2            |
|                                   | RATIO        | 0.912         | 0.861         | 0.694         | 0.750          | 0.670         | 0.501          | 0.486         | 0.464         | 0.773         | 0.788          |
| METEOROLOGICAL SITE<br>BRADLEY    | DIR (DEG)    | 180           | 220           | 320           | 280            | 240           | 80             | 130           | 320           | 210           | 280            |
|                                   | VEL (MPH)    | 6.2           | 8.0           | 4.8           | 5.1            | 1.4           | 6              | 3.0           | 6.9           | 6.9           | 6.6            |
|                                   | SPD (MPH)    | 8.1           | 10.2          | 6.6           | 9.3            | 4.9           | 3.3            | 6.5           | 7.5           | 8.5           | 9.9            |
|                                   | RATIO        | 0.772         | 0.781         | 0.727         | 0.541          | 0.279         | 0.183          | 0.468         | 0.926         | 0.819         | 0.663          |
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG)    | 170           | 260           | 300           | 290            | 250           | 260            | 260           | 260           | 230           | 270            |
|                                   | VEL (MPH)    | 1.4           | 8.2           | 3.5           | 7.1            | 6.7           | 1.9            | 5.4           | 5.2           | 5.5           | 7.7            |
|                                   | SPD (MPH)    | 4.6           | 8.3           | 5.8           | 8.1            | 6.9           | 3.9            | 5.5           | 5.9           | 5.6           | 8.1            |
|                                   | RATIO        | 0.306         | 0.979         | 0.602         | 0.876          | 0.967         | 0.489          | 0.987         | 0.883         | 0.974         | 0.954          |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG)    | 210           | 260           | 300           | 270            | 280           | 280            | 140           | 300           | 260           | 270            |
|                                   | VEL (MPH)    | 5.0           | 9.3           | 4.0           | 8.9            | 6.6           | 5.9            | 3.6           | 7.0           | 6.3           | 7.2            |
|                                   | SPD (MPH)    | 5.8           | 9.3           | 4.2           | 10.4           | 7.0           | 6.2            | 3.6           | 7.5           | 6.8           | 7.8            |
|                                   | RATIO        | 0.864         | 0.997         | 0.957         | 0.858          | 0.932         | 0.960          | 0.992         | 0.934         | 0.934         | 0.929          |

TABLE 2-5, CONTINUED

1990 TEN HIGHEST 24-HOUR AVERAGE PM10 DAYS WITH WIND DATA

UNITS : MICROGRAMS PER CUBIC METER

| TOWN-SITE (SAMPLES)    | RANK      | 1       | 2       | 3       | 4        | 5       | 6       | 7        | 8       | 9       | 10      |
|------------------------|-----------|---------|---------|---------|----------|---------|---------|----------|---------|---------|---------|
| NAUGATUCK-001 (0056)   |           |         |         |         |          |         |         |          |         |         |         |
| METEOROLOGICAL SITE    | PM10      | 74      | 47      | 45      | 43       | 41      | 40      | 37       | 36      | 35      | 35      |
| NEWARK                 | DATE      | 1/17/90 | 7/4/90  | 11/1/90 | 9/2/90   | 8/27/90 | 7/22/90 | 12/13/90 | 12/1/90 | 6/22/90 | 10/8/90 |
|                        | D/R (DEG) | 190     | 230     | 200     | 280      | 340     | 110     | 280      | 250     | 200     | 170     |
|                        | VEL (MPH) | 5.8     | 14.0    | 2.7     | 4.8      | 5.0     | 2.4     | 9.0      | 7.7     | 6.4     | 2.8     |
|                        | SPD (MPH) | 6.3     | 16.2    | 5.5     | 7.2      | 7.2     | 5.0     | 11.9     | 8.8     | 8.3     | 5.0     |
|                        | RATIO     | 0.912   | 0.861   | 0.501   | 0.670    | 0.694   | 0.486   | 0.750    | 0.884   | 0.773   | 0.560   |
| METEOROLOGICAL SITE    | D/R (DEG) | 180     | 220     | 80      | 240      | 320     | 130     | 280      | 190     | 210     | 190     |
| BRADLEY                | DATE      | 1/17/90 | 7/4/90  | 11/1/90 | 9/2/90   | 8/27/90 | 7/22/90 | 12/13/90 | 12/1/90 | 6/22/90 | 10/8/90 |
|                        | D/R (DEG) | 6.2     | 8.0     | 6       | 1.4      | 4.8     | 3.0     | 5.1      | 7.6     | 6.9     | 4.9     |
|                        | VEL (MPH) | 8.1     | 10.2    | 3.3     | 4.9      | 6.6     | 6.5     | 9.3      | 9.9     | 8.5     | 7.0     |
|                        | SPD (MPH) | 8.1     | 10.2    | 3.3     | 4.9      | 6.6     | 6.5     | 9.3      | 9.9     | 8.5     | 7.0     |
|                        | RATIO     | 0.772   | 0.781   | 0.183   | 0.279    | 0.727   | 0.468   | 0.541    | 0.768   | 0.819   | 0.701   |
| METEOROLOGICAL SITE    | D/R (DEG) | 170     | 260     | 260     | 250      | 300     | 110     | 290      | 260     | 230     | 210     |
| BRIDGEPORT             | DATE      | 1/17/90 | 7/4/90  | 11/1/90 | 9/2/90   | 8/27/90 | 7/22/90 | 12/13/90 | 12/1/90 | 6/22/90 | 10/8/90 |
|                        | D/R (DEG) | 1.4     | 8.2     | 1.9     | 6.7      | 3.5     | 5.4     | 7.1      | 7.6     | 5.5     | 1.3     |
|                        | VEL (MPH) | 4.6     | 8.3     | 3.9     | 6.9      | 5.8     | 5.5     | 8.1      | 8.2     | 5.6     | 2.9     |
|                        | SPD (MPH) | 4.6     | 8.3     | 3.9     | 6.9      | 5.8     | 5.5     | 8.1      | 8.2     | 5.6     | 2.9     |
|                        | RATIO     | 0.306   | 0.979   | 0.489   | 0.967    | 0.602   | 0.987   | 0.876    | 0.931   | 0.974   | 0.460   |
| METEOROLOGICAL SITE    | D/R (DEG) | 210     | 260     | 280     | 280      | 300     | 140     | 270      | 250     | 260     | 240     |
| WORCESTER              | DATE      | 1/17/90 | 7/4/90  | 11/1/90 | 9/2/90   | 8/27/90 | 7/22/90 | 12/13/90 | 12/1/90 | 6/22/90 | 10/8/90 |
|                        | D/R (DEG) | 5.0     | 9.3     | 5.9     | 6.6      | 4.0     | 3.6     | 8.9      | 11.1    | 6.3     | 2.5     |
|                        | VEL (MPH) | 5.8     | 9.3     | 6.2     | 7.0      | 4.2     | 3.6     | 10.4     | 11.2    | 6.8     | 5.5     |
|                        | SPD (MPH) | 5.8     | 9.3     | 6.2     | 7.0      | 4.2     | 3.6     | 10.4     | 11.2    | 6.8     | 5.5     |
|                        | RATIO     | 0.864   | 0.997   | 0.960   | 0.932    | 0.957   | 0.992   | 0.858    | 0.989   | 0.934   | 0.458   |
| NEW BRITAIN-012 (0058) |           |         |         |         |          |         |         |          |         |         |         |
| METEOROLOGICAL SITE    | PM10      | 59      | 45      | 43      | 43       | 42      | 37      | 34       | 34      | 34      | 33      |
| NEWARK                 | DATE      | 1/17/90 | 11/1/90 | 9/2/90  | 8/27/90  | 7/7/90  | 12/7/90 | 12/13/90 | 7/22/90 | 6/22/90 | 9/14/90 |
|                        | D/R (DEG) | 190     | 200     | 280     | 340      | 230     | 330     | 280      | 110     | 200     | 140     |
|                        | VEL (MPH) | 5.8     | 2.7     | 4.8     | 5.0      | 14.0    | 1.7     | 9.0      | 2.4     | 6.4     | 6.6     |
|                        | SPD (MPH) | 6.3     | 5.5     | 7.2     | 7.2      | 16.2    | 5.0     | 11.9     | 5.0     | 8.3     | 7.5     |
|                        | RATIO     | 0.912   | 0.501   | 0.670   | 0.694    | 0.861   | 0.334   | 0.750    | 0.486   | 0.773   | 0.881   |
| METEOROLOGICAL SITE    | D/R (DEG) | 180     | 80      | 240     | 320      | 220     | 330     | 280      | 130     | 210     | 160     |
| BRADLEY                | DATE      | 1/17/90 | 11/1/90 | 9/2/90  | 8/27/90  | 7/7/90  | 12/7/90 | 12/13/90 | 7/22/90 | 6/22/90 | 9/14/90 |
|                        | D/R (DEG) | 6.2     | .6      | 1.4     | 4.8      | 8.0     | 1.6     | 5.1      | 3.0     | 6.9     | 5.5     |
|                        | VEL (MPH) | 8.1     | 3.3     | 4.9     | 6.6      | 10.2    | 4.3     | 9.3      | 6.5     | 8.5     | 8.1     |
|                        | SPD (MPH) | 8.1     | 3.3     | 4.9     | 6.6      | 10.2    | 4.3     | 9.3      | 6.5     | 8.5     | 8.1     |
|                        | RATIO     | 0.772   | 0.183   | 0.279   | 0.727    | 0.781   | 0.375   | 0.541    | 0.468   | 0.819   | 0.681   |
| METEOROLOGICAL SITE    | D/R (DEG) | 170     | 260     | 250     | 300      | 260     | 100     | 290      | 110     | 230     | 160     |
| BRIDGEPORT             | DATE      | 1/17/90 | 11/1/90 | 9/2/90  | 8/27/90  | 7/7/90  | 12/7/90 | 12/13/90 | 7/22/90 | 6/22/90 | 9/14/90 |
|                        | D/R (DEG) | 1.4     | 1.9     | 6.7     | 3.5      | 8.2     | 1.3     | 7.1      | 5.4     | 5.5     | 6.1     |
|                        | VEL (MPH) | 4.6     | 3.9     | 6.9     | 5.8      | 8.3     | 2.7     | 8.1      | 5.5     | 5.6     | 6.6     |
|                        | SPD (MPH) | 4.6     | 3.9     | 6.9     | 5.8      | 8.3     | 2.7     | 8.1      | 5.5     | 5.6     | 6.6     |
|                        | RATIO     | 0.306   | 0.489   | 0.967   | 0.602    | 0.979   | 0.466   | 0.876    | 0.987   | 0.974   | 0.922   |
| METEOROLOGICAL SITE    | D/R (DEG) | 210     | 280     | 280     | 300      | 260     | 260     | 270      | 140     | 260     | 170     |
| WORCESTER              | DATE      | 1/17/90 | 11/1/90 | 9/2/90  | 8/27/90  | 7/7/90  | 12/7/90 | 12/13/90 | 7/22/90 | 6/22/90 | 9/14/90 |
|                        | D/R (DEG) | 5.0     | 5.9     | 6.6     | 4.0      | 9.3     | 3.4     | 8.9      | 3.6     | 6.3     | 4.3     |
|                        | VEL (MPH) | 5.8     | 6.2     | 7.0     | 4.2      | 9.3     | 4.3     | 10.4     | 3.6     | 6.8     | 4.3     |
|                        | SPD (MPH) | 5.8     | 6.2     | 7.0     | 4.2      | 9.3     | 4.3     | 10.4     | 3.6     | 6.8     | 4.3     |
|                        | RATIO     | 0.864   | 0.960   | 0.932   | 0.957    | 0.997   | 0.794   | 0.858    | 0.992   | 0.934   | 0.989   |
| NEW HAVEN-013 (0060)   |           |         |         |         |          |         |         |          |         |         |         |
| METEOROLOGICAL SITE    | PM10      | 80      | 48      | 47      | 46       | 42      | 38      | 37       | 35      | 35      | 33      |
| NEWARK                 | DATE      | 1/17/90 | 7/4/90  | 11/1/90 | 12/13/90 | 9/2/90  | 7/22/90 | 6/22/90  | 6/28/90 | 12/7/90 | 3/12/90 |
|                        | D/R (DEG) | 190     | 230     | 200     | 280      | 280     | 110     | 200      | 260     | 330     | 90      |
|                        | VEL (MPH) | 5.8     | 14.0    | 2.7     | 9.0      | 4.8     | 2.4     | 6.4      | 2.4     | 1.7     | 3.5     |
|                        | SPD (MPH) | 6.3     | 16.2    | 5.5     | 11.9     | 7.2     | 5.0     | 8.3      | 5.2     | 5.0     | 4.7     |
|                        | RATIO     | 0.912   | 0.861   | 0.501   | 0.750    | 0.670   | 0.486   | 0.773    | 0.464   | 0.334   | 0.734   |
| METEOROLOGICAL SITE    | D/R (DEG) | 180     | 220     | 80      | 240      | 240     | 130     | 210      | 320     | 330     | 360     |
| BRADLEY                | DATE      | 1/17/90 | 7/4/90  | 11/1/90 | 12/13/90 | 9/2/90  | 7/22/90 | 6/22/90  | 6/28/90 | 12/7/90 | 3/12/90 |
|                        | D/R (DEG) | 6.2     | 8.0     | 6       | 5.1      | 1.4     | 3.0     | 6.9      | 6.9     | 1.6     | 4.3     |
|                        | VEL (MPH) | 8.1     | 10.2    | 3.3     | 4.9      | 4.9     | 3.6     | 8.5      | 7.5     | 4.3     | 4.3     |
|                        | SPD (MPH) | 8.1     | 10.2    | 3.3     | 4.9      | 4.9     | 3.6     | 8.5      | 7.5     | 4.3     | 4.3     |
|                        | RATIO     | 0.772   | 0.781   | 0.183   | 0.541    | 0.279   | 0.468   | 0.819    | 0.926   | 0.375   | 0.992   |

TABLE 2-5, CONTINUED

1990 TEN HIGHEST 24-HOUR AVERAGE PM10 DAYS WITH WIND DATA

UNITS : MICROGRAMS PER CUBIC METER

| TOWN-SITE (SAMPLES)               | RANK         | 1              | 2               | 3               | 4              | 5              | 6               | 7              | 8              | 9             | 10            |
|-----------------------------------|--------------|----------------|-----------------|-----------------|----------------|----------------|-----------------|----------------|----------------|---------------|---------------|
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG)    | 170            | 260             | 260             | 290            | 250            | 110             | 230            | 260            | 100           | 100           |
|                                   | VEL (MPH)    | 1.4            | 8.2             | 1.9             | 7.1            | 6.7            | 5.4             | 5.5            | 5.2            | 1.3           | 6.8           |
|                                   | SPD (MPH)    | 4.6            | 8.3             | 3.9             | 8.1            | 6.9            | 5.5             | 5.6            | 5.9            | 2.7           | 6.9           |
|                                   | RATIO        | 0.306          | 0.979           | 0.489           | 0.876          | 0.967          | 0.987           | 0.974          | 0.863          | 0.466         | 0.983         |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG)    | 210            | 260             | 280             | 270            | 280            | 140             | 260            | 300            | 260           | 130           |
|                                   | VEL (MPH)    | 5.0            | 9.3             | 5.9             | 8.9            | 6.6            | 3.6             | 6.3            | 7.0            | 3.4           | 1.8           |
|                                   | SPD (MPH)    | 5.8            | 9.3             | 6.2             | 10.4           | 7.0            | 3.6             | 6.8            | 7.5            | 4.3           | 2.0           |
|                                   | RATIO        | 0.864          | 0.997           | 0.960           | 0.858          | 0.932          | 0.992           | 0.934          | 0.934          | 0.794         | 0.889         |
| NEW HAVEN-018 (0349)              | PM10<br>DATE | 123<br>1/19/90 | 121<br>11/20/90 | 119<br>11/21/90 | 116<br>1/17/90 | 105<br>8/17/90 | 103<br>11/14/90 | 101<br>3/ 9/90 | 99<br>2/13/90  | 97<br>3/13/90 | 89<br>2/ 8/90 |
| METEOROLOGICAL SITE<br>NEWARK     | DIR (DEG)    | 320            | 330             | 360             | 190            | 190            | 300             | 230            | 180            | 270           | 180           |
|                                   | VEL (MPH)    | 10.5           | 9.6             | 5.4             | 5.8            | 5.8            | 11.5            | 3.2            | 7.5            | 7.8           | 3.4           |
|                                   | SPD (MPH)    | 11.9           | 10.2            | 5.8             | 6.3            | 7.6            | 14.4            | 6.0            | 8.6            | 8.9           | 5.3           |
|                                   | RATIO        | 0.877          | 0.944           | 0.943           | 0.912          | 0.757          | 0.801           | 0.538          | 0.869          | 0.873         | 0.631         |
| METEOROLOGICAL SITE<br>BRADLEY    | DIR (DEG)    | 320            | 340             | 360             | 180            | 210            | 300             | 190            | 190            | 350           | 170           |
|                                   | VEL (MPH)    | 9.1            | 9.3             | 5.5             | 6.2            | 3.1            | 7.3             | 1.5            | 10.5           | 3.7           | 6.1           |
|                                   | SPD (MPH)    | 10.6           | 9.9             | 6.0             | 8.1            | 6.0            | 9.2             | 4.5            | 10.6           | 6.2           | 7.2           |
|                                   | RATIO        | 0.855          | 0.942           | 0.911           | 0.772          | 0.508          | 0.796           | 0.327          | 0.990          | 0.596         | 0.855         |
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG)    | 350            | 360             | 350             | 170            | 210            | 330             | 180            | 240            | 280           | 250           |
|                                   | VEL (MPH)    | 4.4            | 7.6             | 3.3             | 1.4            | 3.4            | 6.0             | 1.1            | 6.7            | 3.4           | 4.9           |
|                                   | SPD (MPH)    | 4.7            | 7.8             | 3.7             | 4.6            | 3.7            | 6.2             | 2.3            | 6.8            | 5.2           | 5.6           |
|                                   | RATIO        | 0.933          | 0.985           | 0.891           | 0.306          | 0.897          | 0.968           | 0.470          | 0.996          | 0.657         | 0.875         |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG)    | 310            | 330             | 350             | 210            | 260            | 310             | 200            | 230            | 290           | 250           |
|                                   | VEL (MPH)    | 7.8            | 9.0             | 4.3             | 5.0            | 5.0            | 9.2             | 1.1            | 8.3            | 7.9           | 7.2           |
|                                   | SPD (MPH)    | 8.3            | 9.1             | 4.7             | 5.8            | 5.5            | 9.5             | 3.9            | 8.6            | 8.3           | 7.6           |
|                                   | RATIO        | 0.930          | 0.992           | 0.904           | 0.864          | 0.923          | 0.975           | 0.293          | 0.968          | 0.952         | 0.947         |
| NEW HAVEN-020 (0060)              | PM10<br>DATE | 73<br>1/17/90  | 53<br>11/ 1/90  | 51<br>12/13/90  | 47<br>7/ 4/90  | 44<br>9/ 2/90  | 41<br>8/27/90   | 41<br>6/28/90  | 40<br>12/ 7/90 | 40<br>6/22/90 | 40<br>2/28/90 |
| METEOROLOGICAL SITE<br>NEWARK     | DIR (DEG)    | 190            | 200             | 280             | 230            | 280            | 340             | 260            | 330            | 200           | 320           |
|                                   | VEL (MPH)    | 5.8            | 2.7             | 9.0             | 14.0           | 4.8            | 5.0             | 2.4            | 1.7            | 6.4           | 10.8          |
|                                   | SPD (MPH)    | 6.3            | 5.5             | 11.9            | 16.2           | 7.2            | 7.2             | 5.2            | 5.0            | 8.3           | 12.1          |
|                                   | RATIO        | 0.912          | 0.501           | 0.750           | 0.861          | 0.670          | 0.694           | 0.464          | 0.334          | 0.773         | 0.891         |
| METEOROLOGICAL SITE<br>BRADLEY    | DIR (DEG)    | 180            | 80              | 280             | 220            | 240            | 320             | 320            | 330            | 210           | 320           |
|                                   | VEL (MPH)    | 6.2            | .6              | 5.1             | 8.0            | 1.4            | 4.8             | 6.9            | 1.6            | 6.9           | 10.1          |
|                                   | SPD (MPH)    | 8.1            | 3.3             | 9.3             | 10.2           | 4.9            | 6.6             | 7.5            | 4.3            | 8.5           | 11.5          |
|                                   | RATIO        | 0.772          | 0.183           | 0.541           | 0.781          | 0.279          | 0.727           | 0.926          | 0.375          | 0.819         | 0.882         |
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG)    | 170            | 260             | 290             | 260            | 250            | 300             | 260            | 100            | 230           | 340           |
|                                   | VEL (MPH)    | 1.4            | 1.9             | 7.1             | 8.2            | 6.7            | 3.5             | 5.2            | 1.3            | 5.5           | 7.0           |
|                                   | SPD (MPH)    | 4.6            | 3.9             | 8.1             | 8.3            | 6.9            | 5.8             | 5.9            | 2.7            | 5.6           | 7.2           |
|                                   | RATIO        | 0.306          | 0.489           | 0.876           | 0.979          | 0.967          | 0.602           | 0.883          | 0.466          | 0.974         | 0.979         |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG)    | 210            | 280             | 270             | 260            | 280            | 300             | 300            | 260            | 260           | 300           |
|                                   | VEL (MPH)    | 5.0            | 5.9             | 8.9             | 9.3            | 6.6            | 4.0             | 7.0            | 3.4            | 6.3           | 7.9           |
|                                   | SPD (MPH)    | 5.8            | 6.2             | 10.4            | 9.3            | 7.0            | 4.2             | 7.5            | 4.3            | 6.8           | 8.1           |
|                                   | RATIO        | 0.864          | 0.960           | 0.858           | 0.997          | 0.932          | 0.957           | 0.934          | 0.794          | 0.934         | 0.986         |

TABLE 2-5, CONTINUED

1990 TEN HIGHEST 24-HOUR AVERAGE PM10 DAYS WITH WIND DATA

UNITS : MICROGRAMS PER CUBIC METER

| TOWN-SITE (SAMPLES)   | RANK | 1       | 2       | 3       | 4       | 5       | 6        | 7       | 8       | 9        | 10       |
|-----------------------|------|---------|---------|---------|---------|---------|----------|---------|---------|----------|----------|
| NEW HAVEN-123 (0055)  |      | 81      | 53      | 53      | 49      | 45      | 45       | 41      | 38      | 37       | 37       |
| METEOROLOGICAL SITE   |      | 1/17/90 | 6/22/90 | 8/27/90 | 7/4/90  | 9/2/90  | 12/13/90 | 8/3/90  | 12/7/90 | 7/22/90  | 10/8/90  |
| NEWARK                |      | 190     | 200     | 340     | 230     | 280     | 280      | 170     | 330     | 110      | 170      |
| DIR (DEG)             |      | 5.8     | 6.4     | 5.0     | 14.0    | 4.8     | 9.0      | 1.0     | 1.7     | 2.4      | 2.8      |
| VEL (MPH)             |      | 6.3     | 8.3     | 7.2     | 16.2    | 7.2     | 11.9     | 4.2     | 5.0     | 5.0      | 5.0      |
| SPD (MPH)             |      | 0.912   | 0.773   | 0.694   | 0.861   | 0.670   | 0.750    | 0.233   | 0.334   | 0.486    | 0.560    |
| RATIO                 |      | 180     | 210     | 320     | 220     | 240     | 280      | 290     | 330     | 130      | 190      |
| BRADLEY               |      | 6.2     | 6.9     | 4.8     | 8.0     | 1.4     | 5.1      | 2.5     | 1.6     | 3.0      | 4.9      |
| DIR (DEG)             |      | 8.1     | 8.5     | 6.6     | 10.2    | 4.9     | 9.3      | 5.0     | 4.3     | 6.5      | 7.0      |
| VEL (MPH)             |      | 0.772   | 0.819   | 0.727   | 0.781   | 0.279   | 0.541    | 0.492   | 0.375   | 0.468    | 0.701    |
| SPD (MPH)             |      | 170     | 230     | 300     | 260     | 250     | 290      | 240     | 100     | 110      | 210      |
| RATIO                 |      | 1.4     | 5.5     | 3.5     | 8.2     | 6.7     | 7.1      | 5.0     | 1.3     | 5.4      | 1.3      |
| BRIDGEPORT            |      | 4.6     | 5.6     | 5.8     | 8.3     | 6.9     | 8.1      | 5.0     | 2.7     | 5.5      | 2.9      |
| DIR (DEG)             |      | 0.306   | 0.974   | 0.662   | 0.979   | 0.967   | 0.876    | 0.996   | 0.466   | 0.987    | 0.460    |
| VEL (MPH)             |      | 210     | 260     | 300     | 260     | 280     | 270      | 300     | 260     | 140      | 240      |
| SPD (MPH)             |      | 5.0     | 6.3     | 4.0     | 9.3     | 6.6     | 8.9      | 5.6     | 3.4     | 3.6      | 2.5      |
| RATIO                 |      | 5.8     | 6.8     | 4.2     | 9.3     | 7.0     | 10.4     | 5.9     | 4.3     | 3.6      | 5.5      |
| WORCESTER             |      | 0.864   | 0.934   | 0.957   | 0.997   | 0.932   | 0.858    | 0.944   | 0.794   | 0.992    | 0.458    |
| METEOROLOGICAL SITE   |      | 58      | 47      | 41      | 39      | 34      | 34       | 33      | 30      | 30       | 29       |
| NEW LONDON-004 (0058) |      | 1/17/90 | 7/4/90  | 9/2/90  | 8/27/90 | 3/12/90 | 6/22/90  | 7/22/90 | 6/28/90 | 12/13/90 | 2/28/90  |
| NEWARK                |      | 190     | 230     | 280     | 340     | 90      | 200      | 110     | 260     | 280      | 320      |
| DIR (DEG)             |      | 5.8     | 14.0    | 4.8     | 5.0     | 3.5     | 6.4      | 2.4     | 2.4     | 9.0      | 10.8     |
| VEL (MPH)             |      | 6.3     | 16.2    | 7.2     | 7.2     | 4.7     | 8.3      | 5.0     | 5.2     | 11.9     | 12.1     |
| SPD (MPH)             |      | 0.912   | 0.861   | 0.670   | 0.694   | 0.734   | 0.773    | 0.486   | 0.464   | 0.750    | 0.891    |
| RATIO                 |      | 180     | 220     | 240     | 320     | 360     | 210      | 130     | 320     | 280      | 320      |
| BRADLEY               |      | 6.2     | 8.0     | 1.4     | 4.8     | 4.3     | 6.9      | 3.0     | 6.9     | 5.1      | 10.1     |
| DIR (DEG)             |      | 8.1     | 10.2    | 4.9     | 6.6     | 4.3     | 8.5      | 6.5     | 7.5     | 9.3      | 11.5     |
| VEL (MPH)             |      | 0.772   | 0.781   | 0.279   | 0.727   | 0.992   | 0.819    | 0.468   | 0.926   | 0.541    | 0.882    |
| SPD (MPH)             |      | 170     | 260     | 250     | 300     | 100     | 230      | 110     | 260     | 290      | 340      |
| RATIO                 |      | 1.4     | 8.2     | 6.7     | 3.5     | 6.8     | 5.5      | 5.4     | 5.2     | 7.1      | 7.0      |
| BRIDGEPORT            |      | 4.6     | 8.3     | 6.9     | 5.8     | 6.9     | 5.6      | 5.5     | 5.9     | 8.1      | 7.2      |
| DIR (DEG)             |      | 0.306   | 0.979   | 0.967   | 0.602   | 0.983   | 0.974    | 0.987   | 0.883   | 0.876    | 0.979    |
| VEL (MPH)             |      | 210     | 260     | 280     | 300     | 130     | 260      | 140     | 300     | 270      | 300      |
| SPD (MPH)             |      | 5.0     | 9.3     | 6.6     | 4.0     | 1.8     | 6.3      | 3.6     | 7.0     | 8.9      | 7.9      |
| RATIO                 |      | 5.8     | 9.3     | 7.0     | 4.2     | 2.0     | 6.8      | 3.6     | 7.5     | 10.4     | 8.1      |
| WORCESTER             |      | 0.864   | 0.997   | 0.932   | 0.957   | 0.889   | 0.934    | 0.992   | 0.934   | 0.858    | 0.986    |
| METEOROLOGICAL SITE   |      | 90      | 82      | 74      | 71      | 63      | 58       | 57      | 56      | 54       | 51       |
| NORWALK-014 (0059)    |      | 1/17/90 | 1/23/90 | 11/1/90 | 8/27/90 | 1/5/90  | 10/2/90  | 3/12/90 | 6/28/90 | 9/2/90   | 10/14/90 |
| NEWARK                |      | 190     | 270     | 200     | 340     | 320     | 300      | 90      | 260     | 280      | 300      |
| DIR (DEG)             |      | 5.8     | 4.8     | 2.7     | 5.0     | 7.2     | 8.2      | 3.5     | 2.4     | 4.8      | 4.5      |
| VEL (MPH)             |      | 6.3     | 8.9     | 5.5     | 7.2     | 9.8     | 10.1     | 4.7     | 5.2     | 7.2      | 6.9      |
| SPD (MPH)             |      | 0.912   | 0.538   | 0.501   | 0.694   | 0.733   | 0.820    | 0.734   | 0.464   | 0.670    | 0.648    |
| RATIO                 |      | 180     | 220     | 80      | 320     | 320     | 300      | 360     | 320     | 240      | 310      |
| BRADLEY               |      | 6.2     | 2.4     | 6       | 4.8     | 8.1     | 12.3     | 4.3     | 6.9     | 1.4      | 5.6      |
| DIR (DEG)             |      | 8.1     | 4.5     | 3.3     | 6.6     | 8.8     | 13.5     | 4.3     | 7.5     | 4.9      | 6.8      |
| VEL (MPH)             |      | 0.772   | 0.541   | 0.183   | 0.727   | 0.920   | 0.912    | 0.992   | 0.926   | 0.279    | 0.824    |
| SPD (MPH)             |      |         |         |         |         |         |          |         |         |          |          |
| RATIO                 |      |         |         |         |         |         |          |         |         |          |          |

TABLE 2-5. CONTINUED

1990 TEN HIGHEST 24-HOUR AVERAGE PM10 DAYS WITH WIND DATA

UNITS : MICROGRAMS PER CUBIC METER

| TOWN-SITE (SAMPLES)               | RANK | 1         | 2         | 3         | 4         | 5         | 6         | 7         | 8         | 9         | 10        |
|-----------------------------------|------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| METEOROLOGICAL SITE<br>BRIDGEPORT |      | 170       | 280       | 260       | 300       | 300       | 320       | 100       | 260       | 250       | 340       |
|                                   |      | DIR (DEG) |
|                                   |      | 1.4       | 3.6       | 1.9       | 3.5       | 3.2       | 8.8       | 6.8       | 5.2       | 6.7       | 4.5       |
|                                   |      | VEL (MPH) |
|                                   |      | 4.6       | 6.0       | 3.9       | 5.8       | 4.0       | 9.3       | 6.9       | 5.9       | 6.9       | 4.6       |
|                                   |      | RATIO     |
|                                   |      | 0.306     | 0.603     | 0.489     | 0.602     | 0.785     | 0.942     | 0.983     | 0.883     | 0.967     | 0.977     |
| METEOROLOGICAL SITE<br>WORCESTER  |      | 210       | 280       | 280       | 300       | 290       | 300       | 130       | 300       | 280       | 340       |
|                                   |      | DIR (DEG) |
|                                   |      | 5.0       | 4.9       | 5.9       | 4.0       | 6.3       | 13.1      | 1.8       | 7.0       | 6.6       | 5.4       |
|                                   |      | VEL (MPH) |
|                                   |      | 5.8       | 5.3       | 6.2       | 4.2       | 6.6       | 13.5      | 2.0       | 7.5       | 7.0       | 5.9       |
|                                   |      | RATIO     |
|                                   |      | 0.864     | 0.922     | 0.960     | 0.957     | 0.954     | 0.967     | 0.889     | 0.934     | 0.932     | 0.915     |
| NORWICH-002 (0059)                |      | 54        | 48        | 43        | 38        | 35        | 35        | 33        | 32        | 32        | 30        |
|                                   |      | DATE      |
|                                   |      | 1/17/90   | 7/4/90    | 9/2/90    | 8/27/90   | 12/7/90   | 7/22/90   | 1/23/90   | 6/22/90   | 12/13/90  | 7/16/90   |
| METEOROLOGICAL SITE<br>NEWARK     |      | 190       | 230       | 280       | 340       | 330       | 110       | 270       | 200       | 280       | 260       |
|                                   |      | DIR (DEG) |
|                                   |      | 5.8       | 14.0      | 4.8       | 5.0       | 1.7       | 2.4       | 4.8       | 6.4       | 9.0       | 7.2       |
|                                   |      | VEL (MPH) |
|                                   |      | 6.3       | 16.2      | 7.2       | 7.2       | 5.0       | 5.0       | 8.9       | 8.3       | 11.9      | 9.2       |
|                                   |      | RATIO     |
|                                   |      | 0.912     | 0.861     | 0.670     | 0.694     | 0.334     | 0.486     | 0.538     | 0.773     | 0.750     | 0.788     |
| METEOROLOGICAL SITE<br>BRADLEY    |      | 180       | 220       | 240       | 320       | 330       | 130       | 220       | 210       | 280       | 280       |
|                                   |      | DIR (DEG) |
|                                   |      | 6.2       | 8.0       | 1.4       | 4.8       | 1.6       | 3.0       | 2.4       | 6.9       | 5.1       | 6.6       |
|                                   |      | VEL (MPH) |
|                                   |      | 8.1       | 10.2      | 4.9       | 6.6       | 4.3       | 6.5       | 4.5       | 8.5       | 9.3       | 9.9       |
|                                   |      | RATIO     |
|                                   |      | 0.772     | 0.781     | 0.279     | 0.727     | 0.375     | 0.468     | 0.541     | 0.819     | 0.541     | 0.663     |
| METEOROLOGICAL SITE<br>BRIDGEPORT |      | 170       | 260       | 250       | 300       | 100       | 110       | 280       | 230       | 290       | 270       |
|                                   |      | DIR (DEG) |
|                                   |      | 1.4       | 8.2       | 6.7       | 3.5       | 1.3       | 5.4       | 3.6       | 5.5       | 7.1       | 7.7       |
|                                   |      | VEL (MPH) |
|                                   |      | 4.6       | 8.3       | 6.9       | 5.8       | 2.7       | 5.5       | 6.0       | 5.6       | 8.1       | 8.1       |
|                                   |      | RATIO     |
|                                   |      | 0.306     | 0.979     | 0.967     | 0.602     | 0.466     | 0.987     | 0.603     | 0.974     | 0.876     | 0.954     |
| METEOROLOGICAL SITE<br>WORCESTER  |      | 210       | 260       | 280       | 300       | 260       | 140       | 280       | 260       | 270       | 270       |
|                                   |      | DIR (DEG) |
|                                   |      | 5.0       | 9.3       | 6.6       | 4.0       | 3.4       | 3.6       | 4.9       | 6.3       | 8.9       | 7.2       |
|                                   |      | VEL (MPH) |
|                                   |      | 5.8       | 9.3       | 7.0       | 4.2       | 4.3       | 3.6       | 5.3       | 6.8       | 10.4      | 7.8       |
|                                   |      | RATIO     |
|                                   |      | 0.864     | 0.997     | 0.932     | 0.957     | 0.794     | 0.992     | 0.922     | 0.934     | 0.858     | 0.929     |
| STAMFORD-001 (0059)               |      | 80        | 48        | 48        | 47        | 44        | 44        | 40        | 37        | 37        | 36        |
|                                   |      | DATE      |
|                                   |      | 1/17/90   | 7/4/90    | 9/2/90    | 11/1/90   | 12/13/90  | 10/8/90   | 6/28/90   | 2/15/90   | 6/22/90   | 12/1/90   |
| METEOROLOGICAL SITE<br>NEWARK     |      | 190       | 230       | 280       | 200       | 280       | 170       | 260       | 50        | 200       | 250       |
|                                   |      | DIR (DEG) |
|                                   |      | 5.8       | 14.0      | 4.8       | 2.7       | 9.0       | 2.8       | 2.4       | 3.1       | 6.4       | 7.7       |
|                                   |      | VEL (MPH) |
|                                   |      | 6.3       | 16.2      | 7.2       | 5.5       | 11.9      | 5.0       | 5.2       | 5.3       | 8.3       | 8.8       |
|                                   |      | RATIO     |
|                                   |      | 0.912     | 0.861     | 0.670     | 0.501     | 0.750     | 0.560     | 0.464     | 0.578     | 0.773     | 0.884     |
| METEOROLOGICAL SITE<br>BRADLEY    |      | 180       | 220       | 240       | 80        | 280       | 190       | 320       | 20        | 210       | 190       |
|                                   |      | DIR (DEG) |
|                                   |      | 6.2       | 8.0       | 1.4       | .6        | 5.1       | 4.9       | 6.9       | 1.2       | 6.9       | 7.6       |
|                                   |      | VEL (MPH) |
|                                   |      | 8.1       | 10.2      | 4.9       | 3.3       | 9.3       | 7.0       | 7.5       | 3.2       | 8.5       | 9.9       |
|                                   |      | RATIO     |
|                                   |      | 0.772     | 0.781     | 0.279     | 0.183     | 0.541     | 0.701     | 0.926     | 0.377     | 0.819     | 0.768     |
| METEOROLOGICAL SITE<br>BRIDGEPORT |      | 170       | 260       | 250       | 260       | 290       | 210       | 260       | 140       | 230       | 260       |
|                                   |      | DIR (DEG) |
|                                   |      | 1.4       | 8.2       | 6.7       | 1.9       | 7.1       | 1.3       | 5.2       | 1.0       | 5.5       | 7.6       |
|                                   |      | VEL (MPH) |
|                                   |      | 4.6       | 8.3       | 6.9       | 3.9       | 8.1       | 2.9       | 2.7       | 2.7       | 5.6       | 8.2       |
|                                   |      | RATIO     |
|                                   |      | 0.306     | 0.979     | 0.967     | 0.489     | 0.876     | 0.460     | 0.883     | 0.383     | 0.974     | 0.931     |
| METEOROLOGICAL SITE<br>WORCESTER  |      | 210       | 260       | 280       | 280       | 270       | 240       | 300       | 10        | 260       | 250       |
|                                   |      | DIR (DEG) |
|                                   |      | 5.0       | 9.3       | 6.6       | 5.9       | 8.9       | 2.5       | 1.9       | 1.9       | 6.3       | 11.1      |
|                                   |      | VEL (MPH) |
|                                   |      | 5.8       | 9.3       | 7.0       | 6.2       | 10.4      | 5.5       | 7.5       | 2.4       | 6.8       | 11.2      |
|                                   |      | RATIO     |
|                                   |      | 0.864     | 0.997     | 0.932     | 0.960     | 0.858     | 0.458     | 0.934     | 0.779     | 0.934     | 0.989     |

TABLE 2-5, CONTINUED

1990 TEN HIGHEST 24-HOUR AVERAGE PM10 DAYS WITH WIND DATA

UNITS : MICROGRAMS PER CUBIC METER

| TOWN-SITE (SAMPLES)   | RANK      | 1       | 2       | 3        | 4       | 5        | 6        | 7       | 8       | 9       | 10       |
|-----------------------|-----------|---------|---------|----------|---------|----------|----------|---------|---------|---------|----------|
| STRATFORD-005 (0055)  |           | 70      | 52      | 49       | 49      | 47       | 44       | 44      | 44      | 43      | 38       |
| METEOROLOGICAL SITE   | DATE      | 1/17/90 | 7/ 4/90 | 12/13/90 | 1/23/90 | 1/ 5/90  | 11/ 1/90 | 9/ 2/90 | 8/27/90 | 6/22/90 | 7/22/90  |
| NEWARK                | DIR (DEG) | 190     | 230     | 280      | 270     | 320      | 200      | 280     | 340     | 200     | 110      |
|                       | VEL (MPH) | 5.8     | 14.0    | 9.0      | 4.8     | 7.2      | 2.7      | 4.8     | 5.0     | 6.4     | 2.4      |
|                       | SPD (MPH) | 6.3     | 16.2    | 11.9     | 8.9     | 9.8      | 5.5      | 7.2     | 7.2     | 8.3     | 5.0      |
|                       | RATIO     | 0.912   | 0.861   | 0.750    | 0.538   | 0.733    | 0.501    | 0.670   | 0.694   | 0.773   | 0.486    |
| METEOROLOGICAL SITE   | DIR (DEG) | 180     | 220     | 280      | 220     | 320      | 80       | 240     | 320     | 210     | 130      |
| BRADLEY               | VEL (MPH) | 6.2     | 8.0     | 5.1      | 2.4     | 8.1      | 6        | 1.4     | 4.8     | 6.9     | 3.0      |
|                       | SPD (MPH) | 8.1     | 10.2    | 9.3      | 4.5     | 8.8      | 3.3      | 4.9     | 6.6     | 8.5     | 6.5      |
|                       | RATIO     | 0.772   | 0.781   | 0.541    | 0.541   | 0.920    | 0.183    | 0.279   | 0.727   | 0.819   | 0.468    |
| METEOROLOGICAL SITE   | DIR (DEG) | 170     | 260     | 290      | 280     | 300      | 260      | 250     | 300     | 230     | 110      |
| BRIDGEPORT            | VEL (MPH) | 1.4     | 8.2     | 7.1      | 3.6     | 3.2      | 1.9      | 6.7     | 3.5     | 5.5     | 5.4      |
|                       | SPD (MPH) | 4.6     | 8.3     | 8.1      | 6.0     | 4.0      | 3.9      | 6.9     | 5.8     | 5.6     | 5.5      |
|                       | RATIO     | 0.306   | 0.979   | 0.876    | 0.603   | 0.785    | 0.489    | 0.967   | 0.602   | 0.974   | 0.987    |
| METEOROLOGICAL SITE   | DIR (DEG) | 210     | 260     | 270      | 280     | 290      | 280      | 280     | 300     | 260     | 140      |
| WORCESTER             | VEL (MPH) | 5.0     | 9.3     | 8.9      | 4.9     | 6.3      | 5.9      | 6.6     | 4.0     | 6.3     | 3.6      |
|                       | SPD (MPH) | 5.8     | 9.3     | 10.4     | 5.3     | 6.6      | 6.2      | 7.0     | 4.2     | 6.8     | 3.6      |
|                       | RATIO     | 0.864   | 0.997   | 0.858    | 0.922   | 0.954    | 0.960    | 0.932   | 0.957   | 0.934   | 0.992    |
| TORRINGTON-001 (0059) |           | 55      | 44      | 39       | 39      | 37       | 35       | 34      | 33      | 32      | 31       |
| METEOROLOGICAL SITE   | DATE      | 1/17/90 | 7/ 4/90 | 9/ 2/90  | 8/27/90 | 10/ 8/90 | 12/13/90 | 9/14/90 | 2/22/90 | 6/22/90 | 7/22/90  |
| NEWARK                | DIR (DEG) | 190     | 230     | 280      | 340     | 170      | 280      | 140     | 210     | 200     | 110      |
|                       | VEL (MPH) | 5.8     | 14.0    | 4.8      | 5.0     | 2.8      | 2.8      | 6.6     | 8.0     | 6.4     | 2.4      |
|                       | SPD (MPH) | 6.3     | 16.2    | 7.2      | 7.2     | 5.0      | 11.9     | 7.5     | 10.8    | 8.3     | 5.0      |
|                       | RATIO     | 0.912   | 0.861   | 0.670    | 0.694   | 0.560    | 0.750    | 0.881   | 0.738   | 0.773   | 0.486    |
| METEOROLOGICAL SITE   | DIR (DEG) | 180     | 220     | 240      | 320     | 190      | 280      | 160     | 190     | 210     | 130      |
| BRADLEY               | VEL (MPH) | 6.2     | 8.0     | 1.4      | 4.8     | 4.9      | 5.1      | 5.5     | 10.0    | 6.9     | 3.0      |
|                       | SPD (MPH) | 8.1     | 10.2    | 4.9      | 6.6     | 7.0      | 9.3      | 8.1     | 13.8    | 8.5     | 6.5      |
|                       | RATIO     | 0.772   | 0.781   | 0.279    | 0.727   | 0.701    | 0.541    | 0.681   | 0.727   | 0.819   | 0.468    |
| METEOROLOGICAL SITE   | DIR (DEG) | 170     | 260     | 250      | 300     | 210      | 290      | 160     | 240     | 230     | 110      |
| BRIDGEPORT            | VEL (MPH) | 1.4     | 8.2     | 6.7      | 3.5     | 1.3      | 7.1      | 6.1     | 8.1     | 5.5     | 5.4      |
|                       | SPD (MPH) | 4.6     | 8.3     | 6.9      | 5.8     | 2.9      | 8.1      | 6.6     | 8.2     | 5.6     | 5.5      |
|                       | RATIO     | 0.306   | 0.979   | 0.967    | 0.602   | 0.460    | 0.876    | 0.922   | 0.986   | 0.974   | 0.987    |
| METEOROLOGICAL SITE   | DIR (DEG) | 210     | 260     | 280      | 300     | 240      | 270      | 170     | 240     | 260     | 140      |
| WORCESTER             | VEL (MPH) | 5.0     | 9.3     | 6.6      | 4.0     | 2.5      | 8.9      | 4.3     | 14.1    | 6.3     | 3.6      |
|                       | SPD (MPH) | 5.8     | 9.3     | 7.0      | 4.2     | 5.5      | 10.4     | 4.3     | 14.2    | 6.8     | 3.6      |
|                       | RATIO     | 0.864   | 0.997   | 0.932    | 0.957   | 0.458    | 0.858    | 0.989   | 0.991   | 0.934   | 0.992    |
| VOLUNTTOWN-001 (0060) |           | 43      | 39      | 33       | 29      | 27       | 27       | 25      | 25      | 24      | 23       |
| METEOROLOGICAL SITE   | DATE      | 7/ 4/90 | 9/ 2/90 | 7/22/90  | 1/17/90 | 9/14/90  | 7/16/90  | 8/ 9/90 | 8/27/90 | 6/22/90 | 10/ 8/90 |
| NEWARK                | DIR (DEG) | 230     | 280     | 110      | 190     | 140      | 260      | 20      | 340     | 200     | 170      |
|                       | VEL (MPH) | 14.0    | 4.8     | 2.4      | 5.8     | 6.6      | 7.2      | 5.8     | 5.0     | 6.4     | 2.8      |
|                       | SPD (MPH) | 16.2    | 7.2     | 5.0      | 6.3     | 7.5      | 9.2      | 7.8     | 7.2     | 8.3     | 5.0      |
|                       | RATIO     | 0.861   | 0.670   | 0.486    | 0.912   | 0.881    | 0.788    | 0.744   | 0.694   | 0.773   | 0.560    |
| METEOROLOGICAL SITE   | DIR (DEG) | 220     | 240     | 130      | 180     | 160      | 280      | 10      | 320     | 210     | 190      |
| BRADLEY               | VEL (MPH) | 8.0     | 1.4     | 3.0      | 6.2     | 5.5      | 6.6      | 3.8     | 4.8     | 6.9     | 4.9      |
|                       | SPD (MPH) | 10.2    | 4.9     | 6.5      | 8.1     | 8.1      | 9.9      | 6.0     | 6.6     | 8.5     | 7.0      |
|                       | RATIO     | 0.781   | 0.279   | 0.468    | 0.772   | 0.681    | 0.663    | 0.637   | 0.727   | 0.819   | 0.701    |

TABLE 2-5, CONTINUED

1990 TEN HIGHEST 24-HOUR AVERAGE PM10 DAYS WITH WIND DATA

UNITS : MICROGRAMS PER CUBIC METER

| TOWN-SITE (SAMPLES)               | RANK | 1         | 2         | 3         | 4         | 5         | 6         | 7         | 8         | 9         | 10        |
|-----------------------------------|------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| METEOROLOGICAL SITE<br>BRIDGEPORT |      | 260       | 250       | 110       | 170       | 160       | 270       | 50        | 300       | 230       | 210       |
|                                   |      | DIR (DEG) |
|                                   |      | 8.2       | 6.7       | 5.4       | 1.4       | 6.1       | 7.7       | 1.2       | 3.5       | 5.5       | 1.3       |
|                                   |      | VEL (MPH) |
|                                   |      | 8.3       | 6.9       | 5.5       | 4.6       | 6.6       | 8.1       | 5.2       | 5.8       | 5.6       | 2.9       |
|                                   |      | SPD (MPH) |
|                                   |      | 0.979     | 0.967     | 0.987     | 0.306     | 0.922     | 0.954     | 0.230     | 0.602     | 0.974     | 0.460     |
|                                   |      | RATIO     |
| METEOROLOGICAL SITE<br>WORCESTER  |      | 260       | 280       | 140       | 210       | 170       | 270       | 80        | 300       | 260       | 240       |
|                                   |      | DIR (DEG) |
|                                   |      | 9.3       | 6.6       | 3.6       | 5.0       | 4.3       | 7.2       | 2.8       | 4.0       | 6.3       | 2.5       |
|                                   |      | VEL (MPH) |
|                                   |      | 9.3       | 7.0       | 3.6       | 5.8       | 4.3       | 7.8       | 4.6       | 4.2       | 6.8       | 5.5       |
|                                   |      | SPD (MPH) |
|                                   |      | 0.997     | 0.932     | 0.992     | 0.864     | 0.989     | 0.929     | 0.600     | 0.957     | 0.934     | 0.458     |
|                                   |      | RATIO     |
| WALLINGFORD-006 (0053)            |      | 57        | 42        | 41        | 37        | 34        | 32        | 31        | 29        | 29        | 27        |
|                                   |      | PM10      |
|                                   |      | DATE      |
|                                   |      | 1/17/90   | 7/4/90    | 9/2/90    | 8/27/90   | 7/22/90   | 1/5/90    | 6/22/90   | 8/9/90    | 12/1/90   | 1/23/90   |
| METEOROLOGICAL SITE<br>NEWARK     |      | 190       | 230       | 280       | 340       | 110       | 320       | 200       | 20        | 250       | 270       |
|                                   |      | DIR (DEG) |
|                                   |      | 5.8       | 14.0      | 4.8       | 5.0       | 2.4       | 7.2       | 6.4       | 5.8       | 7.7       | 4.8       |
|                                   |      | VEL (MPH) |
|                                   |      | 6.3       | 16.2      | 7.2       | 7.2       | 5.0       | 9.8       | 8.3       | 7.8       | 8.8       | 8.9       |
|                                   |      | SPD (MPH) |
|                                   |      | 0.912     | 0.861     | 0.670     | 0.694     | 0.486     | 0.733     | 0.773     | 0.744     | 0.884     | 0.538     |
|                                   |      | RATIO     |
| METEOROLOGICAL SITE<br>BRADLEY    |      | 180       | 220       | 240       | 320       | 130       | 320       | 210       | 10        | 190       | 220       |
|                                   |      | DIR (DEG) |
|                                   |      | 6.2       | 8.0       | 1.4       | 4.8       | 3.0       | 8.1       | 6.9       | 3.8       | 7.6       | 2.4       |
|                                   |      | VEL (MPH) |
|                                   |      | 8.1       | 10.2      | 4.9       | 6.6       | 6.5       | 8.8       | 8.5       | 6.0       | 9.9       | 4.5       |
|                                   |      | SPD (MPH) |
|                                   |      | 0.772     | 0.781     | 0.279     | 0.727     | 0.468     | 0.920     | 0.819     | 0.637     | 0.768     | 0.541     |
|                                   |      | RATIO     |
| METEOROLOGICAL SITE<br>BRIDGEPORT |      | 170       | 260       | 250       | 300       | 110       | 300       | 230       | 50        | 260       | 280       |
|                                   |      | DIR (DEG) |
|                                   |      | 1.4       | 8.2       | 6.7       | 3.5       | 5.4       | 3.2       | 5.5       | 1.2       | 7.6       | 3.6       |
|                                   |      | VEL (MPH) |
|                                   |      | 4.6       | 8.3       | 6.9       | 5.8       | 5.5       | 4.0       | 5.6       | 5.2       | 8.2       | 6.0       |
|                                   |      | SPD (MPH) |
|                                   |      | 0.306     | 0.979     | 0.967     | 0.602     | 0.987     | 0.785     | 0.974     | 0.230     | 0.931     | 0.603     |
|                                   |      | RATIO     |
| METEOROLOGICAL SITE<br>WORCESTER  |      | 210       | 260       | 280       | 300       | 140       | 290       | 260       | 80        | 250       | 280       |
|                                   |      | DIR (DEG) |
|                                   |      | 5.0       | 9.3       | 6.6       | 4.0       | 3.6       | 6.3       | 6.3       | 2.8       | 11.1      | 4.9       |
|                                   |      | VEL (MPH) |
|                                   |      | 5.8       | 9.3       | 7.0       | 4.2       | 3.6       | 6.6       | 6.8       | 4.6       | 11.2      | 5.3       |
|                                   |      | SPD (MPH) |
|                                   |      | 0.864     | 0.997     | 0.932     | 0.957     | 0.992     | 0.954     | 0.934     | 0.600     | 0.989     | 0.922     |
|                                   |      | RATIO     |
| WATERBURY-007 (0059)              |      | 81        | 59        | 47        | 46        | 45        | 45        | 44        | 44        | 43        | 43        |
|                                   |      | PM10      |
|                                   |      | DATE      |
|                                   |      | 1/17/90   | 11/1/90   | 2/16/90   | 1/23/90   | 12/13/90  | 7/4/90    | 9/2/90    | 12/1/90   | 12/7/90   | 8/27/90   |
| METEOROLOGICAL SITE<br>NEWARK     |      | 190       | 200       | 50        | 270       | 280       | 230       | 280       | 250       | 330       | 340       |
|                                   |      | DIR (DEG) |
|                                   |      | 5.8       | 2.7       | 3.1       | 4.8       | 9.0       | 14.0      | 4.8       | 7.7       | 1.7       | 5.0       |
|                                   |      | VEL (MPH) |
|                                   |      | 6.3       | 5.5       | 5.3       | 8.9       | 11.9      | 16.2      | 7.2       | 8.8       | 5.0       | 7.2       |
|                                   |      | SPD (MPH) |
|                                   |      | 0.912     | 0.501     | 0.578     | 0.538     | 0.750     | 0.861     | 0.670     | 0.884     | 0.334     | 0.694     |
|                                   |      | RATIO     |
| METEOROLOGICAL SITE<br>BRADLEY    |      | 180       | 80        | 20        | 220       | 280       | 220       | 240       | 190       | 330       | 320       |
|                                   |      | DIR (DEG) |
|                                   |      | 6.2       | .6        | 1.2       | 2.4       | 5.1       | 8.0       | 1.4       | 7.6       | 1.6       | 4.8       |
|                                   |      | VEL (MPH) |
|                                   |      | 8.1       | 3.3       | 3.2       | 4.5       | 9.3       | 10.2      | 4.9       | 9.9       | 4.3       | 6.6       |
|                                   |      | SPD (MPH) |
|                                   |      | 0.772     | 0.183     | 0.377     | 0.541     | 0.541     | 0.781     | 0.279     | 0.768     | 0.375     | 0.727     |
|                                   |      | RATIO     |
| METEOROLOGICAL SITE<br>BRIDGEPORT |      | 170       | 260       | 140       | 280       | 290       | 260       | 250       | 260       | 100       | 300       |
|                                   |      | DIR (DEG) |
|                                   |      | 1.4       | 1.9       | 1.0       | 3.6       | 7.1       | 8.2       | 6.7       | 7.6       | 1.3       | 3.5       |
|                                   |      | VEL (MPH) |
|                                   |      | 4.6       | 3.9       | 2.7       | 6.0       | 8.1       | 8.3       | 6.9       | 8.2       | 2.7       | 5.8       |
|                                   |      | SPD (MPH) |
|                                   |      | 0.306     | 0.489     | 0.383     | 0.603     | 0.876     | 0.979     | 0.967     | 0.931     | 0.466     | 0.602     |
|                                   |      | RATIO     |
| METEOROLOGICAL SITE<br>WORCESTER  |      | 210       | 280       | 10        | 280       | 270       | 260       | 280       | 250       | 260       | 300       |
|                                   |      | DIR (DEG) |
|                                   |      | 5.0       | 5.9       | 1.9       | 4.9       | 8.9       | 9.3       | 6.6       | 11.1      | 3.4       | 4.0       |
|                                   |      | VEL (MPH) |
|                                   |      | 5.8       | 6.2       | 2.4       | 5.3       | 10.4      | 9.3       | 7.0       | 11.2      | 4.3       | 4.2       |
|                                   |      | SPD (MPH) |
|                                   |      | 0.864     | 0.960     | 0.779     | 0.922     | 0.858     | 0.997     | 0.932     | 0.989     | 0.794     | 0.957     |
|                                   |      | RATIO     |

TABLE 2-5, CONTINUED

1990 TEN HIGHEST 24-HOUR AVERAGE PM10 DAYS WITH WIND DATA

UNITS : MICROGRAMS PER CUBIC METER

| TOWN-SITE (SAMPLES)   | RANK | 1       | 2       | 3      | 4       | 5       | 6       | 7       | 8       | 9        | 10      |
|-----------------------|------|---------|---------|--------|---------|---------|---------|---------|---------|----------|---------|
| WATERBURY-123 (0059)  |      | 81      | 77      | 65     | 64      | 59      | 59      | 52      | 48      | 46       | 46      |
| METEOROLOGICAL SITE   |      | 6/28/90 | 1/17/90 | 8/3/90 | 6/22/90 | 8/27/90 | 2/16/90 | 11/1/90 | 7/16/90 | 1/23/90  | 7/4/90  |
| NEWARK                |      | 260     | 190     | 170    | 200     | 340     | 50      | 200     | 260     | 270      | 230     |
|                       |      | 2.4     | 5.8     | 1.0    | 6.4     | 5.0     | 3.1     | 2.7     | 7.2     | 4.8      | 14.0    |
|                       |      | 5.2     | 6.3     | 4.2    | 8.3     | 7.2     | 5.3     | 5.5     | 9.2     | 8.9      | 16.2    |
|                       |      | 0.464   | 0.912   | 0.233  | 0.773   | 0.694   | 0.578   | 0.501   | 0.788   | 0.538    | 0.861   |
| METEOROLOGICAL SITE   |      | 320     | 180     | 290    | 210     | 320     | 20      | 80      | 280     | 220      | 220     |
| BRADLEY               |      | 6.9     | 6.2     | 2.5    | 6.9     | 4.8     | 1.2     | 6       | 6.6     | 2.4      | 8.0     |
|                       |      | 7.5     | 8.1     | 5.0    | 8.5     | 6.6     | 3.2     | 3.3     | 9.9     | 4.5      | 10.2    |
|                       |      | 0.926   | 0.772   | 0.492  | 0.819   | 0.727   | 0.377   | 0.183   | 0.663   | 0.541    | 0.781   |
| METEOROLOGICAL SITE   |      | 260     | 170     | 240    | 230     | 300     | 140     | 260     | 270     | 280      | 260     |
| BRIDGEPORT            |      | 5.2     | 1.4     | 5.0    | 5.5     | 3.5     | 1.0     | 1.9     | 7.7     | 3.6      | 8.2     |
|                       |      | 5.9     | 4.6     | 5.0    | 5.6     | 5.8     | 2.7     | 3.9     | 8.1     | 6.0      | 8.3     |
|                       |      | 0.883   | 0.306   | 0.996  | 0.974   | 0.602   | 0.383   | 0.489   | 0.954   | 0.603    | 0.979   |
| METEOROLOGICAL SITE   |      | 300     | 210     | 300    | 260     | 300     | 10      | 280     | 270     | 290      | 260     |
| WORCESTER             |      | 7.0     | 5.0     | 5.6    | 6.3     | 4.0     | 1.9     | 5.9     | 7.2     | 4.9      | 9.3     |
|                       |      | 7.5     | 5.8     | 5.9    | 6.8     | 4.2     | 2.4     | 6.2     | 7.8     | 5.3      | 9.3     |
|                       |      | 0.934   | 0.864   | 0.944  | 0.934   | 0.957   | 0.779   | 0.960   | 0.929   | 0.922    | 0.997   |
| WATERFORD-001 (0055)  |      | 49      | 46      | 43     | 40      | 39      | 37      | 37      | 31      | 29       | 26      |
| METEOROLOGICAL SITE   |      | 6/16/90 | 6/22/90 | 7/4/90 | 1/17/90 | 9/2/90  | 6/28/90 | 8/27/90 | 8/21/90 | 7/16/90  | 4/23/90 |
| NEWARK                |      | 120     | 200     | 230    | 190     | 280     | 260     | 340     | 20      | 260      | 360     |
|                       |      | 2.7     | 6.4     | 14.0   | 5.8     | 4.8     | 2.4     | 5.0     | 11.1    | 7.2      | 6.2     |
|                       |      | 4.9     | 8.3     | 16.2   | 6.3     | 7.2     | 5.2     | 7.2     | 11.4    | 9.2      | 7.9     |
|                       |      | 0.562   | 0.773   | 0.861  | 0.912   | 0.670   | 0.464   | 0.694   | 0.976   | 0.788    | 0.786   |
| METEOROLOGICAL SITE   |      | 170     | 210     | 220    | 180     | 240     | 320     | 320     | 20      | 280      | 10      |
| BRADLEY               |      | 2.9     | 6.9     | 8.0    | 6.2     | 1.4     | 6.9     | 4.8     | 8.8     | 6.6      | 6.9     |
|                       |      | 5.9     | 8.5     | 10.2   | 8.1     | 4.9     | 7.5     | 6.6     | 9.3     | 9.9      | 8.8     |
|                       |      | 0.489   | 0.819   | 0.781  | 0.772   | 0.279   | 0.926   | 0.727   | 0.939   | 0.663    | 0.784   |
| METEOROLOGICAL SITE   |      | 140     | 230     | 260    | 170     | 250     | 260     | 300     | 70      | 270      | 10      |
| BRIDGEPORT            |      | 3.2     | 5.5     | 8.2    | 1.4     | 6.7     | 5.2     | 3.5     | 8.3     | 7.7      | 7.2     |
|                       |      | 3.2     | 5.6     | 8.3    | 4.6     | 6.9     | 5.9     | 5.8     | 8.6     | 8.1      | 8.1     |
|                       |      | 0.997   | 0.974   | 0.979  | 0.306   | 0.967   | 0.883   | 0.602   | 0.963   | 0.954    | 0.890   |
| METEOROLOGICAL SITE   |      | 170     | 260     | 260    | 210     | 280     | 300     | 300     | 60      | 270      | 360     |
| WORCESTER             |      | 3.0     | 6.3     | 9.3    | 5.0     | 6.6     | 7.0     | 4.0     | 4.8     | 7.2      | 6.4     |
|                       |      | 3.0     | 6.8     | 9.3    | 5.8     | 7.0     | 7.5     | 4.2     | 4.9     | 7.8      | 8.2     |
|                       |      | 0.989   | 0.934   | 0.997  | 0.864   | 0.932   | 0.934   | 0.957   | 0.991   | 0.929    | 0.785   |
| WEST HAVEN-003 (0057) |      | 68      | 47      | 44     | 44      | 44      | 43      | 43      | 40      | 39       | 39      |
| METEOROLOGICAL SITE   |      | 1/17/90 | 7/4/90  | 9/2/90 | 11/1/90 | 6/28/90 | 8/27/90 | 1/23/90 | 6/22/90 | 12/13/90 | 12/7/90 |
| NEWARK                |      | 190     | 230     | 280    | 200     | 260     | 340     | 270     | 200     | 280      | 330     |
|                       |      | 5.8     | 14.0    | 4.8    | 2.7     | 2.4     | 5.0     | 4.8     | 6.4     | 9.0      | 1.7     |
|                       |      | 6.3     | 16.2    | 7.2    | 5.5     | 5.2     | 7.2     | 8.9     | 8.3     | 11.9     | 5.0     |
|                       |      | 0.912   | 0.861   | 0.670  | 0.501   | 0.464   | 0.694   | 0.538   | 0.773   | 0.750    | 0.334   |
| METEOROLOGICAL SITE   |      | 180     | 220     | 240    | 80      | 320     | 320     | 220     | 210     | 280      | 330     |
| BRADLEY               |      | 6.2     | 8.0     | 1.4    | 6       | 6.9     | 4.8     | 2.4     | 6.9     | 5.1      | 1.6     |
|                       |      | 8.1     | 10.2    | 4.9    | 3.3     | 7.5     | 6.6     | 4.5     | 8.5     | 9.3      | 4.3     |
|                       |      | 0.772   | 0.781   | 0.279  | 0.183   | 0.926   | 0.727   | 0.541   | 0.819   | 0.541    | 0.375   |

TABLE 2-5, CONTINUED

1990 TEN HIGHEST 24-HOUR AVERAGE PM10 DAYS WITH WIND DATA

UNITS : MICROGRAMS PER CUBIC METER

| TOWN-SITE (SAMPLES)               | RANK      | 1       | 2      | 3      | 4       | 5       | 6       | 7       | 8       | 9       | 10      |
|-----------------------------------|-----------|---------|--------|--------|---------|---------|---------|---------|---------|---------|---------|
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG) | 170     | 260    | 250    | 260     | 260     | 300     | 280     | 230     | 290     | 100     |
|                                   | VEL (MPH) | 1.4     | 8.2    | 6.7    | 1.9     | 5.2     | 3.5     | 3.6     | 5.5     | 7.1     | 1.3     |
|                                   | SPD (MPH) | 4.6     | 8.3    | 6.9    | 3.9     | 5.9     | 5.8     | 6.0     | 5.6     | 8.1     | 2.7     |
|                                   | RATIO     | 0.306   | 0.979  | 0.967  | 0.489   | 0.883   | 0.602   | 0.603   | 0.974   | 0.876   | 0.466   |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG) | 210     | 260    | 280    | 280     | 300     | 300     | 280     | 260     | 270     | 260     |
|                                   | VEL (MPH) | 5.0     | 9.3    | 6.6    | 5.9     | 7.0     | 4.0     | 4.9     | 6.3     | 8.9     | 3.4     |
|                                   | SPD (MPH) | 5.8     | 9.3    | 7.0    | 6.2     | 7.5     | 4.2     | 5.3     | 6.8     | 10.4    | 4.3     |
|                                   | RATIO     | 0.864   | 0.997  | 0.932  | 0.960   | 0.934   | 0.957   | 0.922   | 0.934   | 0.858   | 0.794   |
| WILLIMANTIC-002 (0060)            | PM10      | 48      | 41     | 35     | 33      | 32      | 31      | 31      | 30      | 28      | 27      |
|                                   | DATE      | 1/17/90 | 7/4/90 | 9/2/90 | 7/22/90 | 8/27/90 | 12/7/90 | 9/14/90 | 11/1/90 | 12/1/90 | 1/23/90 |
| METEOROLOGICAL SITE<br>NEWARK     | DIR (DEG) | 190     | 230    | 280    | 110     | 340     | 330     | 140     | 200     | 250     | 270     |
|                                   | VEL (MPH) | 5.8     | 14.0   | 4.8    | 2.4     | 5.0     | 1.7     | 6.6     | 2.7     | 7.7     | 4.8     |
|                                   | SPD (MPH) | 6.3     | 16.2   | 7.2    | 5.0     | 7.2     | 5.0     | 7.5     | 5.5     | 8.8     | 8.9     |
|                                   | RATIO     | 0.912   | 0.861  | 0.670  | 0.486   | 0.694   | 0.334   | 0.881   | 0.501   | 0.864   | 0.538   |
| METEOROLOGICAL SITE<br>BRADLEY    | DIR (DEG) | 180     | 220    | 240    | 130     | 320     | 330     | 160     | 80      | 190     | 220     |
|                                   | VEL (MPH) | 6.2     | 8.0    | 1.4    | 3.0     | 4.8     | 1.6     | 5.5     | .6      | 7.6     | 2.4     |
|                                   | SPD (MPH) | 8.1     | 10.2   | 4.9    | 6.5     | 6.6     | 4.3     | 8.1     | 3.3     | 9.9     | 4.5     |
|                                   | RATIO     | 0.772   | 0.781  | 0.279  | 0.468   | 0.727   | 0.375   | 0.681   | 0.183   | 0.768   | 0.541   |
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG) | 170     | 260    | 250    | 110     | 300     | 100     | 160     | 260     | 260     | 280     |
|                                   | VEL (MPH) | 1.4     | 8.2    | 6.7    | 5.4     | 3.5     | 1.3     | 6.1     | 1.9     | 7.6     | 3.6     |
|                                   | SPD (MPH) | 4.6     | 8.3    | 6.9    | 5.5     | 5.8     | 2.7     | 6.6     | 3.9     | 8.2     | 6.0     |
|                                   | RATIO     | 0.306   | 0.979  | 0.967  | 0.987   | 0.602   | 0.466   | 0.922   | 0.489   | 0.931   | 0.603   |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG) | 210     | 260    | 280    | 140     | 300     | 260     | 170     | 280     | 250     | 280     |
|                                   | VEL (MPH) | 5.0     | 9.3    | 6.6    | 3.6     | 4.0     | 3.4     | 4.3     | 5.9     | 11.1    | 4.9     |
|                                   | SPD (MPH) | 5.8     | 9.3    | 7.0    | 3.6     | 4.2     | 4.3     | 4.3     | 6.2     | 11.2    | 5.3     |
|                                   | RATIO     | 0.864   | 0.997  | 0.932  | 0.992   | 0.957   | 0.794   | 0.989   | 0.960   | 0.989   | 0.922   |

**TABLE 2-6**

**PM10 TRENDS: 1985-1990**

**(PAIRED t TEST)**

| PAIRED YEARS | AVERAGE OF ANNUAL GEOMETRIC MEANS (µg/m <sup>3</sup> ) | NO. OF SITES <sup>1</sup> | DIFFERENCES OF THE PAIRED YEAR MEANS |           | SIGNIFICANCE LEVEL <sup>1</sup> |           |  |
|--------------|--|---------------------------|--------------------------------------|-----------|---------------------------------|-----------|--|
|              |  |                           | AVG.                                 | STD. DEV. | TREND AT                        |           | PROBABILITY THAT CHANGE IS NOT SIGNIFICANT |
|              |  |                           |                                      |           | 95% LEVEL                       | 99% LEVEL |  |
| 85<br>86     | 36.3<br>35.2   | 2<br>2                    | -1.10                                | 0.57      | N.C.                            | N.C.      | 0.2220                                     |
| 86<br>87     | 37.7<br>34.0   | 5<br>5                    | -3.72                                | 2.03      | ↓                               | N.C.      | 0.0148                                     |
| 87<br>88     | 37.8<br>32.3   | 3<br>3                    | -5.50                                | 4.20      | N.C.                            | N.C.      | 0.1514                                     |
| 88<br>89     | 32.3<br>31.9   | 3<br>3                    | -0.40                                | 0.87      | N.C.                            | N.C.      | 0.4808                                     |
| 89<br>90     | 22.4<br>20.1   | 37<br>37                  | -2.38                                | 1.35      | ↓                               | ↓         | 0.0001                                     |

Key to Symbols :    ↓ = Significant downward trend  
                           ↑ = Significant upward trend  
                           N.C. = No significant change

<sup>1</sup> When the number of paired sites is small, the results should be interpreted with caution.

### III. SULFUR DIOXIDE

#### HEALTH EFFECTS

Sulfur oxides are heavy, pungent, yellowish gases that come from the burning of sulfur-containing fuel, mainly coal and oil-derived fuels, and also from the smelting of metals and from certain industrial processes. They have a distinctive odor. Sulfur dioxide (SO<sub>2</sub>) comprises about 95 percent of these gases, so scientists use a test for SO<sub>2</sub> alone as a measure of all sulfur oxides.

Exposure to high levels of sulfur oxides can cause an obstruction of breathing that doctors call "pulmonary flow resistance." The amount of breathing obstruction has a direct relation to the amount of sulfur compounds in the air. Moreover, the effect of sulfur pollution is enhanced by the presence of other pollutants, especially particulates and oxidants. The action of two or more pollutants is synergistic: each pollutant augments the other and the combined effect is greater than the sum of the effects that each alone would have.

Many types of respiratory disease are associated with sulfur oxides: coughs and colds, asthma, bronchitis, and emphysema. Some researchers believe that the harm is due not only to the sulfur oxide gases but also to other sulfur compounds that accompany the oxides.

#### CONCLUSIONS

Sulfur dioxide concentrations in 1990 did not exceed any federal primary or secondary standards. Measured concentrations were substantially below the 365 µg/m<sup>3</sup> primary 24-hour standard and well below both the 80 µg/m<sup>3</sup> primary annual standard and the 1300 µg/m<sup>3</sup> secondary 3-hour standard.

#### METHOD OF MEASUREMENT

The DEP Air Monitoring Unit used the pulsed fluorescence method (Teco instruments) to continuously measure sulfur dioxide levels at all 16 sites in 1990.

#### DISCUSSION OF DATA

**Monitoring Network** - Sixteen continuous SO<sub>2</sub> monitors were used to record data in 13 towns during 1990 (see Figure 3-1):

|                   |                 |
|-------------------|-----------------|
| Bridgeport 012    | Hartford 018    |
| Bridgeport 013    | Milford 010     |
| Danbury 123       | New Britain 011 |
| East Hartford 006 | New Haven 123   |
| East Haven 003    | Stamford 025    |
| Enfield 005       | Stamford 123    |
| Greenwich 017     | Waterbury 008   |
| Groton 007        | Waterbury 123   |

All of these sites telemetered their data to the central computer in Hartford three times each day (i.e., at 0700, 1400, and 2400 hours).

**Precision and Accuracy** - 580 precision checks were made on SO<sub>2</sub> monitors in 1990, yielding 95% probability limits ranging from -6% to +5%. Accuracy is determined by introducing a known amount of SO<sub>2</sub> into each of the monitors. Three different concentration levels are tested: low, medium, and high. The 95% probability limits for accuracy based on 17 audits were: low, -12% to +9%; medium, -9% to +8%; and high, -8% to +7%.

**Annual Averages** - SO<sub>2</sub> levels were below the primary annual standard of 80 µg/m<sup>3</sup> at all sites in 1990 (see Table 3-1). The annual average SO<sub>2</sub> levels decreased at 12 of the 14 monitoring sites that had adequate data in both 1989 and 1990 to produce valid annual averages. The largest decrease was 8 µg/m<sup>3</sup>, which occurred at Waterbury 008. No change was evident at Groton 007 and Waterbury 123.

**Statistical Projections** - A statistical analysis of the sulfur dioxide data is presented in Table 3-2. This analysis is produced by a DEP computer program and provides information to compensate for any loss of data caused by instrumentation problems. The format of Table 3-2 is the same as that used to present the statistical projections for particulate matter (see Table 2-1). Since the statistical projections are made for the 24-hour standard, the hourly SO<sub>2</sub> data are first converted to 24-hour block averages. These 24-hour "samples" form the basis for the annual arithmetic and geometric means and the arithmetic and geometric standard deviations employed by the DEP computer program to make the statistical projections and calculate the 95% confidence limits.

The data indicate that there were no violations of the primary SO<sub>2</sub> standard at any site in Connecticut in the last three years. However, statistical predictions of one day exceeding the primary 24-hour standard of 365 µg/m<sup>3</sup> did occur during this period at New Haven 017 in 1988. This implies that a slight increase in SO<sub>2</sub> emissions might have jeopardized the attainment of the standard at this site. Two days over the standard are required for the standard to be violated at a site.

The annual averages in Table 3-2 differ slightly from those in Table 3-1 due to the manner in which they were derived. The averages in Table 3-1 are based on the available hourly readings, while those in Table 3-2 are based on valid calendar day 24-hour averages. (At least 18 hourly readings are required to produce a valid 24-hour average.)

**24-Hour Averages** - Figure 3-2 presents the first and second high calendar day average concentrations recorded at each monitoring site in 1990. No site recorded SO<sub>2</sub> levels in excess of the 24-hour primary standard of 365 µg/m<sup>3</sup>. Second high calendar day SO<sub>2</sub> average concentrations decreased at 12 of the 14 monitoring sites that had a sufficient distribution and quantity of data in both 1989 and 1990. The decreases ranged from 1 µg/m<sup>3</sup> at Stamford 025 to 85 µg/m<sup>3</sup> at New Haven 123. Increases in the second high concentration were experienced at Bridgeport 013 and Groton 007 and were less than 10 µg/m<sup>3</sup>.

Current EPA policy bases compliance with the primary 24-hour SO<sub>2</sub> standard on calendar day averages. Assessment of compliance is based on the second highest calendar day average in the year. Running averages are averages computed for the 24-hour periods ending at every hour. If running averages were used, assessment of compliance would be based on the value of the second highest of the two highest non-overlapping 24-hour periods in the year. There has been some contention over which average is the more appropriate one on which to base compliance. Table 3-3 contains the two highest 24-hour SO<sub>2</sub> readings at each site in terms of both the running averages and the calendar day averages. The first high 24-hour running averages are all larger than the first high calendar day averages except at Greenwich 017 where it was the same. The differences vary in magnitude up to 25 µg/m<sup>3</sup>, which occurred at Waterbury 123.

**3-Hour Averages** - Figure 3-3 presents the first and second high 3-hour concentrations recorded at each monitoring site. Measured SO<sub>2</sub> concentrations were far below the federal secondary 3-hour standard of 1300 µg/m<sup>3</sup> at all DEP monitoring sites in 1990. Of the 14 sites that had a sufficient

distribution and quantity of data in both 1989 and 1990, 13 had lower second high concentrations in 1990. The decreases ranged from 1  $\mu\text{g}/\text{m}^3$  at Groton 007 to 292  $\mu\text{g}/\text{m}^3$  at New Haven 123. Bridgeport 012 had a second high concentration in 1990 that was higher than 1989 by 18  $\mu\text{g}/\text{m}^3$ .

**10-High Days with Wind Data** - Table 3-4 lists the ten highest 24-hour calendar day  $\text{SO}_2$  averages and the dates of occurrence for each  $\text{SO}_2$  site in Connecticut in 1990. Only those 15 sites were used which had a sufficient distribution and quantity of data to produce a valid annual average in 1990. The table also shows the average wind conditions that occurred on each of these dates. (The origin and use of these wind data are described in the discussion of Table 2-5 in the particulate matter section of this Air Quality Summary.)

Once again, as with particulate matter, many (i.e., 70%) of the highest  $\text{SO}_2$  days occurred with winds out of the southwest quadrant, and most of these days had relatively persistent winds. This relationship is caused, at least in part, by  $\text{SO}_2$  transport, but any transport is limited by the chemical instability of  $\text{SO}_2$ . In the atmosphere,  $\text{SO}_2$  reacts with other gases to produce, among other things, sulfate particulates. Therefore,  $\text{SO}_2$  is not likely to be transported very long distances. Previous studies conducted by the DEP have shown that, during periods of southwest winds, levels of  $\text{SO}_2$  in Connecticut decrease with distance from the New York City metropolitan area. This relationship tends to support the transport hypothesis. On the other hand, these studies also revealed that certain meteorological parameters, most notably mixing height and wind speed, are more conducive to high  $\text{SO}_2$  levels on days when there are southwesterly winds than on other days.

The data in Table 3-4 also suggest another reason for high  $\text{SO}_2$  levels. Approximately 86% of the tabulated days occurred during the winter, and 13% occurred in late autumn. This phenomenon can be attributed to the fact that more fuel oil is burned during cold weather resulting in greater  $\text{SO}_2$  emissions.

In summary, high levels of  $\text{SO}_2$  in Connecticut seem to be caused by a number of related factors. First, Connecticut experiences its highest  $\text{SO}_2$  levels during the late fall and winter months, when there is an increased amount of fuel combustion. Second, the New York City metropolitan area, a large emission source, is located to the southwest of Connecticut, and southwest winds occur relatively often in this region in comparison to other wind directions. Also, adverse meteorological conditions are often associated with southwest winds. The net effect is that during the colder months when a persistent southwesterly wind occurs, an air mass picks up increased amounts of  $\text{SO}_2$  over the New York City metropolitan area and transports this  $\text{SO}_2$  into Connecticut, where the  $\text{SO}_2$  levels are already relatively high. In addition, relatively low mixing heights are associated with warm air advection (i.e., southwest wind flow), which inhibits vertical mixing and contributes to the enhanced  $\text{SO}_2$  concentrations.

The levels of transported  $\text{SO}_2$  eventually decline with increasing distance from New York City, as the  $\text{SO}_2$  is dispersed and as it slowly reacts to produce sulfate particulates. These sulfate particulates may fall to the ground in either a dry state (dry deposition) or in a wet state after combination with water droplets (wet deposition or "acid rain").

**Trends** - In order to perform a valid trend analysis, the data for the period of interest must be adequate, reliable and from similar sampling methods. Up until 1978, the only monitoring method for  $\text{SO}_2$  that was thought to consistently fit these criteria was the sulfation plate. Between 1978 and 1982 there were approximately three times as much sulfation rate data as continuous  $\text{SO}_2$  data and the former method was used for the purpose of analyzing  $\text{SO}_2$  trends. However, available information now indicates that sulfation rate-derived  $\text{SO}_2$  values may not be as accurate as once thought. Sulfation rate data are dependent on relative humidity and wind speed -- being extremely sensitive to the latter -- and the precision of the data suffers even under uniform conditions. Furthermore, EPA has requested that DEP use continuous  $\text{SO}_2$  data in order to analyze  $\text{SO}_2$  trends. Consequently, the  $\text{SO}_2$  trend analysis now uses only continuous  $\text{SO}_2$  data. The results are summarized in Figure 3-4 and Table 3-5. (For a discussion of the paired  $t$  test used in Table 3-5, see the discussion of Table 2-6 in the particulate matter section of this Air Quality Summary.)

In response to the skyrocketing prices of low sulfur fuels in the late 1970's, most states relaxed their sulfur-in-fuel requirements to the full extent the law allowed, creating considerable pressure on Connecticut to follow suit. This caused Connecticut to reevaluate its philosophy for controlling sulfur oxide emissions in 1981. To meet the challenge of increased costs of fuel in the economy, DEP restructured its air pollution control requirements for fuel burning sources. Under this new "three-pronged" program, Connecticut's businesses and industries are (1) now allowed (effective November 1981) to burn a less expensive grade of oil with a higher sulfur content -- one percent (1.0%) sulfur oil, and (2) allowed to burn higher sulfur content oil in exchange for reductions in energy use. The third aspect of the program was the repeal of the 24-hour secondary air quality standard for sulfur oxides.

This action increased statewide allowable sulfur oxide emissions by almost 60%. Sulfur oxide emissions were not doubled by going from 0.5% to 1.0% sulfur-in-fuel since residential fuel users, which account for almost one-third of annual statewide sulfur oxide emissions, use distillate fuel oil with a sulfur content of less than 0.5%. Nevertheless, given this increase in allowable SO<sub>2</sub> emissions, one would have expected measured SO<sub>2</sub> levels to increase in 1982 and subsequent years, as compared to 1981. However, no significant trend was apparent in 1982; SO<sub>2</sub> levels actually declined in 1983; and since 1983, there has been no significant change in SO<sub>2</sub> levels until 1990 (see Table 3-5). This development may be attributable to year-to-year fluctuations in meteorology or decreased fuel use caused by increased fuel prices and/or increased fuel efficiency (i.e., 'tighter' buildings).

The long-term trend of SO<sub>2</sub> concentrations is shown in graphical form in Figure 3-4. An improvement in SO<sub>2</sub> levels is demonstrated by the decrease over time of concentrations in excess of 30 µg/m<sup>3</sup>. The year-to-year trends in ambient SO<sub>2</sub> levels are illustrated in Table 3-5 and show significant changes only from 1982 to 1983 and from 1989 to 1990.

The results of continuous SO<sub>2</sub> monitoring indicate that sulfur dioxide levels in 1990 were significantly lower than those in 1989 (see Table 3-5). Temperature is an important factor in determining SO<sub>2</sub> emissions. The change in measured SO<sub>2</sub> levels may have been due to the fact that for Connecticut 1990 was appreciably cooler than 1989. This is normally reflected in the number of "degree days" -- a measure of heating requirement (see Tables 9-1 and 9-2). As the number of degree days decreases, the amount of fuel that must be burned to heat buildings also decreases. Consequently, as less fuel is burned, the emissions of sulfur dioxide are proportionately decreased. There was approximately a 3% decrease in degrees days for Connecticut from 1989 to 1990.



## TABLE 3-1

### 1990 ANNUAL ARITHMETIC AVERAGES OF SULFUR DIOXIDE

(PRIMARY STANDARD: 80  $\mu\text{g}/\text{m}^3$ )

| <u>TOWN-SITE</u>  | <u>SITE NAME</u>          | <u>ANNUAL AVG</u><br>( $\mu\text{g}/\text{m}^3$ ) |
|-------------------|---------------------------|---|
| Bridgeport 012    | Edison School             | 33  |
| Bridgeport 013    | Hallett Street            | 25  |
| Danbury 123       | Western CT State College  | 19  |
| East Hartford 006 | High Street               | 21  |
| East Haven 003    | Animal Shelter            | 19  |
| Enfield 005       | Department of Corrections | 16  |
| Greenwich 017     | Greenwich Point Park      | 12  |
| Groton 007        | Fire Headquarters         | 20  |
| Hartford 018      | Sheldon Street            | 24  |
| Milford 010       | Devon Community Center    | 23*   |
| New Britain 011   | Armory                    | 21  |
| New Haven 123     | State Street              | 36  |
| Stamford 025      | Recreation Center         | 22  |
| Stamford 123      | Health Department         | 23  |
| Waterbury 008     | Armory                    | 22  |
| Waterbury 123     | Bank Street               | 25  |

\* A valid annual average cannot be calculated because either the sampling was not random or the number of observations does not satisfy the minimum sampling criteria.

TABLE 3-2

## 1988-1990 SO2 ANNUAL AVERAGES AND STATISTICAL PROJECTIONS

| TOWN NAME     | SITE | YEAR | SAMPLES | ARITHMETIC 95-PCT-LIMITS |       |       | STANDARD DEVIATION | PREDICTED DAYS OVER 365 UG/M3 |
|---------------|------|------|---------|--------------------------|-------|-------|--------------------|-------------------------------|
|               |      |      |         | MEAN                     | LOWER | UPPER |                    |                               |
| BRIDGEPORT    | 012  | 1988 | 363     | 35.5                     | 35.3  | 35.7  | 28.269             |                               |
|               | 012  | 1989 | 362     | 35.8                     | 35.5  | 36.0  | 26.908             |                               |
|               | 012  | 1990 | 358     | 32.9                     | 32.5  | 33.3  | 27.329             |                               |
| BRIDGEPORT    | 013  | 1988 | 363     | 28.1                     | 27.9  | 28.3  | 23.821             |                               |
|               | 013  | 1989 | 348     | 26.0                     | 25.5  | 26.4  | 19.517             |                               |
|               | 013  | 1990 | 362     | 25.5                     | 25.3  | 25.7  | 20.468             |                               |
| DANBURY       | 123  | 1988 | 341     | 23.1                     | 22.6  | 23.7  | 20.905             |                               |
|               | 123  | 1989 | 362     | 22.1                     | 21.9  | 22.2  | 17.365             |                               |
|               | 123  | 1990 | 345     | 19.4                     | 19.0  | 19.8  | 16.290             |                               |
| EAST HARTFORD | 006  | 1989 | 139*    | 27.5                     | 24.7  | 30.2  | 21.076             |                               |
|               | 006  | 1990 | 364     | 21.0                     | 20.9  | 21.1  | 17.149             |                               |
| EAST HAVEN    | 003  | 1988 | 347     | 25.0                     | 24.5  | 25.6  | 24.503             |                               |
|               | 003  | 1989 | 349     | 22.2                     | 21.7  | 22.7  | 22.662             |                               |
|               | 003  | 1990 | 365     | 18.8                     | 18.8  | 18.8  | 16.076             |                               |
| ENFIELD       | 005  | 1988 | 344     | 18.9                     | 18.5  | 19.4  | 16.213             |                               |
|               | 005  | 1989 | 356     | 17.4                     | 17.2  | 17.7  | 13.374             |                               |
|               | 005  | 1990 | 352     | 15.6                     | 15.3  | 15.8  | 11.994             |                               |
| GREENWICH     | 017  | 1988 | 356     | 16.1                     | 15.9  | 16.3  | 12.034             |                               |
|               | 017  | 1989 | 360     | 15.8                     | 15.7  | 16.0  | 13.551             |                               |
|               | 017  | 1990 | 364     | 12.5                     | 12.4  | 12.6  | 10.371             |                               |
| GROTON        | 007  | 1988 | 357     | 22.7                     | 22.4  | 22.9  | 16.958             |                               |
|               | 007  | 1989 | 341     | 19.9                     | 19.6  | 20.2  | 12.749             |                               |
|               | 007  | 1990 | 357     | 20.4                     | 20.1  | 20.6  | 14.369             |                               |
| HARTFORD      | 018  | 1989 | 339     | 27.5                     | 26.9  | 28.0  | 19.595             |                               |
|               | 018  | 1990 | 362     | 24.2                     | 24.0  | 24.4  | 18.618             |                               |

\* THE RANDOMNESS OR QUANTITY OF DATA IS NOT SUFFICIENT FOR REPRESENTATIVE ANNUAL STATISTICS.

N.B. THE ARITHMETIC MEAN AND STANDARD DEVIATION HAVE UNITS OF MICROGRAMS PER CUBIC METER.

TABLE 3-2, CONTINUED  
 1988-1990 SO2 ANNUAL AVERAGES AND STATISTICAL PROJECTIONS

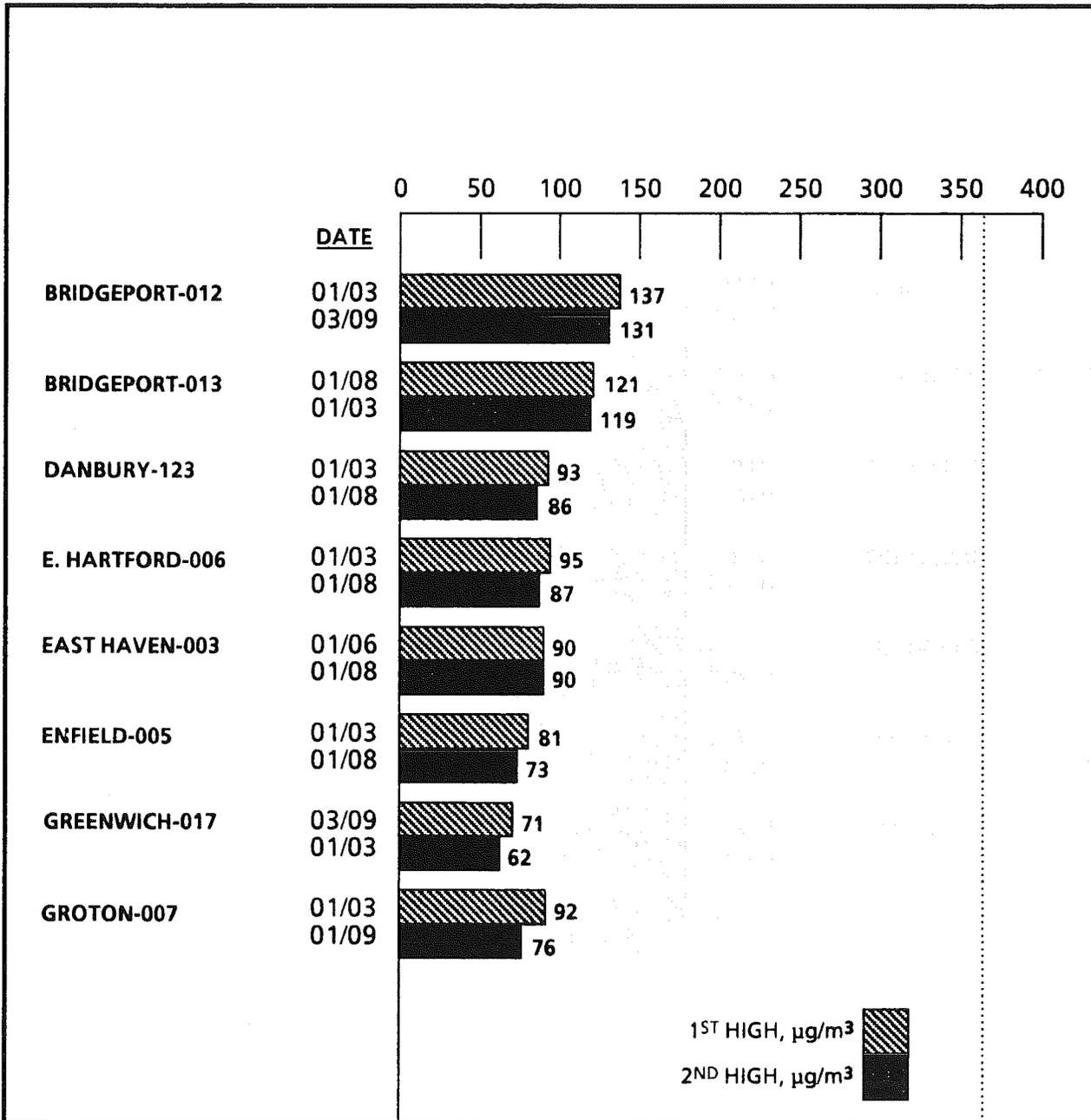
| TOWN NAME   | SITE | YEAR | SAMPLES | ARITHMETIC 95-PCT-LIMITS |       |       | STANDARD DEVIATION | PREDICTED DAYS OVER 365 UG/M3 |
|-------------|------|------|---------|--------------------------|-------|-------|--------------------|-------------------------------|
|             |      |      |         | MEAN                     | LOWER | UPPER |                    |                               |
| MILFORD     | 010  | 1988 | 280     | 27.2                     | 25.8  | 28.7  | 25.024             |                               |
| MILFORD     | 010  | 1989 | 323     | 25.5                     | 24.7  | 26.3  | 22.218             |                               |
| MILFORD     | 010  | 1990 | 283*    | 23.3                     | 22.2  | 24.4  | 20.582             |                               |
| NEW BRITAIN | 011  | 1988 | 359     | 25.1                     | 24.7  | 25.5  | 27.279             |                               |
| NEW BRITAIN | 011  | 1989 | 355     | 23.9                     | 23.6  | 24.3  | 21.577             |                               |
| NEW BRITAIN | 011  | 1990 | 316     | 21.2                     | 20.4  | 21.9  | 18.814             |                               |
| NEW HAVEN   | 017  | 1988 | 303     | 40.3                     | 38.7  | 42.0  | 35.247             | 1                             |
| NEW HAVEN   | 017  | 1989 | 249*    | 29.5                     | 27.5  | 31.4  | 27.983             |                               |
| NEW HAVEN   | 123  | 1988 | 362     | 43.9                     | 43.5  | 44.3  | 37.280             |                               |
| NEW HAVEN   | 123  | 1989 | 345     | 41.1                     | 40.2  | 42.0  | 35.953             |                               |
| NEW HAVEN   | 123  | 1990 | 353     | 35.7                     | 35.2  | 36.2  | 27.077             |                               |
| STAMFORD    | 025  | 1988 | 338     | 27.6                     | 26.8  | 28.3  | 25.278             |                               |
| STAMFORD    | 025  | 1989 | 357     | 28.2                     | 27.8  | 28.5  | 22.593             |                               |
| STAMFORD    | 025  | 1990 | 315     | 21.9                     | 21.0  | 22.7  | 20.806             |                               |
| STAMFORD    | 123  | 1988 | 360     | 24.5                     | 24.2  | 24.9  | 23.560             |                               |
| STAMFORD    | 123  | 1989 | 364     | 25.1                     | 25.0  | 25.2  | 22.175             |                               |
| STAMFORD    | 123  | 1990 | 354     | 23.1                     | 22.8  | 23.5  | 19.813             |                               |
| WATERBURY   | 008  | 1988 | 343     | 26.7                     | 26.0  | 27.5  | 27.919             |                               |
| WATERBURY   | 008  | 1989 | 360     | 29.9                     | 29.5  | 30.2  | 29.408             |                               |
| WATERBURY   | 008  | 1990 | 317     | 22.3                     | 21.4  | 23.2  | 22.754             |                               |
| WATERBURY   | 123  | 1988 | 351     | 26.2                     | 25.7  | 26.6  | 22.552             |                               |
| WATERBURY   | 123  | 1989 | 341     | 25.4                     | 24.8  | 26.0  | 21.647             |                               |
| WATERBURY   | 123  | 1990 | 358     | 24.9                     | 24.7  | 25.2  | 17.648             |                               |

\* THE RANDOMNESS OR QUANTITY OF DATA IS NOT SUFFICIENT FOR REPRESENTATIVE ANNUAL STATISTICS.

N.B. THE ARITHMETIC MEAN AND STANDARD DEVIATION HAVE UNITS OF MICROGRAMS PER CUBIC METER.

### FIGURE 3-2

#### 1990 MAXIMUM CALENDAR DAY AVERAGE SO<sub>2</sub> CONCENTRATIONS

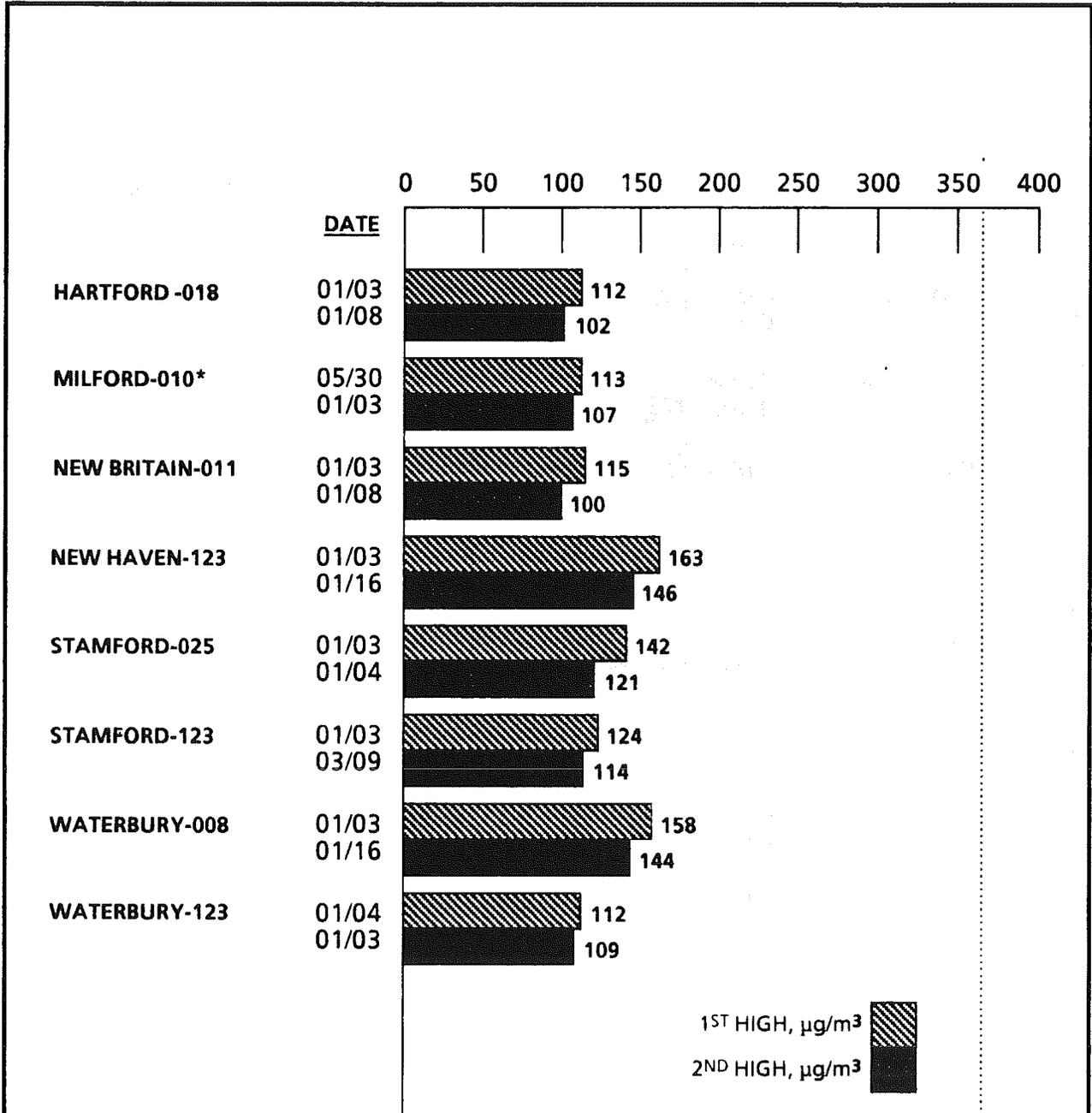


365  
PRIMARY STANDARD

N.B. When a listed concentration occurs more than once at a site, the earliest date of occurrence is given first.

## FIGURE 3-2, CONTINUED

### 1990 MAXIMUM CALENDAR DAY AVERAGE SO<sub>2</sub> CONCENTRATIONS



365  
PRIMARY STANDARD

\* The site has insufficient data to satisfy the minimum sampling criteria.  
 N.B. When a listed concentration occurs more than once at a site, the earliest date of occurrence is given first.

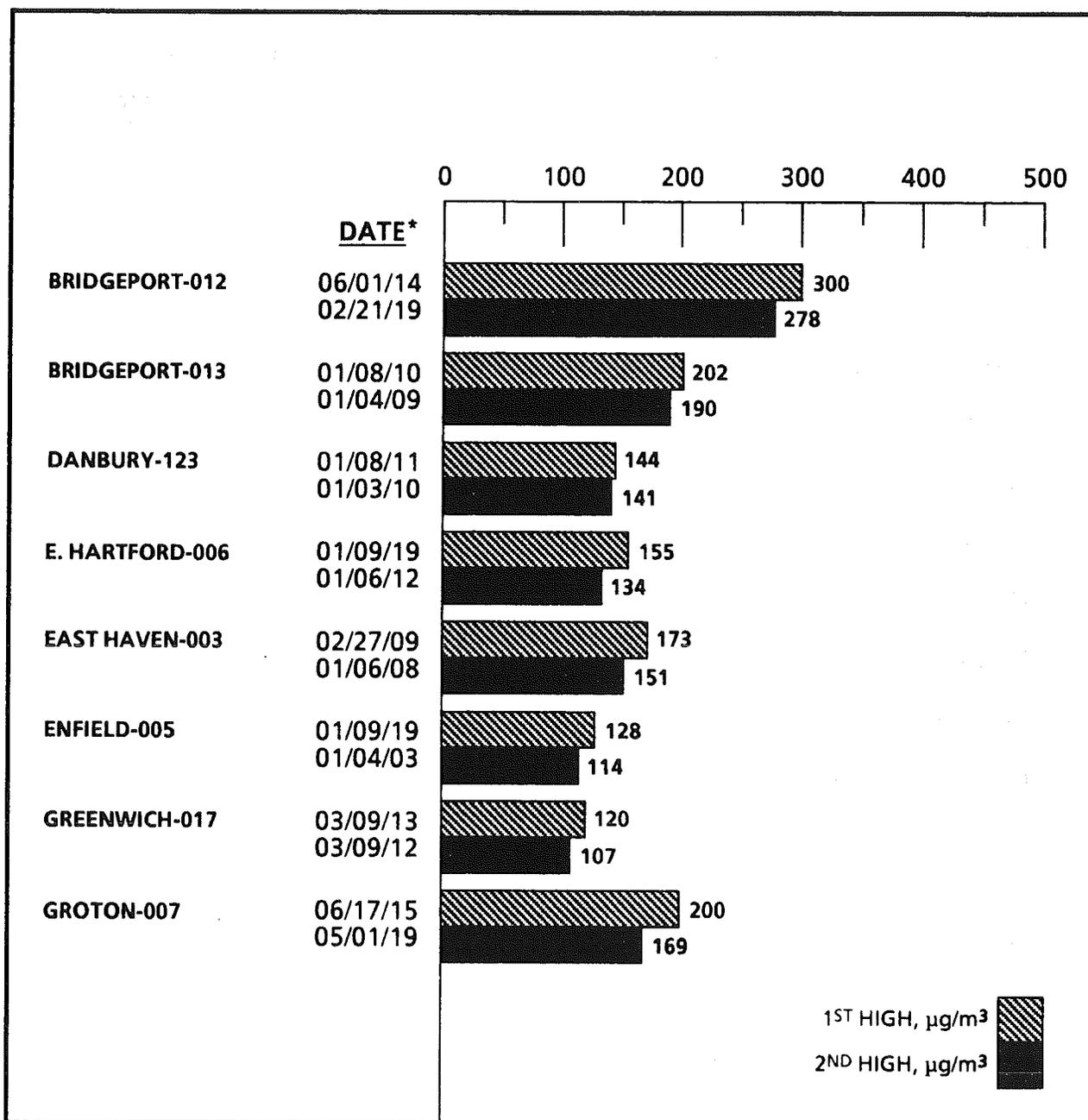
**TABLE 3-3****COMPARISONS OF FIRST AND SECOND HIGH CALENDAR DAY  
AND 24-HOUR RUNNING SO<sub>2</sub> AVERAGES FOR 1990**

| <u>SITE</u>     | <u>FIRST HIGH AVERAGE</u>  |                         | <u>SECOND HIGH AVERAGE</u> |                         |
|-----------------|----------------------------|-------------------------|----------------------------|-------------------------|
|                 | <u>RUNNING<br/>24-HOUR</u> | <u>CALENDAR<br/>DAY</u> | <u>RUNNING<br/>24-HOUR</u> | <u>CALENDAR<br/>DAY</u> |
| Bridgeport-012  | 150                        | 137                     | 133                        | 131                     |
| Bridgeport-013  | 138                        | 121                     | 130                        | 119                     |
| Danbury-123     | 98                         | 93                      | 89                         | 86                      |
| E. Hartford-006 | 106                        | 95                      | 90                         | 87                      |
| East Haven-003  | 95                         | 90                      | 95                         | 90                      |
| Enfield-005     | 92                         | 81                      | 77                         | 73                      |
| Greenwich-017   | 71                         | 71                      | 71                         | 62                      |
| Groton-007      | 93                         | 92                      | 82                         | 76                      |
| Hartford-018    | 128                        | 112                     | 111                        | 102                     |
| Milford-010*    | 114                        | 113                     | 114                        | 107                     |
| New Britain-011 | 128                        | 115                     | 108                        | 100                     |
| New Haven-123   | 186                        | 163                     | 163                        | 146                     |
| Stamford-025    | 158                        | 142                     | 135                        | 121                     |
| Stamford-123    | 137                        | 124                     | 117                        | 114                     |
| Waterbury-008   | 170                        | 158                     | 144                        | 144                     |
| Waterbury-123   | 137                        | 112                     | 115                        | 109                     |

\* The site has insufficient data to satisfy the minimum sampling criteria.  
N.B. The averages have units of  $\mu\text{g}/\text{m}^3$ .

### FIGURE 3-3

#### 1990 MAXIMUM 3-HOUR RUNNING AVERAGE SO<sub>2</sub> CONCENTRATIONS



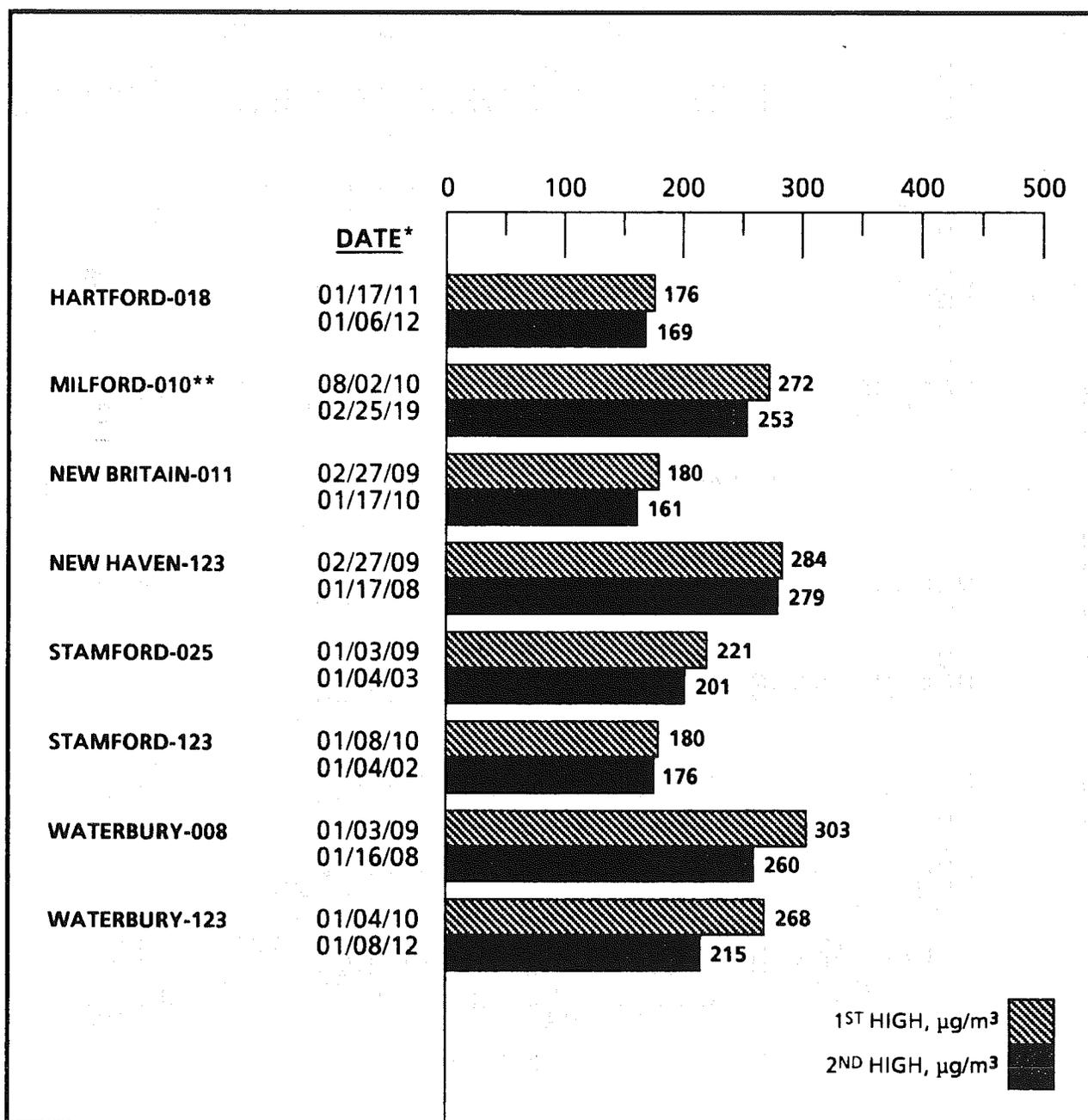
\* The date is the month/day/ending hour of occurrence.

N.B. When a listed concentration occurs more than once at a site, the earliest date of occurrence is given first.

Secondary standard = 1300 µg/m<sup>3</sup>.

### FIGURE 3-3, CONTINUED

#### 1990 MAXIMUM 3-HOUR RUNNING AVERAGE SO<sub>2</sub> CONCENTRATIONS



\* The date is the month/day/ending hour of occurrence.

\*\* The site has insufficient data to satisfy the minimum sampling criteria.

N.B. When a listed concentration occurs more than once at a site, the earliest date of occurrence is given first.

Secondary standard = 1300 µg/m<sup>3</sup>.

TABLE 3-4

1990 TEN HIGHEST 24-HOUR AVERAGE SO2 DAYS WITH WIND DATA

UNITS : MICROGRAMS PER CUBIC METER

| TOWN-SITE (SAMPLES)   | RANK      | 1       | 2       | 3       | 4       | 5       | 6       | 7       | 8       | 9       | 10       |
|-----------------------|-----------|---------|---------|---------|---------|---------|---------|---------|---------|---------|----------|
| BRIDGEPORT-012 (0358) | SO2       | 137     | 131     | 126     | 122     | 121     | 120     | 118     | 118     | 116     | 116      |
|                       | DATE      | 1/ 3/90 | 3/ 9/90 | 1/16/90 | 2/13/90 | 1/17/90 | 1/ 8/90 | 2/22/90 | 2/ 1/90 | 2/ 8/90 | 1/ 4/90  |
| METEOROLOGICAL SITE   | DIR (DEG) | 220     | 230     | 240     | 180     | 190     | 360     | 210     | 200     | 180     | 240      |
| NEWARK                | VEL (MPH) | 3.4     | 3.2     | 5.3     | 7.5     | 5.8     | 3.6     | 8.0     | 5.9     | 3.4     | 6.3      |
|                       | SPD (MPH) | 6.6     | 6.0     | 6.6     | 8.6     | 6.3     | 6.0     | 10.8    | 7.0     | 5.3     | 9.2      |
|                       | RATIO     | 0.520   | 0.538   | 0.809   | 0.869   | 0.912   | 0.602   | 0.738   | 0.841   | 0.631   | 0.687    |
| METEOROLOGICAL SITE   | DIR (DEG) | 180     | 220     | 180     | 190     | 180     | 10      | 190     | 200     | 170     | 180      |
| BRADLEY               | VEL (MPH) | 4.3     | 1.5     | 4.1     | 10.5    | 6.2     | 1.8     | 10.0    | 8.7     | 6.1     | 6.5      |
|                       | SPD (MPH) | 7.6     | 4.5     | 6.5     | 10.6    | 8.1     | 5.6     | 13.8    | 8.9     | 7.2     | 8.5      |
|                       | RATIO     | 0.565   | 0.327   | 0.631   | 0.990   | 0.772   | 0.316   | 0.727   | 0.972   | 0.855   | 0.770    |
| METEOROLOGICAL SITE   | DIR (DEG) | 260     | 180     | 260     | 240     | 170     | 90      | 240     | 230     | 250     | 250      |
| BRIDGEPORT            | VEL (MPH) | 3.1     | 1.1     | 4.6     | 6.7     | 1.4     | 2.4     | 8.1     | 4.3     | 4.9     | 5.3      |
|                       | SPD (MPH) | 3.2     | 2.3     | 4.7     | 6.8     | 4.6     | 3.6     | 8.2     | 5.0     | 5.6     | 5.6      |
|                       | RATIO     | 0.987   | 0.470   | 0.969   | 0.996   | 0.306   | 0.681   | 0.986   | 0.850   | 0.875   | 0.946    |
| METEOROLOGICAL SITE   | DIR (DEG) | 280     | 200     | 290     | 230     | 210     | 250     | 240     | 240     | 240     | 240      |
| WORCESTER             | VEL (MPH) | 6.9     | 1.1     | 5.9     | 8.3     | 5.0     | 2.3     | 14.1    | 9.3     | 7.2     | 8.2      |
|                       | SPD (MPH) | 7.0     | 3.9     | 6.0     | 8.6     | 5.8     | 4.5     | 14.2    | 9.5     | 7.6     | 8.8      |
|                       | RATIO     | 0.975   | 0.293   | 0.980   | 0.968   | 0.864   | 0.517   | 0.991   | 0.985   | 0.947   | 0.932    |
| BRIDGEPORT-013 (0362) | SO2       | 121     | 119     | 108     | 106     | 101     | 92      | 91      | 90      | 87      | 87       |
|                       | DATE      | 1/ 8/90 | 1/ 3/90 | 1/ 4/90 | 3/ 9/90 | 1/16/90 | 1/17/90 | 2/ 7/90 | 1/ 7/90 | 1/ 9/90 | 11/15/90 |
| METEOROLOGICAL SITE   | DIR (DEG) | 360     | 220     | 240     | 230     | 240     | 190     | 360     | 220     | 200     | 220      |
| NEWARK                | VEL (MPH) | 3.6     | 3.4     | 6.3     | 3.2     | 5.3     | 5.8     | 4.6     | 6.2     | 5.0     | 8.1      |
|                       | SPD (MPH) | 6.0     | 6.6     | 9.2     | 6.0     | 6.6     | 6.3     | 6.6     | 8.8     | 6.2     | 9.5      |
|                       | RATIO     | 0.602   | 0.520   | 0.687   | 0.538   | 0.809   | 0.912   | 0.701   | 0.711   | 0.806   | 0.853    |
| METEOROLOGICAL SITE   | DIR (DEG) | 10      | 180     | 180     | 220     | 180     | 180     | 160     | 190     | 170     | 170      |
| BRADLEY               | VEL (MPH) | 1.8     | 4.3     | 6.5     | 1.5     | 4.1     | 6.2     | .7      | 6.4     | 5.6     | 6.3      |
|                       | SPD (MPH) | 5.6     | 7.6     | 8.5     | 4.5     | 6.5     | 8.1     | 4.2     | 9.2     | 7.0     | 7.5      |
|                       | RATIO     | 0.316   | 0.565   | 0.770   | 0.327   | 0.631   | 0.772   | 0.169   | 0.698   | 0.790   | 0.836    |
| METEOROLOGICAL SITE   | DIR (DEG) | 90      | 260     | 250     | 180     | 260     | 170     | 90      | 250     | 240     | 260      |
| BRIDGEPORT            | VEL (MPH) | 2.4     | 3.1     | 5.3     | 1.1     | 4.6     | 1.4     | 2.9     | 5.3     | 5.4     | 8.7      |
|                       | SPD (MPH) | 3.6     | 3.2     | 5.6     | 2.3     | 4.7     | 4.6     | 5.3     | 5.5     | 5.9     | 9.1      |
|                       | RATIO     | 0.681   | 0.987   | 0.946   | 0.470   | 0.969   | 0.306   | 0.554   | 0.971   | 0.909   | 0.965    |
| METEOROLOGICAL SITE   | DIR (DEG) | 250     | 280     | 240     | 200     | 290     | 210     | 240     | 240     | 230     | 270      |
| WORCESTER             | VEL (MPH) | 2.3     | 6.9     | 8.2     | 1.1     | 5.9     | 5.0     | 6.7     | 7.8     | 6.1     | 10.6     |
|                       | SPD (MPH) | 4.5     | 7.0     | 8.8     | 3.9     | 6.0     | 5.8     | 6.9     | 8.2     | 6.5     | 10.6     |
|                       | RATIO     | 0.517   | 0.975   | 0.932   | 0.293   | 0.980   | 0.864   | 0.970   | 0.955   | 0.938   | 0.998    |
| DANBURY-123 (0345)    | SO2       | 93      | 86      | 80      | 77      | 72      | 71      | 71      | 68      | 67      | 66       |
|                       | DATE      | 1/ 3/90 | 1/ 8/90 | 1/ 9/90 | 3/ 9/90 | 1/ 4/90 | 3/10/90 | 1/17/90 | 1/31/90 | 2/ 1/90 | 1/16/90  |
| METEOROLOGICAL SITE   | DIR (DEG) | 220     | 360     | 200     | 230     | 240     | 160     | 190     | 310     | 200     | 240      |
| NEWARK                | VEL (MPH) | 3.4     | 3.6     | 5.0     | 3.2     | 6.3     | 2.8     | 5.8     | .8      | 5.9     | 5.3      |
|                       | SPD (MPH) | 6.6     | 6.0     | 6.2     | 6.0     | 9.2     | 3.2     | 6.3     | 3.2     | 7.0     | 6.6      |
|                       | RATIO     | 0.520   | 0.602   | 0.806   | 0.538   | 0.687   | 0.877   | 0.912   | 0.263   | 0.841   | 0.809    |
| METEOROLOGICAL SITE   | DIR (DEG) | 180     | 10      | 170     | 220     | 180     | 180     | 180     | 360     | 200     | 180      |
| BRADLEY               | VEL (MPH) | 4.3     | 1.8     | 5.6     | 1.5     | 6.5     | 4.6     | 6.2     | .9      | 8.7     | 4.1      |
|                       | SPD (MPH) | 7.6     | 5.6     | 7.0     | 4.5     | 8.5     | 6.6     | 8.1     | 3.7     | 8.9     | 6.5      |
|                       | RATIO     | 0.565   | 0.316   | 0.790   | 0.327   | 0.770   | 0.696   | 0.772   | 0.229   | 0.972   | 0.631    |

TABLE 3-4, CONTINUED

1990 TEN HIGHEST 24-HOUR AVERAGE SO<sub>2</sub> DAYS WITH WIND DATA

| TOWN-SITE (SAMPLES)                | RANK            | 1       | 2       | 3       | 4       | 5       | 6        | 7        | 8       | 9        | 10       |
|------------------------------------|-----------------|---------|---------|---------|---------|---------|----------|----------|---------|----------|----------|
| UNITS : MICROGRAMS PER CUBIC METER |                 |         |         |         |         |         |          |          |         |          |          |
| METEOROLOGICAL SITE<br>BRIDGEPORT  | DIR (DEG)       | 260     | 90      | 240     | 180     | 250     | 110      | 170      | 230     | 230      | 260      |
|                                    | VEL (MPH)       | 3.1     | 2.4     | 5.4     | 5.3     | 5.3     | 5.5      | 1.4      | 4.3     | 4.3      | 4.6      |
|                                    | SPD (MPH)       | 3.2     | 3.6     | 5.9     | 2.3     | 5.6     | 2.4      | 4.6      | 1.7     | 5.0      | 4.7      |
|                                    | RATIO           | 0.987   | 0.681   | 0.909   | 0.470   | 0.946   | 0.190    | 0.306    | 0.188   | 0.850    | 0.969    |
| METEOROLOGICAL SITE<br>WORCESTER   | DIR (DEG)       | 280     | 250     | 230     | 200     | 240     | 220      | 210      | 270     | 240      | 290      |
|                                    | VEL (MPH)       | 6.9     | 2.3     | 6.1     | 1.1     | 8.2     | 4.7      | 3.1      | 3.1     | 9.3      | 5.9      |
|                                    | SPD (MPH)       | 7.0     | 4.5     | 6.5     | 3.9     | 8.8     | 5.5      | 5.8      | 3.9     | 9.5      | 6.0      |
|                                    | RATIO           | 0.975   | 0.517   | 0.938   | 0.293   | 0.932   | 0.867    | 0.864    | 0.793   | 0.985    | 0.980    |
| EAST HARTFORD-006 (0364)           |                 |         |         |         |         |         |          |          |         |          |          |
|                                    | SO <sub>2</sub> | 95      | 87      | 82      | 77      | 76      | 75       | 74       | 72      | 71       | 67       |
|                                    | DATE            | 1/ 3/90 | 1/ 8/90 | 1/ 9/90 | 1/ 4/90 | 1/ 6/90 | 11/15/90 | 1/31/90  | 1/16/90 | 1/17/90  | 11/16/90 |
| METEOROLOGICAL SITE<br>NEWARK      | DIR (DEG)       | 220     | 360     | 200     | 240     | 310     | 220      | 310      | 240     | 190      | 210      |
|                                    | VEL (MPH)       | 3.4     | 3.6     | 5.0     | 6.3     | 6.0     | 8.1      | 8.8      | 5.3     | 5.8      | 6.8      |
|                                    | SPD (MPH)       | 6.6     | 6.0     | 6.2     | 9.2     | 7.6     | 9.5      | 3.2      | 6.6     | 6.3      | 8.5      |
|                                    | RATIO           | 0.520   | 0.602   | 0.806   | 0.687   | 0.782   | 0.853    | 0.263    | 0.809   | 0.912    | 0.803    |
| METEOROLOGICAL SITE<br>BRADLEY     | DIR (DEG)       | 180     | 10      | 170     | 180     | 310     | 170      | 360      | 180     | 180      | 180      |
|                                    | VEL (MPH)       | 4.3     | 1.8     | 5.6     | 6.5     | 3.4     | 6.3      | 9.9      | 4.1     | 6.2      | 7.0      |
|                                    | SPD (MPH)       | 7.6     | 5.6     | 7.0     | 8.5     | 5.3     | 7.5      | 3.7      | 6.5     | 8.1      | 9.9      |
|                                    | RATIO           | 0.565   | 0.316   | 0.790   | 0.770   | 0.638   | 0.836    | 0.229    | 0.631   | 0.772    | 0.701    |
| METEOROLOGICAL SITE<br>BRIDGEPORT  | DIR (DEG)       | 260     | 90      | 240     | 250     | 310     | 260      | 230      | 260     | 170      | 260      |
|                                    | VEL (MPH)       | 3.1     | 2.4     | 5.4     | 5.3     | 3.3     | 8.7      | 3.3      | 4.6     | 1.4      | 5.6      |
|                                    | SPD (MPH)       | 3.2     | 3.6     | 5.9     | 5.6     | 5.0     | 9.1      | 1.7      | 4.7     | 4.6      | 5.9      |
|                                    | RATIO           | 0.987   | 0.681   | 0.909   | 0.946   | 0.653   | 0.965    | 0.188    | 0.969   | 0.306    | 0.951    |
| METEOROLOGICAL SITE<br>WORCESTER   | DIR (DEG)       | 280     | 250     | 230     | 240     | 280     | 270      | 270      | 290     | 210      | 250      |
|                                    | VEL (MPH)       | 6.9     | 2.3     | 6.1     | 8.2     | 6.0     | 10.6     | 3.1      | 5.9     | 5.0      | 8.6      |
|                                    | SPD (MPH)       | 7.0     | 4.5     | 6.5     | 8.8     | 6.5     | 10.6     | 3.9      | 6.0     | 5.8      | 8.8      |
|                                    | RATIO           | 0.975   | 0.517   | 0.938   | 0.932   | 0.924   | 0.998    | 0.793    | 0.980   | 0.864    | 0.985    |
| EAST HAVEN-003 (0365)              |                 |         |         |         |         |         |          |          |         |          |          |
|                                    | SO <sub>2</sub> | 90      | 90      | 89      | 79      | 75      | 69       | 68       | 66      | 64       | 62       |
|                                    | DATE            | 1/ 6/90 | 1/ 8/90 | 1/ 3/90 | 2/27/90 | 3/ 9/90 | 12/ 7/90 | 11/15/90 | 1/16/90 | 12/15/90 | 2/21/90  |
| METEOROLOGICAL SITE<br>NEWARK      | DIR (DEG)       | 310     | 360     | 220     | 230     | 230     | 330      | 220      | 240     | 310      | 230      |
|                                    | VEL (MPH)       | 6.0     | 3.6     | 3.4     | 8.7     | 3.2     | 1.7      | 8.1      | 5.3     | 4.0      | 8.3      |
|                                    | SPD (MPH)       | 7.6     | 6.0     | 6.6     | 10.2    | 6.0     | 5.0      | 9.5      | 6.6     | 6.2      | 9.8      |
|                                    | RATIO           | 0.782   | 0.602   | 0.520   | 0.853   | 0.538   | 0.334    | 0.853    | 0.809   | 0.639    | 0.849    |
| METEOROLOGICAL SITE<br>BRADLEY     | DIR (DEG)       | 310     | 10      | 180     | 200     | 220     | 330      | 170      | 180     | 360      | 210      |
|                                    | VEL (MPH)       | 3.4     | 1.8     | 4.3     | 6.1     | 1.5     | 1.6      | 6.3      | 4.1     | 3.1      | 7.7      |
|                                    | SPD (MPH)       | 5.3     | 5.6     | 7.6     | 8.5     | 4.5     | 4.3      | 7.5      | 6.5     | 3.5      | 8.8      |
|                                    | RATIO           | 0.638   | 0.316   | 0.565   | 0.724   | 0.327   | 0.375    | 0.836    | 0.631   | 0.894    | 0.882    |
| METEOROLOGICAL SITE<br>BRIDGEPORT  | DIR (DEG)       | 310     | 90      | 260     | 260     | 180     | 100      | 260      | 260     | 270      | 260      |
|                                    | VEL (MPH)       | 3.3     | 2.4     | 3.1     | 8.4     | 1.1     | 1.3      | 8.7      | 4.6     | 1.9      | 9.9      |
|                                    | SPD (MPH)       | 5.0     | 3.6     | 3.2     | 9.6     | 2.3     | 2.7      | 9.1      | 4.7     | 5.0      | 10.1     |
|                                    | RATIO           | 0.653   | 0.681   | 0.987   | 0.877   | 0.470   | 0.466    | 0.965    | 0.969   | 0.372    | 0.980    |
| METEOROLOGICAL SITE<br>WORCESTER   | DIR (DEG)       | 280     | 250     | 280     | 220     | 200     | 260      | 290      | 290     | 250      | 270      |
|                                    | VEL (MPH)       | 6.0     | 2.3     | 6.9     | 8.5     | 1.1     | 3.4      | 10.6     | 5.9     | 4.3      | 11.9     |
|                                    | SPD (MPH)       | 6.5     | 4.5     | 7.0     | 8.8     | 3.9     | 4.3      | 10.6     | 6.0     | 7.3      | 11.9     |
|                                    | RATIO           | 0.924   | 0.517   | 0.975   | 0.967   | 0.293   | 0.794    | 0.998    | 0.980   | 0.587    | 0.998    |

TABLE 3-4, CONTINUED

1990 TEN HIGHEST 24-HOUR AVERAGE SO2 DAYS WITH WIND DATA

UNITS : MICROGRAMS PER CUBIC METER

| TOWN-SITE (SAMPLES)  | RANK      | 1       | 2       | 3        | 4       | 5        | 6       | 7       | 8        | 9        | 10       |
|----------------------|-----------|---------|---------|----------|---------|----------|---------|---------|----------|----------|----------|
| ENFIELD-005 (0352)   | SO2       | 81      | 73      | 71       | 62      | 54       | 53      | 50      | 50       | 47       | 45       |
|                      | DATE      | 1/ 3/90 | 1/ 8/90 | 1/ 4/90  | 1/ 9/90 | 2/ 1/90  | 1/25/90 | 1/16/90 | 3/ 2/90  | 3/10/90  | 2/ 8/90  |
| METEOROLOGICAL SITE  | DIR (DEG) | 220     | 360     | 240      | 200     | 200      | 90      | 240     | 230      | 160      | 180      |
| NEWARK               | VEL (MPH) | 3.4     | 3.6     | 6.3      | 5.0     | 5.9      | 3.7     | 5.3     | 7.7      | 2.8      | 3.4      |
|                      | SPD (MPH) | 6.6     | 6.0     | 9.2      | 6.2     | 7.0      | 5.3     | 6.6     | 10.2     | 3.2      | 5.3      |
|                      | RATIO     | 0.520   | 0.602   | 0.687    | 0.806   | 0.841    | 0.697   | 0.809   | 0.755    | 0.877    | 0.631    |
| METEOROLOGICAL SITE  | DIR (DEG) | 180     | 10      | 180      | 170     | 200      | 340     | 180     | 200      | 180      | 170      |
| BRADLEY              | VEL (MPH) | 4.3     | 1.8     | 6.5      | 5.6     | 8.7      | 3.8     | 4.1     | 9.7      | 4.6      | 6.1      |
|                      | SPD (MPH) | 7.6     | 5.6     | 8.5      | 7.0     | 8.9      | 4.3     | 6.5     | 11.9     | 6.6      | 7.2      |
|                      | RATIO     | 0.565   | 0.316   | 0.770    | 0.790   | 0.972    | 0.892   | 0.631   | 0.812    | 0.696    | 0.855    |
| METEOROLOGICAL SITE  | DIR (DEG) | 260     | 90      | 250      | 240     | 230      | 80      | 260     | 260      | 110      | 250      |
| BRIDGEPORT           | VEL (MPH) | 3.1     | 2.4     | 5.3      | 5.4     | 4.3      | 3.0     | 4.6     | 10.6     | 5        | 4.9      |
|                      | SPD (MPH) | 3.2     | 3.6     | 5.6      | 5.9     | 5.0      | 6.5     | 4.7     | 10.6     | 2.4      | 5.6      |
|                      | RATIO     | 0.987   | 0.681   | 0.946    | 0.909   | 0.850    | 0.467   | 0.969   | 0.992    | 0.190    | 0.875    |
| METEOROLOGICAL SITE  | DIR (DEG) | 280     | 250     | 240      | 230     | 240      | 130     | 290     | 250      | 220      | 250      |
| WORCESTER            | VEL (MPH) | 6.9     | 2.3     | 8.2      | 6.1     | 9.3      | 1.5     | 5.9     | 12.3     | 4.7      | 7.2      |
|                      | SPD (MPH) | 7.0     | 4.5     | 8.8      | 6.5     | 9.5      | 3.2     | 6.0     | 12.4     | 5.5      | 7.6      |
|                      | RATIO     | 0.975   | 0.517   | 0.932    | 0.938   | 0.985    | 0.462   | 0.980   | 0.996    | 0.867    | 0.947    |
| GREENWICH-017 (0364) | SO2       | 71      | 62      | 57       | 44      | 43       | 43      | 42      | 41       | 41       | 39       |
|                      | DATE      | 3/ 9/90 | 1/ 3/90 | 11/15/90 | 1/ 8/90 | 12/ 1/90 | 1/ 4/90 | 1/16/90 | 11/16/90 | 12/12/90 | 12/ 6/90 |
| METEOROLOGICAL SITE  | DIR (DEG) | 230     | 220     | 220      | 360     | 250      | 240     | 240     | 210      | 220      | 260      |
| NEWARK               | VEL (MPH) | 3.2     | 3.4     | 8.1      | 3.6     | 7.7      | 6.3     | 5.3     | 6.8      | 8        | 8.5      |
|                      | SPD (MPH) | 6.0     | 6.6     | 9.5      | 6.0     | 8.8      | 9.2     | 6.6     | 8.5      | 3.7      | 10.2     |
|                      | RATIO     | 0.538   | 0.520   | 0.853    | 0.602   | 0.884    | 0.687   | 0.809   | 0.803    | 0.221    | 0.837    |
| METEOROLOGICAL SITE  | DIR (DEG) | 220     | 180     | 170      | 10      | 190      | 180     | 180     | 180      | 130      | 230      |
| BRADLEY              | VEL (MPH) | 1.5     | 4.3     | 6.3      | 1.8     | 7.6      | 6.5     | 4.1     | 7.0      | 2.0      | 8.4      |
|                      | SPD (MPH) | 4.5     | 7.6     | 7.5      | 5.6     | 9.9      | 8.5     | 6.5     | 9.9      | 5.2      | 10.9     |
|                      | RATIO     | 0.327   | 0.565   | 0.836    | 0.316   | 0.768    | 0.770   | 0.631   | 0.701    | 0.396    | 0.770    |
| METEOROLOGICAL SITE  | DIR (DEG) | 180     | 260     | 260      | 90      | 260      | 250     | 260     | 260      | 120      | 270      |
| BRIDGEPORT           | VEL (MPH) | 1.1     | 3.1     | 8.7      | 2.4     | 7.6      | 5.3     | 4.6     | 5.6      | 2.6      | 7.4      |
|                      | SPD (MPH) | 2.3     | 3.2     | 9.1      | 3.6     | 8.2      | 5.6     | 4.7     | 5.9      | 3.5      | 7.5      |
|                      | RATIO     | 0.470   | 0.987   | 0.965    | 0.681   | 0.931    | 0.946   | 0.951   | 0.969    | 0.747    | 0.991    |
| METEOROLOGICAL SITE  | DIR (DEG) | 200     | 280     | 270      | 250     | 250      | 240     | 290     | 250      | 180      | 260      |
| WORCESTER            | VEL (MPH) | 1.1     | 6.9     | 10.6     | 2.3     | 11.1     | 8.2     | 5.9     | 8.6      | 2.8      | 7.1      |
|                      | SPD (MPH) | 3.9     | 7.0     | 10.6     | 4.5     | 11.2     | 8.8     | 6.0     | 8.8      | 4.9      | 7.2      |
|                      | RATIO     | 0.293   | 0.975   | 0.998    | 0.517   | 0.989    | 0.932   | 0.980   | 0.985    | 0.567    | 0.986    |
| GROTON-007 (0357)    | SO2       | 92      | 76      | 75       | 72      | 71       | 67      | 64      | 60       | 60       | 59       |
|                      | DATE      | 1/ 3/90 | 1/ 9/90 | 1/ 8/90  | 3/ 9/90 | 1/16/90  | 2/ 8/90 | 1/17/90 | 3/22/90  | 1/31/90  | 12/ 6/90 |
| METEOROLOGICAL SITE  | DIR (DEG) | 220     | 200     | 360      | 230     | 240      | 180     | 190     | 160      | 310      | 260      |
| NEWARK               | VEL (MPH) | 3.4     | 5.0     | 3.6      | 3.2     | 5.3      | 3.4     | 5.8     | 7.6      | 8        | 8.5      |
|                      | SPD (MPH) | 6.6     | 6.2     | 6.0      | 6.0     | 6.6      | 5.3     | 6.3     | 8.9      | 3.2      | 10.2     |
|                      | RATIO     | 0.520   | 0.806   | 0.602    | 0.538   | 0.809    | 0.631   | 0.912   | 0.856    | 0.263    | 0.837    |
| METEOROLOGICAL SITE  | DIR (DEG) | 180     | 170     | 10       | 220     | 180      | 170     | 180     | 190      | 360      | 230      |
| BRADLEY              | VEL (MPH) | 4.3     | 5.6     | 1.8      | 1.5     | 4.1      | 6.1     | 6.2     | 8.8      | 9        | 8.4      |
|                      | SPD (MPH) | 7.6     | 7.0     | 5.6      | 4.5     | 6.5      | 7.2     | 8.1     | 10.1     | 3.7      | 10.9     |
|                      | RATIO     | 0.565   | 0.790   | 0.316    | 0.327   | 0.631    | 0.855   | 0.772   | 0.878    | 0.229    | 0.770    |

TABLE 3-4. CONTINUED

1990 TEN HIGHEST 24-HOUR AVERAGE SO<sub>2</sub> DAYS WITH WIND DATA

UNITS : MICROGRAMS PER CUBIC METER

| TOWN-SITE (SAMPLES)               | RANK            | 1       | 2       | 3       | 4       | 5       | 6       | 7       | 8       | 9        | 10      |
|-----------------------------------|-----------------|---------|---------|---------|---------|---------|---------|---------|---------|----------|---------|
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG)       | 260     | 240     | 90      | 180     | 260     | 250     | 170     | 220     | 230      | 270     |
|                                   | VEL (MPH)       | 3.1     | 5.4     | 2.4     | 1.1     | 4.6     | 4.9     | 1.4     | 5.8     | .3       | 7.4     |
|                                   | SPD (MPH)       | 3.2     | 5.9     | 3.6     | 2.3     | 4.7     | 5.6     | 4.6     | 7.3     | 1.7      | 7.5     |
|                                   | RATIO           | 0.987   | 0.909   | 0.681   | 0.470   | 0.969   | 0.875   | 0.306   | 0.787   | 0.188    | 0.991   |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG)       | 280     | 230     | 250     | 200     | 290     | 250     | 210     | 210     | 270      | 260     |
|                                   | VEL (MPH)       | 6.9     | 6.1     | 2.3     | 1.1     | 5.9     | 7.2     | 5.0     | 7.1     | 3.1      | 7.1     |
|                                   | SPD (MPH)       | 7.0     | 6.5     | 4.5     | 3.9     | 6.0     | 7.6     | 5.8     | 7.6     | 3.9      | 7.2     |
|                                   | RATIO           | 0.975   | 0.938   | 0.517   | 0.293   | 0.980   | 0.947   | 0.864   | 0.928   | 0.793    | 0.986   |
| HARTFORD-018 (0362)               | SO <sub>2</sub> | 112     | 102     | 100     | 95      | 95      | 92      | 88      | 83      | 81       | 78      |
|                                   | DATE            | 1/ 3/90 | 1/ 8/90 | 1/ 4/90 | 1/ 9/90 | 1/17/90 | 1/ 6/90 | 1/16/90 | 1/24/90 | 11/15/90 | 1/31/90 |
| METEOROLOGICAL SITE<br>NEWARK     | DIR (DEG)       | 220     | 360     | 240     | 200     | 190     | 310     | 240     | 230     | 220      | 310     |
|                                   | VEL (MPH)       | 3.4     | 3.6     | 6.3     | 5.0     | 5.8     | 6.0     | 5.3     | 2.7     | 8.1      | .8      |
|                                   | SPD (MPH)       | 6.6     | 6.0     | 9.2     | 6.2     | 6.3     | 7.6     | 6.6     | 5.2     | 9.5      | 3.2     |
|                                   | RATIO           | 0.520   | 0.602   | 0.687   | 0.806   | 0.912   | 0.782   | 0.809   | 0.521   | 0.853    | 0.263   |
| METEOROLOGICAL SITE<br>BRADLEY    | DIR (DEG)       | 180     | 10      | 180     | 170     | 180     | 310     | 180     | 220     | 170      | 360     |
|                                   | VEL (MPH)       | 4.3     | 1.8     | 6.5     | 5.6     | 6.2     | 3.4     | 4.1     | 2.1     | 6.3      | .9      |
|                                   | SPD (MPH)       | 7.6     | 5.6     | 8.5     | 7.0     | 8.1     | 5.3     | 6.5     | 6.2     | 7.5      | 3.7     |
|                                   | RATIO           | 0.565   | 0.316   | 0.770   | 0.790   | 0.772   | 0.638   | 0.631   | 0.336   | 0.836    | 0.229   |
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG)       | 260     | 90      | 250     | 240     | 170     | 310     | 260     | 110     | 260      | 230     |
|                                   | VEL (MPH)       | 3.1     | 2.4     | 5.3     | 5.4     | 1.4     | 3.3     | 4.6     | 1.0     | 8.7      | .3      |
|                                   | SPD (MPH)       | 3.2     | 3.6     | 5.6     | 5.9     | 4.6     | 5.0     | 4.7     | 4.9     | 9.1      | 1.7     |
|                                   | RATIO           | 0.987   | 0.681   | 0.946   | 0.909   | 0.306   | 0.653   | 0.969   | 0.210   | 0.965    | 0.188   |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG)       | 280     | 250     | 240     | 230     | 210     | 280     | 290     | 220     | 270      | 270     |
|                                   | VEL (MPH)       | 6.9     | 2.3     | 8.2     | 6.1     | 5.0     | 6.0     | 5.9     | 5.7     | 10.6     | 3.1     |
|                                   | SPD (MPH)       | 7.0     | 4.5     | 8.8     | 6.5     | 5.8     | 6.5     | 6.0     | 7.6     | 10.6     | 3.9     |
|                                   | RATIO           | 0.975   | 0.517   | 0.932   | 0.938   | 0.864   | 0.924   | 0.980   | 0.750   | 0.998    | 0.793   |
| NEW BRITAIN-011 (0316)            | SO <sub>2</sub> | 115     | 100     | 97      | 96      | 89      | 87      | 81      | 80      | 77       | 77      |
|                                   | DATE            | 1/ 3/90 | 1/ 8/90 | 1/ 4/90 | 1/ 9/90 | 2/27/90 | 1/17/90 | 1/ 6/90 | 3/ 9/90 | 11/15/90 | 1/16/90 |
| METEOROLOGICAL SITE<br>NEWARK     | DIR (DEG)       | 220     | 360     | 240     | 200     | 230     | 190     | 310     | 230     | 220      | 240     |
|                                   | VEL (MPH)       | 3.4     | 3.6     | 6.3     | 5.0     | 8.7     | 5.8     | 6.0     | 3.2     | 8.1      | 5.3     |
|                                   | SPD (MPH)       | 6.6     | 6.0     | 9.2     | 6.2     | 10.2    | 6.3     | 7.6     | 6.0     | 9.5      | 6.6     |
|                                   | RATIO           | 0.520   | 0.602   | 0.687   | 0.806   | 0.853   | 0.912   | 0.782   | 0.538   | 0.853    | 0.809   |
| METEOROLOGICAL SITE<br>BRADLEY    | DIR (DEG)       | 180     | 10      | 180     | 170     | 200     | 180     | 310     | 220     | 170      | 180     |
|                                   | VEL (MPH)       | 4.3     | 1.8     | 6.5     | 5.6     | 6.1     | 6.2     | 3.4     | 1.5     | 6.3      | 4.1     |
|                                   | SPD (MPH)       | 7.6     | 5.6     | 8.5     | 7.0     | 8.5     | 8.1     | 5.3     | 4.5     | 7.5      | 6.5     |
|                                   | RATIO           | 0.565   | 0.316   | 0.770   | 0.790   | 0.724   | 0.772   | 0.638   | 0.327   | 0.836    | 0.631   |
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG)       | 260     | 90      | 250     | 240     | 260     | 170     | 310     | 180     | 260      | 260     |
|                                   | VEL (MPH)       | 3.1     | 2.4     | 5.3     | 5.4     | 8.4     | 1.4     | 3.3     | 1.1     | 8.7      | 4.6     |
|                                   | SPD (MPH)       | 3.2     | 3.6     | 5.6     | 5.9     | 9.6     | 4.6     | 5.0     | 2.3     | 9.1      | 4.7     |
|                                   | RATIO           | 0.987   | 0.681   | 0.946   | 0.909   | 0.877   | 0.306   | 0.653   | 0.470   | 0.965    | 0.969   |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG)       | 280     | 250     | 240     | 230     | 220     | 210     | 280     | 200     | 270      | 290     |
|                                   | VEL (MPH)       | 6.9     | 2.3     | 8.2     | 6.1     | 8.5     | 5.0     | 6.0     | 6.0     | 10.6     | 5.9     |
|                                   | SPD (MPH)       | 7.0     | 4.5     | 8.8     | 6.5     | 8.8     | 5.8     | 6.5     | 3.9     | 10.6     | 6.0     |
|                                   | RATIO           | 0.975   | 0.517   | 0.932   | 0.938   | 0.967   | 0.864   | 0.924   | 0.293   | 0.998    | 0.980   |

TABLE 3-4. CONTINUED

1990 TEN HIGHEST 24-HOUR AVERAGE SO<sub>2</sub> DAYS WITH WIND DATA

UNITS : MICROGRAMS PER CUBIC METER

| TOWN-SITE (SAMPLES)  | RANK | 1         | 2       | 3       | 4       | 5       | 6        | 7        | 8       | 9       | 10     |
|----------------------|------|-----------|---------|---------|---------|---------|----------|----------|---------|---------|--------|
| NEW HAVEN-123 (0353) |      | 163       | 146     | 137     | 128     | 125     | 122      | 116      | 112     | 110     | 110    |
|                      |      | 1/3/90    | 1/16/90 | 1/4/90  | 2/27/90 | 1/8/90  | 3/9/90   | 1/17/90  | 2/8/90  | 1/6/90  | 1/9/90 |
| METEOROLOGICAL SITE  |      | 220       | 240     | 240     | 230     | 360     | 230      | 190      | 180     | 310     | 200    |
| NEWARK               |      | 3.4       | 5.3     | 6.3     | 8.7     | 3.6     | 3.2      | 5.8      | 3.4     | 6.0     | 5.0    |
|                      |      | VEL (MPH) |         |         |         |         |          |          |         |         |        |
|                      |      | 6.6       | 6.6     | 9.2     | 10.2    | 6.0     | 6.0      | 6.3      | 5.3     | 7.6     | 6.2    |
|                      |      | SPD (MPH) |         |         |         |         |          |          |         |         |        |
|                      |      | 0.520     | 0.809   | 0.687   | 0.853   | 0.602   | 0.538    | 0.912    | 0.631   | 0.782   | 0.806  |
|                      |      | RATIO     |         |         |         |         |          |          |         |         |        |
| METEOROLOGICAL SITE  |      | 180       | 180     | 180     | 200     | 10      | 220      | 180      | 170     | 310     | 170    |
| BRADLEY              |      | 4.3       | 4.1     | 6.5     | 6.1     | 1.8     | 1.5      | 6.2      | 6.1     | 3.4     | 5.6    |
|                      |      | VEL (MPH) |         |         |         |         |          |          |         |         |        |
|                      |      | 7.6       | 6.5     | 8.5     | 8.5     | 5.6     | 4.5      | 8.1      | 7.2     | 5.3     | 7.0    |
|                      |      | SPD (MPH) |         |         |         |         |          |          |         |         |        |
|                      |      | 0.565     | 0.631   | 0.770   | 0.724   | 0.316   | 0.327    | 0.772    | 0.855   | 0.638   | 0.790  |
|                      |      | RATIO     |         |         |         |         |          |          |         |         |        |
| METEOROLOGICAL SITE  |      | 260       | 260     | 250     | 260     | 90      | 180      | 170      | 250     | 310     | 240    |
| BRIDGEPORT           |      | 3.1       | 4.6     | 5.3     | 8.4     | 2.4     | 1.1      | 1.4      | 4.9     | 3.3     | 5.4    |
|                      |      | VEL (MPH) |         |         |         |         |          |          |         |         |        |
|                      |      | 3.2       | 4.7     | 5.6     | 9.6     | 3.6     | 2.3      | 4.6      | 5.6     | 5.0     | 5.9    |
|                      |      | SPD (MPH) |         |         |         |         |          |          |         |         |        |
|                      |      | 0.987     | 0.969   | 0.946   | 0.877   | 0.681   | 0.470    | 0.306    | 0.875   | 0.653   | 0.909  |
|                      |      | RATIO     |         |         |         |         |          |          |         |         |        |
| METEOROLOGICAL SITE  |      | 280       | 290     | 240     | 220     | 250     | 200      | 210      | 250     | 280     | 230    |
| WORCESTER            |      | 6.9       | 5.9     | 8.2     | 8.5     | 2.3     | 1.1      | 5.0      | 7.2     | 6.0     | 6.1    |
|                      |      | VEL (MPH) |         |         |         |         |          |          |         |         |        |
|                      |      | 7.0       | 6.0     | 8.8     | 8.8     | 4.5     | 3.9      | 5.8      | 7.6     | 6.5     | 6.5    |
|                      |      | SPD (MPH) |         |         |         |         |          |          |         |         |        |
|                      |      | 0.975     | 0.980   | 0.932   | 0.967   | 0.517   | 0.293    | 0.864    | 0.947   | 0.924   | 0.938  |
|                      |      | RATIO     |         |         |         |         |          |          |         |         |        |
| STAMFORD-025 (0315)  |      | 142       | 121     | 119     | 118     | 100     | 94       | 81       | 81      | 79      | 77     |
|                      |      | 1/3/90    | 1/4/90  | 1/16/90 | 3/9/90  | 1/17/90 | 11/15/90 | 11/16/90 | 2/8/90  | 3/2/90  | 2/7/90 |
| METEOROLOGICAL SITE  |      | 220       | 240     | 240     | 230     | 190     | 220      | 210      | 180     | 230     | 360    |
| NEWARK               |      | 3.4       | 6.3     | 5.3     | 3.2     | 5.8     | 8.1      | 6.8      | 3.4     | 7.7     | 4.6    |
|                      |      | VEL (MPH) |         |         |         |         |          |          |         |         |        |
|                      |      | 6.6       | 9.2     | 6.6     | 6.0     | 6.3     | 9.5      | 8.5      | 5.3     | 10.2    | 6.6    |
|                      |      | SPD (MPH) |         |         |         |         |          |          |         |         |        |
|                      |      | 0.520     | 0.687   | 0.809   | 0.538   | 0.912   | 0.853    | 0.803    | 0.631   | 0.755   | 0.701  |
|                      |      | RATIO     |         |         |         |         |          |          |         |         |        |
| METEOROLOGICAL SITE  |      | 180       | 180     | 180     | 220     | 180     | 170      | 180      | 170     | 200     | 160    |
| BRADLEY              |      | 4.3       | 6.5     | 4.1     | 1.5     | 6.2     | 6.3      | 7.0      | 6.1     | 9.7     | 7      |
|                      |      | VEL (MPH) |         |         |         |         |          |          |         |         |        |
|                      |      | 7.6       | 8.5     | 6.5     | 4.5     | 8.1     | 7.5      | 9.9      | 7.2     | 11.9    | 4.2    |
|                      |      | SPD (MPH) |         |         |         |         |          |          |         |         |        |
|                      |      | 0.565     | 0.770   | 0.631   | 0.327   | 0.772   | 0.836    | 0.701    | 0.855   | 0.812   | 0.169  |
|                      |      | RATIO     |         |         |         |         |          |          |         |         |        |
| METEOROLOGICAL SITE  |      | 260       | 250     | 260     | 180     | 170     | 260      | 260      | 250     | 260     | 90     |
| BRIDGEPORT           |      | 3.1       | 5.3     | 4.6     | 1.1     | 1.4     | 8.7      | 5.6      | 4.9     | 10.6    | 2.9    |
|                      |      | VEL (MPH) |         |         |         |         |          |          |         |         |        |
|                      |      | 3.2       | 5.6     | 4.7     | 2.3     | 4.6     | 9.1      | 5.9      | 5.6     | 10.6    | 5.3    |
|                      |      | SPD (MPH) |         |         |         |         |          |          |         |         |        |
|                      |      | 0.987     | 0.946   | 0.969   | 0.470   | 0.306   | 0.965    | 0.951    | 0.875   | 0.992   | 0.554  |
|                      |      | RATIO     |         |         |         |         |          |          |         |         |        |
| METEOROLOGICAL SITE  |      | 280       | 240     | 290     | 200     | 210     | 270      | 250      | 250     | 250     | 240    |
| WORCESTER            |      | 6.9       | 8.2     | 5.9     | 1.1     | 5.0     | 10.6     | 8.6      | 7.2     | 12.3    | 6.7    |
|                      |      | VEL (MPH) |         |         |         |         |          |          |         |         |        |
|                      |      | 7.0       | 8.8     | 6.0     | 3.9     | 5.8     | 10.6     | 8.8      | 7.6     | 12.4    | 6.9    |
|                      |      | SPD (MPH) |         |         |         |         |          |          |         |         |        |
|                      |      | 0.975     | 0.932   | 0.980   | 0.293   | 0.864   | 0.998    | 0.985    | 0.947   | 0.996   | 0.970  |
|                      |      | RATIO     |         |         |         |         |          |          |         |         |        |
| STAMFORD-123 (0354)  |      | 124       | 114     | 107     | 105     | 90      | 88       | 80       | 77      | 74      | 73     |
|                      |      | 1/3/90    | 3/9/90  | 1/8/90  | 1/4/90  | 3/2/90  | 11/15/90 | 1/9/90   | 12/1/90 | 1/20/90 | 1/7/90 |
| METEOROLOGICAL SITE  |      | 220       | 230     | 360     | 240     | 230     | 220      | 200      | 250     | 130     | 220    |
| NEWARK               |      | 3.4       | 3.2     | 3.6     | 6.3     | 7.7     | 8.1      | 5.0      | 7.7     | 1.0     | 6.2    |
|                      |      | VEL (MPH) |         |         |         |         |          |          |         |         |        |
|                      |      | 6.6       | 6.0     | 6.0     | 9.2     | 10.2    | 9.5      | 6.2      | 8.8     | 3.3     | 8.8    |
|                      |      | SPD (MPH) |         |         |         |         |          |          |         |         |        |
|                      |      | 0.520     | 0.538   | 0.602   | 0.687   | 0.755   | 0.853    | 0.806    | 0.884   | 0.308   | 0.711  |
|                      |      | RATIO     |         |         |         |         |          |          |         |         |        |
| METEOROLOGICAL SITE  |      | 180       | 220     | 10      | 180     | 200     | 170      | 170      | 190     | 150     | 190    |
| BRADLEY              |      | 4.3       | 1.5     | 1.8     | 6.5     | 9.7     | 6.3      | 5.6      | 7.6     | 3.3     | 6.4    |
|                      |      | VEL (MPH) |         |         |         |         |          |          |         |         |        |
|                      |      | 7.6       | 4.5     | 5.6     | 8.5     | 11.9    | 7.5      | 7.0      | 9.9     | 5.5     | 9.2    |
|                      |      | SPD (MPH) |         |         |         |         |          |          |         |         |        |
|                      |      | 0.565     | 0.327   | 0.316   | 0.770   | 0.812   | 0.836    | 0.790    | 0.768   | 0.600   | 0.698  |
|                      |      | RATIO     |         |         |         |         |          |          |         |         |        |

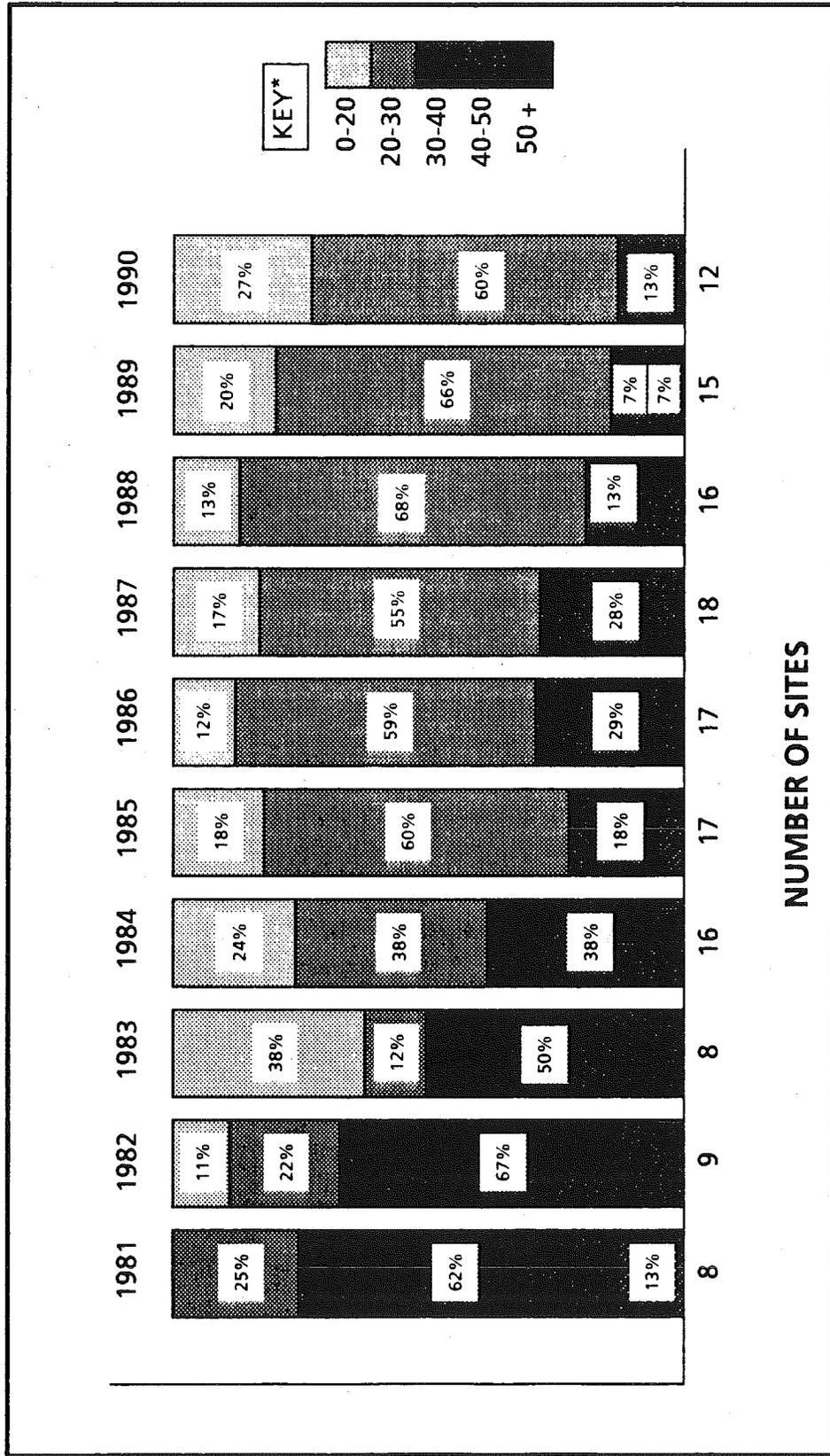
TABLE 3-4, CONTINUED

1990 TEN HIGHEST 24-HOUR AVERAGE SO2 DAYS WITH WIND DATA

UNITS : MICROGRAMS PER CUBIC METER

| TOWN-SITE (SAMPLES)               | RANK      | 1      | 2       | 3      | 4      | 5       | 6        | 7        | 8       | 9       | 10      |
|-----------------------------------|-----------|--------|---------|--------|--------|---------|----------|----------|---------|---------|---------|
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG) | 260    | 180     | 90     | 250    | 260     | 260      | 240      | 260     | 120     | 250     |
|                                   | VEL (MPH) | 3.1    | 1.1     | 2.4    | 5.3    | 10.6    | 8.7      | 5.4      | 7.6     | 1.5     | 5.3     |
|                                   | SPD (MPH) | 3.2    | 2.3     | 3.6    | 5.6    | 10.6    | 9.1      | 5.9      | 8.2     | 1.6     | 5.5     |
|                                   | RATIO     | 0.987  | 0.470   | 0.681  | 0.946  | 0.992   | 0.965    | 0.909    | 0.931   | 0.930   | 0.971   |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG) | 280    | 200     | 250    | 240    | 250     | 270      | 230      | 250     | 240     | 240     |
|                                   | VEL (MPH) | 6.9    | 1.1     | 2.3    | 8.2    | 12.3    | 10.6     | 6.1      | 11.1    | 5.4     | 7.8     |
|                                   | SPD (MPH) | 7.0    | 3.9     | 4.5    | 8.8    | 12.4    | 10.6     | 6.5      | 11.2    | 5.5     | 8.2     |
|                                   | RATIO     | 0.975  | 0.293   | 0.517  | 0.932  | 0.996   | 0.998    | 0.938    | 0.989   | 0.993   | 0.955   |
| WATERBURY-008 (0317)              | SO2       | 158    | 144     | 116    | 109    | 103     | 101      | 92       | 90      | 88      | 78      |
|                                   | DATE      | 1/3/90 | 1/16/90 | 1/4/90 | 3/9/90 | 1/17/90 | 2/8/90   | 11/15/90 | 2/27/90 | 1/31/90 | 1/23/90 |
| METEOROLOGICAL SITE<br>NEWARK     | DIR (DEG) | 220    | 240     | 240    | 230    | 190     | 180      | 220      | 230     | 310     | 270     |
|                                   | VEL (MPH) | 3.4    | 5.3     | 6.3    | 3.2    | 5.8     | 3.4      | 8.1      | 8.7     | 8       | 4.8     |
|                                   | SPD (MPH) | 6.6    | 6.6     | 9.2    | 6.0    | 6.3     | 5.3      | 9.5      | 10.2    | 3.2     | 8.9     |
|                                   | RATIO     | 0.520  | 0.809   | 0.687  | 0.538  | 0.912   | 0.631    | 0.853    | 0.853   | 0.263   | 0.538   |
| METEOROLOGICAL SITE<br>BRADLEY    | DIR (DEG) | 180    | 180     | 180    | 220    | 180     | 170      | 170      | 200     | 360     | 220     |
|                                   | VEL (MPH) | 4.3    | 4.1     | 6.5    | 1.5    | 6.2     | 6.1      | 6.3      | 6.1     | 9       | 2.4     |
|                                   | SPD (MPH) | 7.6    | 6.5     | 8.5    | 4.5    | 8.1     | 7.2      | 7.5      | 8.5     | 3.7     | 4.5     |
|                                   | RATIO     | 0.565  | 0.631   | 0.770  | 0.327  | 0.772   | 0.855    | 0.836    | 0.724   | 0.229   | 0.541   |
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG) | 260    | 260     | 250    | 180    | 170     | 250      | 260      | 260     | 230     | 280     |
|                                   | VEL (MPH) | 3.1    | 4.6     | 5.3    | 1.1    | 1.4     | 4.9      | 8.7      | 8.4     | 3       | 3.6     |
|                                   | SPD (MPH) | 3.2    | 4.7     | 5.6    | 2.3    | 4.6     | 5.6      | 9.1      | 9.6     | 1.7     | 6.0     |
|                                   | RATIO     | 0.987  | 0.969   | 0.946  | 0.470  | 0.306   | 0.875    | 0.965    | 0.877   | 0.188   | 0.603   |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG) | 280    | 290     | 240    | 200    | 210     | 250      | 270      | 220     | 270     | 280     |
|                                   | VEL (MPH) | 6.9    | 5.9     | 8.2    | 1.1    | 5.0     | 7.2      | 10.6     | 8.5     | 3.1     | 4.9     |
|                                   | SPD (MPH) | 7.0    | 6.0     | 8.8    | 3.9    | 5.8     | 7.6      | 10.6     | 8.8     | 3.9     | 5.3     |
|                                   | RATIO     | 0.975  | 0.980   | 0.932  | 0.293  | 0.864   | 0.947    | 0.998    | 0.967   | 0.793   | 0.922   |
| WATERBURY-123 (0358)              | SO2       | 112    | 109     | 108    | 100    | 100     | 80       | 79       | 75      | 67      | 67      |
|                                   | DATE      | 1/4/90 | 1/3/90  | 1/8/90 | 3/9/90 | 1/9/90  | 11/15/90 | 1/16/90  | 3/10/90 | 1/17/90 | 1/7/90  |
| METEOROLOGICAL SITE<br>NEWARK     | DIR (DEG) | 240    | 220     | 360    | 230    | 200     | 220      | 240      | 160     | 190     | 220     |
|                                   | VEL (MPH) | 6.3    | 3.4     | 3.6    | 3.2    | 5.0     | 8.1      | 5.3      | 2.8     | 5.8     | 6.2     |
|                                   | SPD (MPH) | 9.2    | 6.6     | 6.0    | 6.0    | 6.2     | 9.5      | 6.6      | 3.2     | 6.3     | 8.8     |
|                                   | RATIO     | 0.687  | 0.520   | 0.602  | 0.538  | 0.806   | 0.853    | 0.809    | 0.877   | 0.912   | 0.711   |
| METEOROLOGICAL SITE<br>BRADLEY    | DIR (DEG) | 180    | 180     | 10     | 220    | 170     | 170      | 180      | 180     | 180     | 190     |
|                                   | VEL (MPH) | 6.5    | 4.3     | 1.8    | 1.5    | 5.6     | 6.3      | 4.1      | 4.6     | 6.2     | 6.4     |
|                                   | SPD (MPH) | 8.5    | 7.6     | 5.6    | 4.5    | 7.0     | 7.5      | 6.5      | 6.6     | 8.1     | 9.2     |
|                                   | RATIO     | 0.770  | 0.565   | 0.316  | 0.327  | 0.790   | 0.836    | 0.631    | 0.696   | 0.772   | 0.698   |
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG) | 250    | 260     | 90     | 180    | 240     | 260      | 260      | 110     | 170     | 250     |
|                                   | VEL (MPH) | 5.3    | 3.1     | 2.4    | 1.1    | 5.4     | 8.7      | 4.6      | 5       | 1.4     | 5.3     |
|                                   | SPD (MPH) | 5.6    | 3.2     | 3.6    | 2.3    | 5.9     | 9.1      | 4.7      | 2.4     | 4.6     | 5.5     |
|                                   | RATIO     | 0.946  | 0.987   | 0.681  | 0.470  | 0.909   | 0.965    | 0.969    | 0.190   | 0.306   | 0.971   |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG) | 240    | 280     | 250    | 200    | 230     | 270      | 290      | 220     | 210     | 240     |
|                                   | VEL (MPH) | 8.2    | 6.9     | 2.3    | 1.1    | 6.1     | 10.6     | 5.9      | 4.7     | 5.0     | 7.8     |
|                                   | SPD (MPH) | 8.8    | 7.0     | 4.5    | 3.9    | 6.5     | 10.6     | 6.0      | 5.5     | 5.8     | 8.2     |
|                                   | RATIO     | 0.932  | 0.975   | 0.517  | 0.293  | 0.938   | 0.998    | 0.980    | 0.867   | 0.864   | 0.955   |

**FIGURE 3-4**  
**SULFUR DIOXIDE TREND FROM CONTINUOUS DATA**  
**"PERCENT OF SITES WITHIN EACH RANGE"**



\* ANNUAL ARITHMETIC MEAN ( $\mu\text{g}/\text{m}^3$ )

PRIMARY ANNUAL STANDARD =  $80 \mu\text{g}/\text{m}^3$

**TABLE 3-5**

**SO<sub>2</sub> TRENDS FROM CONTINUOUS DATA: 1981-1990**  
**(PAIRED *t* TEST)**

| PAIRED YEARS | AVERAGE OF ANNUAL GEOMETRIC MEANS (µg/m <sup>3</sup> ) | NO. OF SITES | DIFFERENCES OF THE PAIRED YEAR MEANS |           | SIGNIFICANCE LEVEL |           |  |
|--------------|--|--------------|--------------------------------------|-----------|--------------------|-----------|--|
|              |  |              | AVG.                                 | STD. DEV. | TREND AT           |           | PROBABILITY THAT CHANGE IS NOT SIGNIFICANT |
|              |  |              |                                      |           | 95% LEVEL          | 99% LEVEL |  |
| 81<br>82     | 20.9<br>21.0   | 8<br>8       | 0.09                                 | 3.98      | N.C.               | N.C.      | 0.9522                                     |
| 82<br>83     | 20.0<br>18.1   | 8<br>8       | -1.96                                | 0.79      | ↓                  | ↓         | 0.0002                                     |
| 83<br>84     | 18.1<br>18.2   | 8<br>8       | 0.11                                 | 3.20      | N.C.               | N.C.      | 0.9237                                     |
| 84<br>85     | 16.4<br>16.5   | 15<br>15     | 0.04                                 | 3.51      | N.C.               | N.C.      | 0.9654                                     |
| 85<br>86     | 14.6<br>15.5   | 16<br>16     | 0.86                                 | 3.76      | N.C.               | N.C.      | 0.3772                                     |
| 86<br>87     | 15.6<br>16.1   | 16<br>16     | 0.47                                 | 2.65      | N.C.               | N.C.      | 0.4899                                     |
| 87<br>88     | 16.5<br>16.4   | 15<br>15     | -0.13                                | 3.06      | N.C.               | N.C.      | 0.8784                                     |
| 88<br>89     | 15.8<br>16.3   | 14<br>14     | 0.51                                 | 1.51      | N.C.               | N.C.      | 0.2245                                     |
| 89<br>90     | 16.7<br>14.7   | 14<br>14     | -2.03                                | 2.01      | ↓                  | ↓         | 0.0023                                     |

Key to Symbols :    ↓ = Significant downward trend  
                           ↑ = Significant upward trend  
                           N.C. = No significant change

## IV. OZONE

### HEALTH EFFECTS

Ozone is a highly reactive form of oxygen and the principal component of modern smog. Until recently, EPA called this type of pollution "photochemical oxidants." The name has been changed to ozone because ozone is the only oxidant actually measured and is the most plentiful.

Ozone and other oxidants -- including peroxyacetal nitrates (PAN), formaldehyde and peroxides -- are not usually emitted into the air directly. They are formed by chemical reactions in the air from two other pollutants: hydrocarbons and nitrogen oxides. Energy from sunlight is needed for these chemical reactions. This accounts for the term photochemical smog and the daily variation in ozone levels, which increase during the day and decrease at night.

Ozone is a pungent gas with a faintly bluish color. It irritates the mucous membranes of the respiratory system, causing coughing, choking and impaired lung function. It aggravates chronic respiratory diseases like asthma and bronchitis and is believed capable of hastening the death, by pneumonia, of persons in already weakened health. PAN and the other oxidants that accompany ozone are powerful eye irritants.

### NATIONAL AMBIENT AIR QUALITY STANDARD

On February 8, 1979 the EPA established a national ambient air quality standard (NAAQS) for ozone of 0.12 ppm for a one-hour average. Compliance with this standard is determined by summing the number of days at each monitoring site over a consecutive three-year period when the 1-hour standard is exceeded and then computing the average number of exceedances over this interval. If the resulting average value is less than or equal to 1.0 (that is, if the fourth highest daily value in a consecutive three-year period is less than or equal to 0.12 ppm) the ozone standard is considered attained at the site. This standard replaces the old photochemical oxidant Standard of 0.08 ppm. The definition of the pollutant was changed along with the numerical value of the standard, partly because the instruments used to measure photochemical oxidants in the air really measure only ozone. Ozone is one of a group of chemicals which are formed photochemically in the air and are called photochemical oxidants. In the past, the two terms have often been used interchangeably. This Air Quality Summary uses the term "ozone" in conjunction with the NAAQS to reflect the change in both the numerical value of the NAAQS and the definition of the pollutant.

The EPA defines the ozone standard to two decimal places. Therefore, the standard is considered exceeded when a level of 0.13 ppm is reached. However, since the DEP still measures ozone levels to three decimal places, any one-hour average ozone reading which equals or is greater than 0.125 ppm is considered an exceedance of the 0.12 ppm standard in Connecticut. This interpretation of the ozone standard differs from the one used by the DEP before 1982, when a one-hour ozone concentration of 0.121 ppm was considered an exceedance of the standard.

### CONCLUSIONS

As in past years, Connecticut experienced very high concentrations of ozone in the summer months of 1990. Levels in excess of the one-hour NAAQS of 0.12 ppm were frequently recorded at nine of the ten monitored sites. No site experienced levels greater than 0.20 ppm in 1990, compared to one site in 1989 and nine sites in 1988. All ten sites operated in both 1989 and 1990.

There was no clear trend in the high and second high concentrations at the monitoring sites from 1989 to 1990. Six sites had lower high concentrations in 1990, and the differences ranged up to 0.076 ppm, which occurred at Stratford 007. Of the four sites with higher high concentrations in 1990, Madison 002 had the largest increase: 0.048 ppm. Six sites had higher second high concentrations in 1990, and four had lower second high concentrations. The increases ranged up to 0.047 ppm at Madison 002, and the largest decrease was 0.059 ppm at Stratford 007.

The incidence of ozone concentrations in excess of the 1-hour 0.12 ppm standard was lower in 1990 than in 1989 (see Table 4-1). There was a total of 145 exceedances in 1989 and 96 exceedances in 1990 at the ten monitored sites. This represents a decrease in the frequency of such exceedances from 3.2 per 1000 sampling hours in 1989 to 2.4 per 1000 sampling hours in 1990: a 34% decrease. The actual number of hours when the ozone standard was exceeded in the state decreased only moderately from 65 in 1989 to 59 in 1990.

The number of site-days on which the ozone monitors experienced ozone levels in excess of the 1-hour standard decreased from 50 in 1989 to 43 in 1990 at the ten monitoring sites (see Table 4-2). This represents a decrease in the frequency of such occurrences from 2.6 per 100 sampling days in 1989 to 2.2 per 100 sampling days in 1990: a 15% decrease. The actual number of days on which the ozone standard was exceeded in the state stayed constant at 13 from 1989 to 1990.

The yearly changes in ozone concentrations can be attributed primarily to year-to-year variations in regional weather conditions, especially wind direction, temperature and the amount of sunlight. A large portion of the peak ozone concentrations in Connecticut is caused by the transport of ozone and/or precursors (i.e., hydrocarbons and nitrogen oxides) from the New York City area and other points to the west and southwest. Therefore, a decrease in the frequency of winds out of the southwest would help to explain the decrease in the number of ozone exceedances from 1989 to 1990. However, the percentage of southwest winds during the "ozone season" actually increased from 31% in 1989 to 38% in 1990, as is shown by the wind roses from Newark (Figures 4-1 and 4-2). The magnitude of high ozone levels can be partly associated with yearly variations in temperature, since ozone production is greatest at high temperatures and in strong sunlight. However, the summer season's daily high temperatures were actually higher in 1990 than in 1989. This is demonstrated by the number of days exceeding 90° F which increased from three in 1989 to four in 1990 at Sikorsky Airport in Bridgeport, and from eleven in 1989 to fourteen in 1990 at Bradley International Airport (see Tables 9-1 and 9-2). The incidence of high ozone levels is dependent on the percentage of possible sunshine, since sunlight is essential to the creation of ozone. According to National Weather Service local climatological data recorded at Bradley Airport, the percentage of sunshine decreased from 57% in 1989 to 53% in 1990 for the months June through September. The average for the summer months at Bradley is usually 61%. Of the three meteorological parameters, only the percentage of possible sunshine can be invoked as a contributor to explain the decrease in ozone levels from 1989 to 1990.

The meteorological influences notwithstanding, additional and important factors contributing to the decrease in ozone concentrations in 1990 are the continuing efforts of the EPA and the state Department of Environmental Protection to control the emissions of nitrogen oxides and hydrocarbons. Newer automobiles continue to be less polluting, and the use of lower vapor pressure gasoline in the summer months, which was initiated in 1989, is a major effective control strategy.

#### **METHOD OF MEASUREMENT**

The DEP Air Monitoring Unit uses UV photometry to measure and record instantaneous concentrations of ozone continuously by means of a UV absorption technique. Properly calibrated, instruments of this type are shown to be remarkably reliable and stable.

## DISCUSSION OF DATA

**Monitoring Network** - In order to gather information which will further the understanding of ozone production and transport, and to provide real-time data for the daily Pollutant Standards Index, DEP operated a state-wide ozone monitoring network consisting of four types of sites in 1990 (see Figure 4-3):

|                                    |   |
|------------------------------------|---|
| Urban                              | - East Hartford, Middletown             |
| Advection from Southwest           | - Greenwich, Groton, Madison, Stratford |
| Urban and advection from Southwest | - Bridgeport, Danbury, New Haven        |
| Rural                              | - Stafford                              |

**Precision and Accuracy** - The ozone monitors had a total of 166 precision checks during 1990. The resulting 95% probability limits were -6% to +7%. Accuracy is determined by introducing a known amount of ozone into each of the monitors. Three different concentration levels are tested: low, medium, and high. The 95% probability limits, based on 9 audits conducted on the monitoring system, were: low, +2% to +11%; medium, -2% to +12%; and high, -2% to +11%.

**1-Hour Average** - The 1-hour ozone standard was exceeded at all the DEP monitoring sites in 1990, except at New Haven 123. There was no clear trend in the values of the high and second high ozone concentrations from 1989 to 1990.

The number of hours when the ozone standard was exceeded at each site during the summertime "ozone season" is presented in Table 4-1. The number of days on which the 1-hour standard was exceeded at each site is presented in Table 4-2. Figure 4-4 shows the year's high and second high concentrations at each site.

**10 High Days with Wind Data** - Table 4-3 lists the ten highest 1-hour ozone averages and their dates of occurrence for each ozone site in 1990. The wind data associated with these high readings are also presented. (See the discussion of Table 2-5 in the particulate matter section of this Air Quality Summary for a description of the origin and use of these wind data.)

Most (i.e., 88%) of the tabulated high ozone levels occurred on days with winds out of the southwest. This is due to the special features of a southwest wind blowing over Connecticut. The first feature is that, during the summer, southwest winds are usually accompanied by high temperatures and bright sunshine, which are important to the production of ozone. The second feature of a southwest wind is that it will transport precursor emissions from New York City and other urban areas to the southwest of Connecticut. It is the combination of these factors that often produces unhealthy ozone levels in Connecticut.

There are also many instances of high ozone levels on non-southwest wind days. This suggests that pollution control programs currently being implemented in this state are needed to protect the public health of Connecticut's citizenry on days when Connecticut is responsible for its own pollution.

**Trends** - Ozone trends can be illustrated in a number of ways using various statistics: daily mean concentration, daily maximum concentration, number of hourly exceedances, number of daily exceedances, etc. Each has its merits. The daily maximum ozone concentration is used here as the basis for a trend analysis because (1) it represents a more robust dataset than hourly or daily exceedances, and (2) a maximum concentration is more relevant to the NAAQS for ozone.

Figure 4-5 shows the unweighted average of the annual means of the maximum daily concentrations at ten ozone sites from 1981 to 1990. There is a lot of variation in the statistic from one year to the next. The importance of meteorology in the formation of ozone explains much of this

variation. However, unless the effect of meteorology can be factored out, one cannot judge the effect of emission control measures on ozone production. A regression line through the data in Figure 4-5 would trend down, but the reason for this would not be evident.

The effect of meteorology on an ozone trend can be diminished by multiple year averaging. Periods of multiple years exhibit much less meteorological variability than do single years, and a trend analysis based on multiple years should more clearly reveal the effect of emission controls on ambient ozone concentrations. Figure 4-6 illustrates five year averages of the data that is presented in Figure 4-5. It is evident that the ozone trend, freed from meteorological effects, is down over the past five years.

**TABLE 4-1**

**NUMBER OF EXCEEDANCES OF THE 1-HOUR OZONE STANDARD IN 1990**

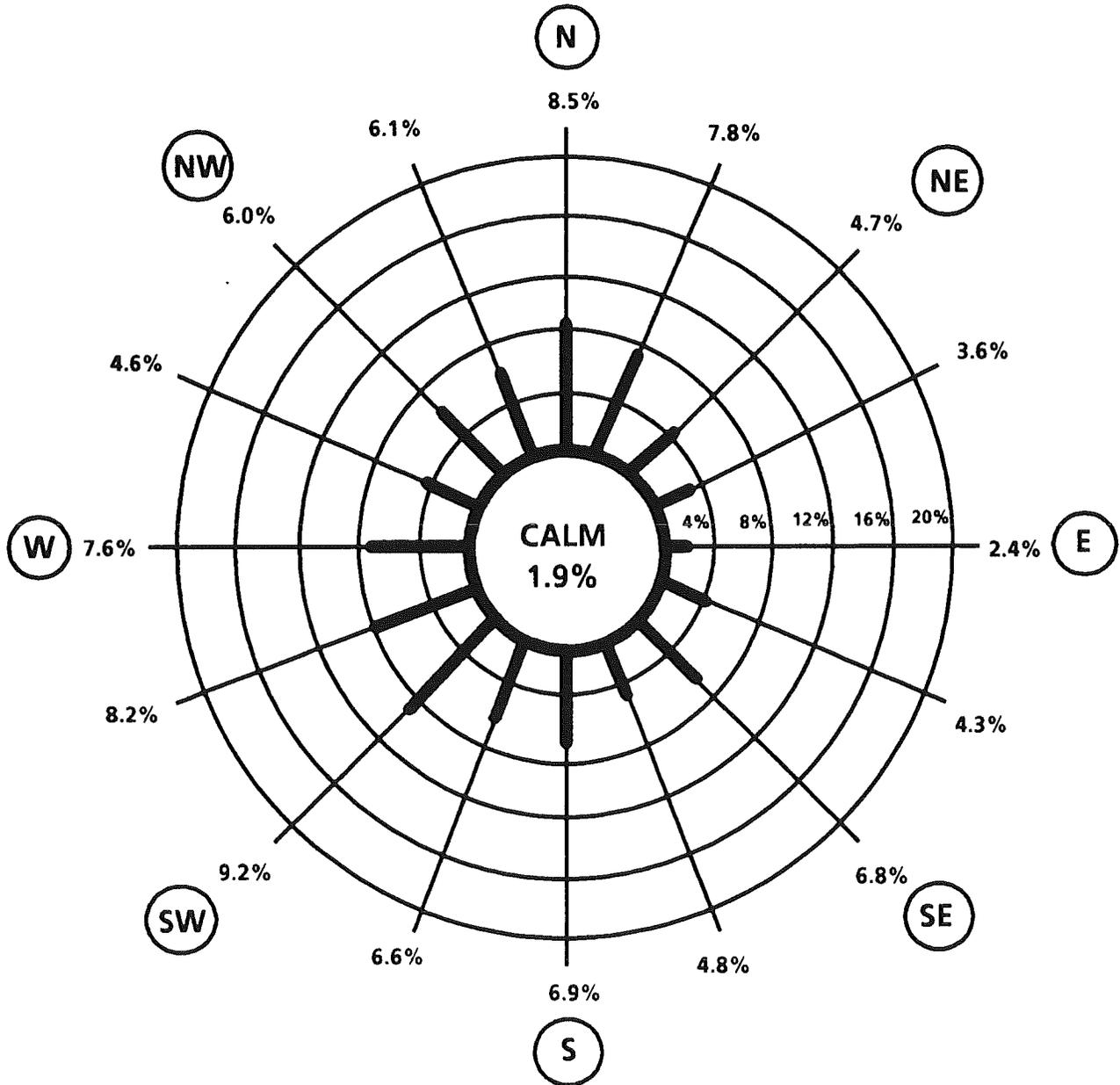
| <u>SITE</u>      | <u>APRIL</u> | <u>MAY</u> | <u>JUNE</u> | <u>JULY</u> | <u>AUG.</u> | <u>SEPT.</u> | <u>OCT.</u> | <u>THIS YEAR</u> | <u>LAST YEAR</u> |
|------------------|--------------|------------|-------------|-------------|-------------|--------------|-------------|------------------|------------------|
| Bridgeport-013   | 0            | 0          | 0           | 3           | 2           | 0            | 0           | 5                | 11               |
| Danbury-123      | 0            | 0          | 3           | 2           | 4           | 0            | 0           | 9                | 3                |
| E. Hartford-003  | 0            | 0          | 0           | 4           | 3           | 0            | 0           | 7                | 10               |
| Greenwich-017    | 0            | 0          | 0           | 9           | 3           | 3            | 0           | 15               | 21               |
| Groton-008       | 0            | 0          | 0           | 15          | 1           | 0            | 0           | 16               | 19               |
| Madison-002      | 0            | 0          | 0           | 14          | 10          | 0            | 0           | 24               | 9                |
| Middletown-007   | 0            | 0          | 0           | 6           | 0           | 0            | 0           | 6                | 16               |
| New Haven-123    | 0            | 0          | 0           | 0           | 0           | 0            | 0           | 0                | 8                |
| Stafford-001     | 0            | 0          | 1           | 3           | 4           | 0            | 0           | 8                | 7                |
| Stratford-007    | 0            | 0          | 0           | 6           | 0           | 0            | 0           | <u>6</u>         | <u>41</u>        |
| TOTAL SITE HOURS |              |            |             |             |             |              |             | 96               | 145              |

**TABLE 4-2**  
**NUMBER OF DAYS WHEN THE 1-HOUR OZONE STANDARD**  
**WAS EXCEEDED IN 1990**

| <u>SITE</u>     | <u>APRIL</u> | <u>MAY</u> | <u>JUNE</u> | <u>JULY</u> | <u>AUG.</u> | <u>SEPT.</u> | <u>OCT.</u> | <u>THIS YEAR</u> | <u>LAST YEAR</u> |
|-----------------|--------------|------------|-------------|-------------|-------------|--------------|-------------|------------------|------------------|
| Bridgeport-013  | 0            | 0          | 0           | 2           | 1           | 0            | 0           | 3                | 4                |
| Danbury-123     | 0            | 0          | 1           | 1           | 2           | 0            | 0           | 4                | 2                |
| E. Hartford-003 | 0            | 0          | 0           | 2           | 2           | 0            | 0           | 4                | 5                |
| Greenwich-017   | 0            | 0          | 0           | 4           | 2           | 1            | 0           | 7                | 7                |
| Groton-008      | 0            | 0          | 0           | 5           | 1           | 0            | 0           | 6                | 6                |
| Madison-002     | 0            | 0          | 0           | 4           | 3           | 0            | 0           | 7                | 4                |
| Middletown-007  | 0            | 0          | 0           | 3           | 0           | 0            | 0           | 3                | 5                |
| New Haven-123   | 0            | 0          | 0           | 0           | 0           | 0            | 0           | 0                | 3                |
| Stafford-001    | 0            | 0          | 1           | 2           | 2           | 0            | 0           | 5                | 3                |
| Stratford-007   | 0            | 0          | 0           | 4           | 0           | 0            | 0           | <u>4</u>         | <u>11</u>        |
| TOTAL SITE DAYS |              |            |             |             |             |              |             | 43               | 50               |

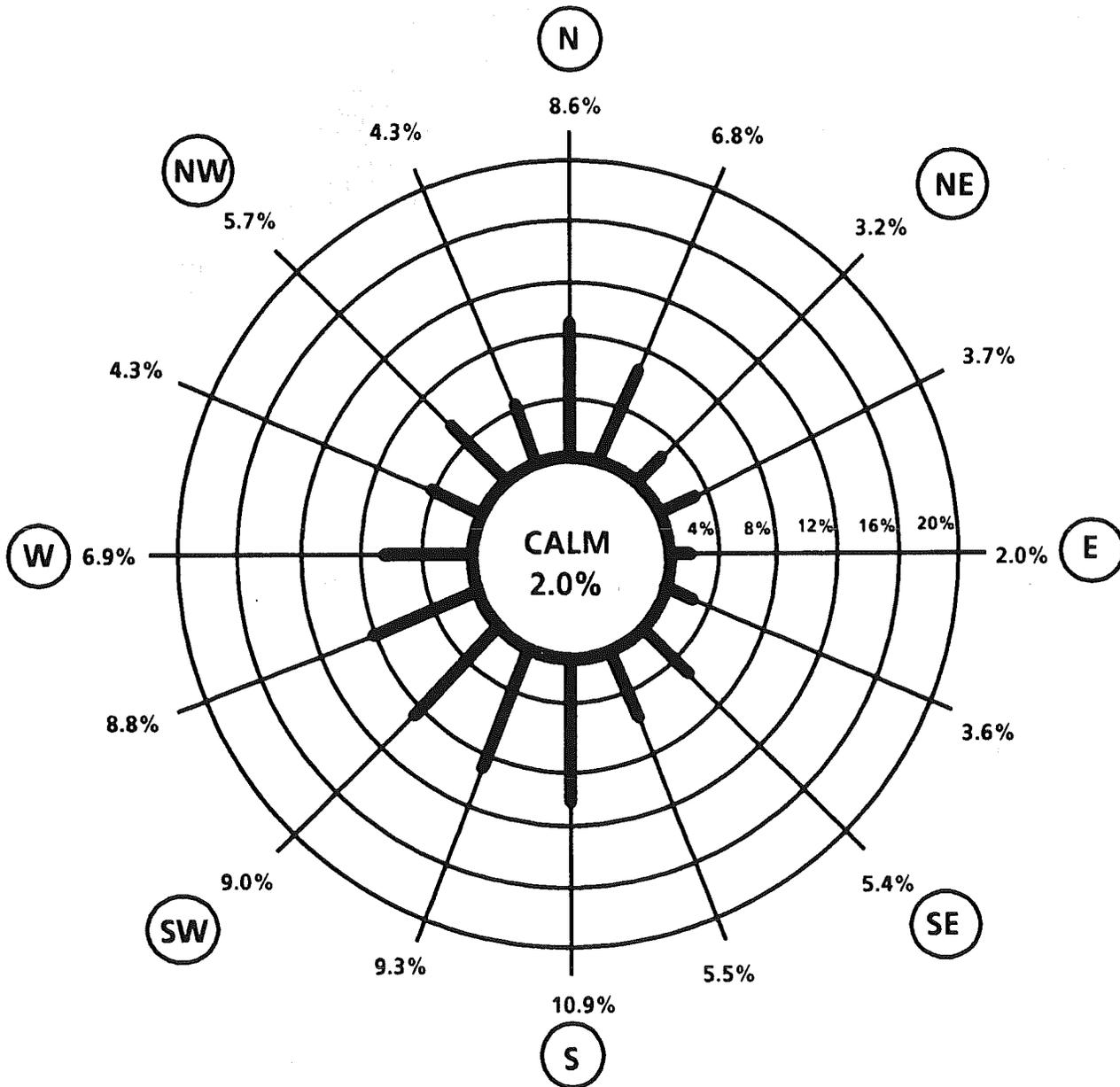
**FIGURE 4-1**

**WIND ROSE FOR APRIL - OCTOBER 1989**  
**NEWARK INTERNATIONAL AIRPORT**  
**NEWARK, NEW JERSEY**



**FIGURE 4-2**

**WIND ROSE FOR APRIL - OCTOBER 1990**  
**NEWARK INTERNATIONAL AIRPORT**  
**NEWARK, NEW JERSEY**



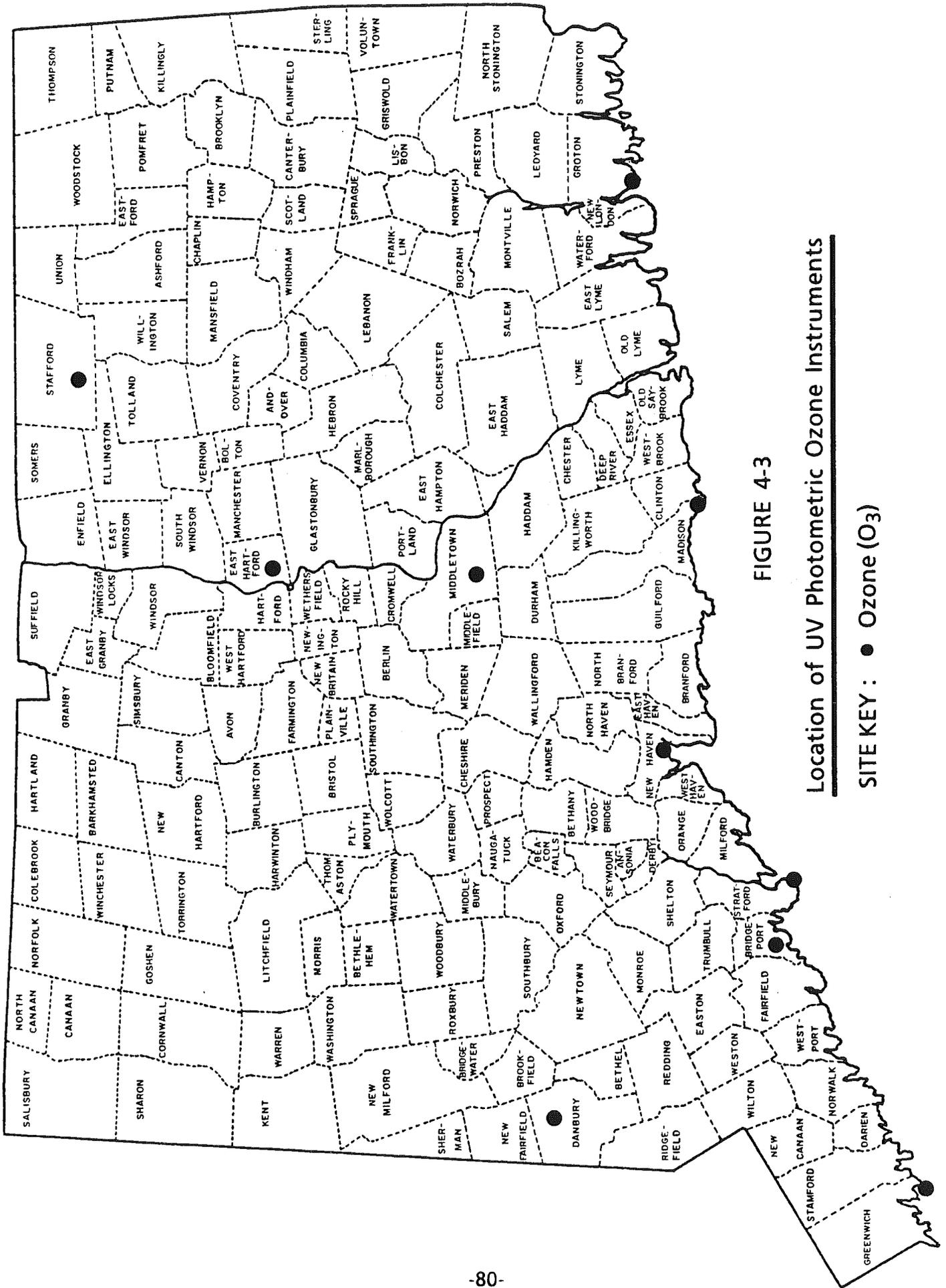


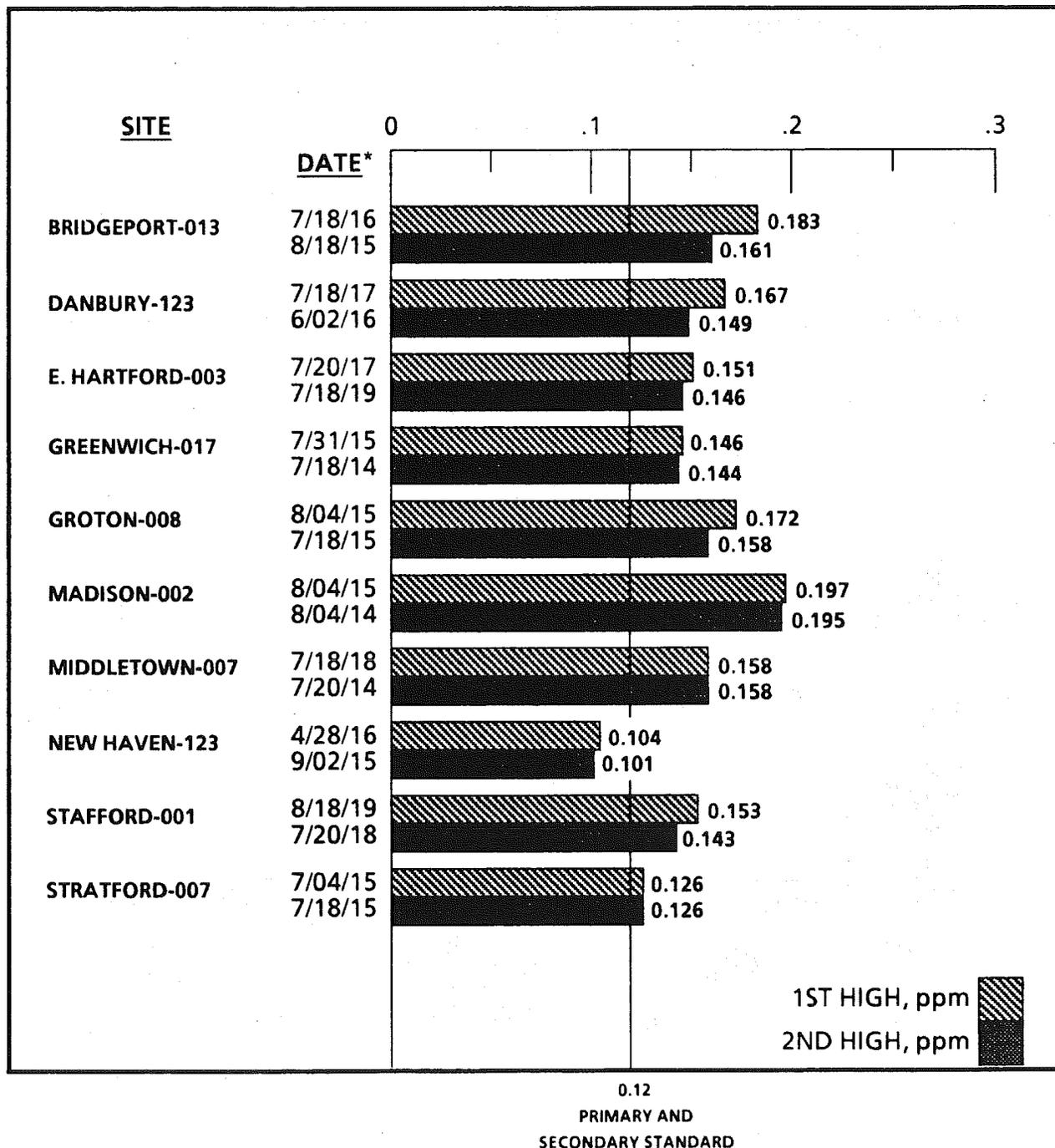
FIGURE 4-3

Location of UV Photometric Ozone Instruments

SITE KEY : ● Ozone (O<sub>3</sub>)

# FIGURE 4-4

## 1990 MAXIMUM 1-HOUR OZONE CONCENTRATIONS



\* The date is the month/day/ending hour of occurrence.

N.B. When a listed concentration occurs more than once at a site, the earliest date is given first.

TABLE 4-3

1990 TEN HIGHEST 1-HOUR AVERAGE OZONE DAYS WITH WIND DATA

UNITS : PARTS PER MILLION

| TOWN-SITE (SAMPLES)             | RANK  | 1     | 2     | 3     | 4     | 5     | 6     | 7     | 8     | 9     | 10    |
|---------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| <b>BRIDGEPORT-013 (4878)</b>    |       |       |       |       |       |       |       |       |       |       |       |
| <b>METEOROLOGICAL SITE</b>      |       |       |       |       |       |       |       |       |       |       |       |
| NEWARK                          |       |       |       |       |       |       |       |       |       |       |       |
| DIR (DEG)                       | 183   | .161  | .134  | .117  | .111  | .106  | .105  | .105  | .105  | .099  | .094  |
| VEL (MPH)                       | 230   | 230   | 230   | 230   | 290   | 150   | 230   | 230   | 280   | 190   | 260   |
| SPD (MPH)                       | 5.2   | 7.0   | 7.3   | 14.0  | 4.1   | 3.8   | 7.2   | 8.6   | 4.8   | 5.8   | 5.6   |
| RATIO                           | 0.685 | 0.734 | 0.723 | 0.861 | 0.548 | 0.485 | 0.833 | 0.670 | 0.757 | 0.722 | 0.722 |
| <b>METEOROLOGICAL SITE</b>      |       |       |       |       |       |       |       |       |       |       |       |
| BRADLEY                         |       |       |       |       |       |       |       |       |       |       |       |
| DIR (DEG)                       | 240   | 200   | 240   | 220   | 310   | 180   | 240   | 220   | 240   | 210   | 250   |
| VEL (MPH)                       | 6.0   | 5.9   | 5.3   | 8.0   | 5.1   | 2.7   | 4.5   | 4.5   | 1.4   | 3.1   | 6.0   |
| SPD (MPH)                       | 8.5   | 7.8   | 8.6   | 10.2  | 6.2   | 5.8   | 7.3   | 7.3   | 4.9   | 6.0   | 8.3   |
| RATIO                           | 0.704 | 0.764 | 0.613 | 0.781 | 0.831 | 0.478 | 0.614 | 0.279 | 0.508 | 0.723 | 0.723 |
| <b>METEOROLOGICAL SITE</b>      |       |       |       |       |       |       |       |       |       |       |       |
| BRIDGEPORT                      |       |       |       |       |       |       |       |       |       |       |       |
| DIR (DEG)                       | 240   | 250   | 240   | 260   | 220   | 200   | 260   | 260   | 250   | 210   | 260   |
| VEL (MPH)                       | 5.4   | 7.4   | 7.2   | 8.2   | 1.8   | 3.8   | 6.2   | 6.2   | 6.7   | 3.4   | 6.4   |
| SPD (MPH)                       | 5.6   | 7.6   | 7.3   | 8.3   | 4.0   | 4.0   | 6.9   | 6.9   | 6.9   | 3.7   | 6.5   |
| RATIO                           | 0.966 | 0.974 | 0.976 | 0.979 | 0.448 | 0.936 | 0.897 | 0.967 | 0.967 | 0.897 | 0.996 |
| <b>METEOROLOGICAL SITE</b>      |       |       |       |       |       |       |       |       |       |       |       |
| WORCESTER                       |       |       |       |       |       |       |       |       |       |       |       |
| DIR (DEG)                       | 270   | 260   | 260   | 260   | 40    | 220   | 220   | 270   | 280   | 260   | 280   |
| VEL (MPH)                       | 6.2   | 5.7   | 7.5   | 9.3   | 3.9   | 1.4   | 6.5   | 6.5   | 6.6   | 5.0   | 6.7   |
| SPD (MPH)                       | 6.3   | 6.0   | 8.2   | 9.3   | 4.3   | 3.5   | 6.8   | 6.8   | 7.0   | 5.5   | 6.9   |
| RATIO                           | 0.983 | 0.948 | 0.913 | 0.997 | 0.907 | 0.418 | 0.967 | 0.932 | 0.923 | 0.923 | 0.971 |
| <b>DANBURY-123 (4816)</b>       |       |       |       |       |       |       |       |       |       |       |       |
| <b>METEOROLOGICAL SITE</b>      |       |       |       |       |       |       |       |       |       |       |       |
| NEWARK                          |       |       |       |       |       |       |       |       |       |       |       |
| DIR (DEG)                       | 167   | .149  | .134  | .129  | .123  | .118  | .116  | .116  | .115  | .113  | .111  |
| VEL (MPH)                       | 230   | 210   | 190   | 230   | 220   | 230   | 200   | 200   | 170   | 150   | 150   |
| SPD (MPH)                       | 5.2   | 8.7   | 5.8   | 7.0   | 5.7   | 7.3   | 6.4   | 6.4   | 6.8   | 3.8   | 4.7   |
| RATIO                           | 0.685 | 0.841 | 0.757 | 0.734 | 0.597 | 0.723 | 0.773 | 0.801 | 0.801 | 0.485 | 0.698 |
| <b>METEOROLOGICAL SITE</b>      |       |       |       |       |       |       |       |       |       |       |       |
| BRADLEY                         |       |       |       |       |       |       |       |       |       |       |       |
| DIR (DEG)                       | 240   | 240   | 210   | 200   | 200   | 240   | 210   | 210   | 190   | 190   | 130   |
| VEL (MPH)                       | 6.0   | 7.3   | 3.1   | 5.9   | 5.2   | 5.3   | 6.9   | 6.9   | 7.1   | 2.7   | 1.3   |
| SPD (MPH)                       | 8.5   | 10.1  | 6.0   | 7.8   | 8.1   | 8.6   | 8.5   | 8.5   | 8.9   | 5.8   | 6.6   |
| RATIO                           | 0.704 | 0.722 | 0.508 | 0.764 | 0.651 | 0.613 | 0.819 | 0.797 | 0.478 | 0.478 | 0.190 |
| <b>METEOROLOGICAL SITE</b>      |       |       |       |       |       |       |       |       |       |       |       |
| BRIDGEPORT                      |       |       |       |       |       |       |       |       |       |       |       |
| DIR (DEG)                       | 240   | 240   | 210   | 250   | 230   | 240   | 230   | 230   | 230   | 200   | 250   |
| VEL (MPH)                       | 5.4   | 6.2   | 3.4   | 7.4   | 6.1   | 7.2   | 5.5   | 6.7   | 6.7   | 3.8   | 3.3   |
| SPD (MPH)                       | 5.6   | 6.6   | 3.7   | 7.6   | 6.2   | 7.3   | 5.6   | 8.3   | 8.3   | 4.0   | 4.2   |
| RATIO                           | 0.966 | 0.940 | 0.897 | 0.974 | 0.980 | 0.976 | 0.974 | 0.799 | 0.936 | 0.936 | 0.784 |
| <b>METEOROLOGICAL SITE</b>      |       |       |       |       |       |       |       |       |       |       |       |
| WORCESTER                       |       |       |       |       |       |       |       |       |       |       |       |
| DIR (DEG)                       | 270   | 260   | 260   | 260   | 240   | 240   | 260   | 260   | 210   | 220   | 360   |
| VEL (MPH)                       | 6.2   | 8.9   | 5.0   | 5.7   | 8.5   | 7.5   | 6.3   | 6.3   | 5.8   | 1.4   | 2.8   |
| SPD (MPH)                       | 6.3   | 9.2   | 5.5   | 6.0   | 8.6   | 8.2   | 6.8   | 6.8   | 6.0   | 3.5   | 7.0   |
| RATIO                           | 0.983 | 0.966 | 0.923 | 0.948 | 0.990 | 0.913 | 0.934 | 0.961 | 0.418 | 0.418 | 0.392 |
| <b>EAST HARTFORD-003 (4739)</b> |       |       |       |       |       |       |       |       |       |       |       |
| <b>METEOROLOGICAL SITE</b>      |       |       |       |       |       |       |       |       |       |       |       |
| NEWARK                          |       |       |       |       |       |       |       |       |       |       |       |
| DIR (DEG)                       | 151   | .146  | .140  | .130  | .118  | .114  | .109  | .109  | .101  | .097  | .097  |
| VEL (MPH)                       | 230   | 230   | 230   | 190   | 200   | 230   | 150   | 150   | 220   | 150   | 170   |
| SPD (MPH)                       | 7.3   | 5.2   | 7.0   | 5.8   | 6.4   | 14.0  | 3.8   | 3.8   | 5.7   | 4.7   | 6.8   |
| RATIO                           | 0.723 | 0.685 | 0.734 | 0.757 | 0.773 | 0.861 | 0.485 | 0.597 | 0.597 | 0.698 | 0.801 |
| <b>METEOROLOGICAL SITE</b>      |       |       |       |       |       |       |       |       |       |       |       |
| BRADLEY                         |       |       |       |       |       |       |       |       |       |       |       |
| DIR (DEG)                       | 240   | 240   | 200   | 210   | 210   | 220   | 190   | 190   | 200   | 130   | 190   |
| VEL (MPH)                       | 5.3   | 6.0   | 5.9   | 3.1   | 6.9   | 8.0   | 2.7   | 5.2   | 5.2   | 1.3   | 7.1   |
| SPD (MPH)                       | 8.6   | 8.5   | 7.8   | 6.0   | 8.5   | 10.2  | 8.1   | 8.1   | 8.1   | 6.6   | 8.9   |
| RATIO                           | 0.613 | 0.704 | 0.764 | 0.508 | 0.819 | 0.781 | 0.478 | 0.651 | 0.651 | 0.190 | 0.797 |

TABLE 4-3. CONTINUED

1990 TEN HIGHEST 1-HOUR AVERAGE OZONE DAYS WITH WIND DATA

UNITS : PARTS PER MILLION

| TOWN-SITE (SAMPLES)               | RANK      | 1       | 2       | 3       | 4       | 5       | 6       | 7       | 8       | 9       | 10      |
|-----------------------------------|-----------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG) | 240     | 240     | 250     | 210     | 230     | 260     | 200     | 230     | 250     | 230     |
|                                   | VEL (MPH) | 7.2     | 5.4     | 7.4     | 3.4     | 5.5     | 8.2     | 3.8     | 6.1     | 3.3     | 6.7     |
|                                   | SPD (MPH) | 7.3     | 5.6     | 7.6     | 3.7     | 5.6     | 8.3     | 4.0     | 6.2     | 4.2     | 8.3     |
|                                   | RATIO     | 0.976   | 0.966   | 0.974   | 0.897   | 0.974   | 0.979   | 0.936   | 0.980   | 0.784   | 0.799   |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG) | 260     | 270     | 260     | 260     | 260     | 260     | 220     | 240     | 360     | 210     |
|                                   | VEL (MPH) | 7.5     | 6.2     | 5.7     | 5.0     | 6.3     | 9.3     | 1.4     | 8.5     | 2.8     | 5.8     |
|                                   | SPD (MPH) | 8.2     | 6.3     | 6.0     | 5.5     | 6.8     | 9.3     | 3.5     | 8.6     | 7.0     | 6.0     |
|                                   | RATIO     | 0.913   | 0.983   | 0.948   | 0.923   | 0.934   | 0.997   | 0.418   | 0.990   | 0.392   | 0.961   |
| GREENWICH-017 (4873)              | OZONE     | .146    | .144    | .143    | .139    | .130    | .128    | .127    | .124    | .118    | .109    |
|                                   | DATE      | 7/31/90 | 7/18/90 | 9/2/90  | 8/17/90 | 7/19/90 | 7/20/90 | 8/16/90 | 8/18/90 | 7/4/90  | 7/9/90  |
| METEOROLOGICAL SITE<br>NEWARK     | DIR (DEG) | 290     | 230     | 280     | 190     | 260     | 230     | 250     | 230     | 230     | 230     |
|                                   | VEL (MPH) | 4.1     | 5.2     | 4.8     | 5.8     | 5.6     | 7.3     | 4.1     | 7.0     | 14.0    | 10.1    |
|                                   | SPD (MPH) | 7.5     | 7.6     | 7.2     | 7.6     | 7.8     | 10.1    | 6.2     | 9.5     | 16.2    | 13.1    |
|                                   | RATIO     | 0.548   | 0.685   | 0.670   | 0.757   | 0.722   | 0.723   | 0.666   | 0.734   | 0.861   | 0.775   |
| METEOROLOGICAL SITE<br>BRADLEY    | DIR (DEG) | 310     | 240     | 240     | 210     | 250     | 240     | 230     | 200     | 220     | 230     |
|                                   | VEL (MPH) | 5.1     | 6.0     | 1.4     | 3.1     | 6.0     | 5.3     | 3.0     | 5.9     | 8.0     | 7.0     |
|                                   | SPD (MPH) | 6.2     | 8.5     | 4.9     | 6.0     | 8.3     | 8.6     | 6.0     | 7.8     | 10.2    | 10.6    |
|                                   | RATIO     | 0.831   | 0.704   | 0.279   | 0.508   | 0.723   | 0.613   | 0.505   | 0.764   | 0.781   | 0.656   |
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG) | 220     | 240     | 250     | 210     | 260     | 240     | 230     | 250     | 260     | 250     |
|                                   | VEL (MPH) | 1.8     | 5.4     | 6.7     | 3.4     | 6.4     | 7.2     | 3.8     | 7.4     | 8.2     | 4.2     |
|                                   | SPD (MPH) | 4.0     | 5.6     | 6.9     | 3.7     | 6.5     | 7.3     | 4.6     | 7.6     | 8.3     | 4.6     |
|                                   | RATIO     | 0.448   | 0.966   | 0.967   | 0.897   | 0.996   | 0.976   | 0.819   | 0.974   | 0.979   | 0.918   |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG) | 40      | 270     | 280     | 260     | 280     | 260     | 280     | 260     | 260     | 250     |
|                                   | VEL (MPH) | 3.9     | 6.2     | 6.6     | 5.0     | 6.7     | 7.5     | 4.6     | 5.7     | 9.3     | 8.3     |
|                                   | SPD (MPH) | 4.3     | 6.3     | 7.0     | 5.5     | 6.9     | 8.2     | 4.9     | 6.0     | 9.3     | 8.5     |
|                                   | RATIO     | 0.907   | 0.983   | 0.932   | 0.923   | 0.971   | 0.913   | 0.950   | 0.948   | 0.997   | 0.982   |
| GROTON-008 (4813)                 | OZONE     | .172    | .158    | .149    | .140    | .135    | .127    | .119    | .116    | .115    | .113    |
|                                   | DATE      | 8/4/90  | 7/18/90 | 7/19/90 | 7/4/90  | 7/17/90 | 7/20/90 | 6/22/90 | 9/2/90  | 7/31/90 | 8/17/90 |
| METEOROLOGICAL SITE<br>NEWARK     | DIR (DEG) | 150     | 230     | 260     | 230     | 230     | 230     | 200     | 280     | 290     | 190     |
|                                   | VEL (MPH) | 3.8     | 5.2     | 5.6     | 14.0    | 7.2     | 7.3     | 6.4     | 4.8     | 4.1     | 5.8     |
|                                   | SPD (MPH) | 7.8     | 7.6     | 7.8     | 16.2    | 8.6     | 10.1    | 8.3     | 7.2     | 7.5     | 7.6     |
|                                   | RATIO     | 0.485   | 0.685   | 0.722   | 0.861   | 0.833   | 0.723   | 0.773   | 0.670   | 0.548   | 0.757   |
| METEOROLOGICAL SITE<br>BRADLEY    | DIR (DEG) | 190     | 240     | 250     | 220     | 220     | 240     | 210     | 240     | 310     | 210     |
|                                   | VEL (MPH) | 2.7     | 6.0     | 6.0     | 8.0     | 4.5     | 5.3     | 6.9     | 1.4     | 5.1     | 3.1     |
|                                   | SPD (MPH) | 5.8     | 8.5     | 8.3     | 10.2    | 7.3     | 8.6     | 8.5     | 4.9     | 6.2     | 6.0     |
|                                   | RATIO     | 0.478   | 0.704   | 0.723   | 0.781   | 0.614   | 0.613   | 0.819   | 0.279   | 0.831   | 0.508   |
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG) | 200     | 240     | 260     | 260     | 260     | 240     | 230     | 250     | 220     | 210     |
|                                   | VEL (MPH) | 3.8     | 5.4     | 6.4     | 8.2     | 6.2     | 7.2     | 5.5     | 6.7     | 1.8     | 3.4     |
|                                   | SPD (MPH) | 4.0     | 5.6     | 6.5     | 8.3     | 6.9     | 7.3     | 5.6     | 6.9     | 4.0     | 3.7     |
|                                   | RATIO     | 0.936   | 0.966   | 0.996   | 0.979   | 0.897   | 0.976   | 0.974   | 0.967   | 0.448   | 0.897   |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG) | 220     | 270     | 280     | 260     | 270     | 260     | 260     | 280     | 40      | 260     |
|                                   | VEL (MPH) | 1.4     | 6.2     | 6.7     | 9.3     | 6.5     | 7.5     | 6.6     | 6.6     | 3.9     | 5.0     |
|                                   | SPD (MPH) | 3.5     | 6.3     | 6.9     | 9.3     | 6.8     | 8.2     | 6.8     | 7.0     | 4.3     | 5.5     |
|                                   | RATIO     | 0.418   | 0.983   | 0.971   | 0.997   | 0.967   | 0.913   | 0.934   | 0.932   | 0.907   | 0.923   |

TABLE 4-3, CONTINUED

1990 TEN HIGHEST 1-HOUR AVERAGE OZONE DAYS WITH WIND DATA

UNITS : PARTS PER MILLION

| TOWN-SITE (SAMPLES)          | RANK | 1         | 2         | 3         | 4         | 5         | 6         | 7         | 8         | 9         | 10        |
|------------------------------|------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| <b>MADISON-002 (4388)</b>    |      |           |           |           |           |           |           |           |           |           |           |
| OZONE                        |      | .197      | .157      | .153      | .151      | .133      | .129      | .129      | .121      | .119      | .116      |
| DATE                         |      | 8/ 4/90   | 8/17/90   | 7/ 4/90   | 8/18/90   | 7/19/90   | 7/20/90   | 7/18/90   | 7/31/90   | 6/22/90   | 7/17/90   |
| METEOROLOGICAL SITE          |      | 150       | 190       | 230       | 230       | 260       | 230       | 230       | 290       | 200       | 230       |
| NEWARK                       |      | DIR (DEG) |
| VEL (MPH)                    |      | 3.8       | 5.8       | 14.0      | 7.0       | 5.6       | 7.3       | 5.2       | 4.1       | 6.4       | 7.2       |
| SPD (MPH)                    |      | 7.8       | 7.6       | 16.2      | 9.5       | 7.6       | 10.1      | 7.6       | 7.5       | 8.3       | 8.6       |
| RATIO                        |      | 0.485     | 0.757     | 0.861     | 0.734     | 0.722     | 0.723     | 0.685     | 0.548     | 0.773     | 0.833     |
| METEOROLOGICAL SITE          |      | 190       | 210       | 220       | 200       | 250       | 240       | 240       | 310       | 210       | 220       |
| BRADLEY                      |      | DIR (DEG) |
| VEL (MPH)                    |      | 2.7       | 3.1       | 8.0       | 5.9       | 6.0       | 5.3       | 6.0       | 5.1       | 6.9       | 4.5       |
| SPD (MPH)                    |      | 5.8       | 6.0       | 10.2      | 7.8       | 8.3       | 8.6       | 8.5       | 6.2       | 8.5       | 7.3       |
| RATIO                        |      | 0.478     | 0.508     | 0.781     | 0.764     | 0.723     | 0.613     | 0.704     | 0.831     | 0.819     | 0.614     |
| METEOROLOGICAL SITE          |      | 200       | 210       | 260       | 250       | 260       | 240       | 240       | 220       | 230       | 260       |
| BRIDGEPORT                   |      | DIR (DEG) |
| VEL (MPH)                    |      | 3.8       | 3.4       | 8.2       | 7.4       | 6.4       | 7.2       | 5.4       | 1.8       | 5.5       | 6.2       |
| SPD (MPH)                    |      | 4.0       | 3.7       | 8.3       | 7.6       | 6.5       | 7.3       | 5.6       | 4.0       | 5.6       | 6.9       |
| RATIO                        |      | 0.936     | 0.897     | 0.979     | 0.974     | 0.996     | 0.976     | 0.966     | 0.448     | 0.974     | 0.897     |
| METEOROLOGICAL SITE          |      | 220       | 260       | 260       | 260       | 280       | 260       | 270       | 40        | 260       | 270       |
| WORCESTER                    |      | DIR (DEG) |
| VEL (MPH)                    |      | 1.4       | 5.0       | 9.3       | 5.7       | 6.7       | 7.5       | 6.2       | 3.9       | 6.3       | 6.5       |
| SPD (MPH)                    |      | 3.5       | 5.5       | 9.3       | 6.0       | 6.9       | 8.2       | 6.3       | 4.3       | 6.8       | 6.8       |
| RATIO                        |      | 0.418     | 0.923     | 0.997     | 0.948     | 0.971     | 0.913     | 0.983     | 0.907     | 0.934     | 0.967     |
| <b>MIDDLETOWN-007 (4250)</b> |      |           |           |           |           |           |           |           |           |           |           |
| OZONE                        |      | .158      | .158      | .125      | .123      | .119      | .104      | .098      | .096      | .095      | .092      |
| DATE                         |      | 7/28/90   | 7/18/90   | 7/17/90   | 8/ 4/90   | 7/ 4/90   | 7/ 9/90   | 7/31/90   | 7/19/90   | 6/29/90   | 6/ 2/90   |
| METEOROLOGICAL SITE          |      | 230       | 230       | 230       | 150       | 230       | 230       | 290       | 260       | 190       | 210       |
| NEWARK                       |      | DIR (DEG) |
| VEL (MPH)                    |      | 7.3       | 5.2       | 7.2       | 3.8       | 14.0      | 10.1      | 4.1       | 5.6       | 1.7       | 8.7       |
| SPD (MPH)                    |      | 10.1      | 7.6       | 8.6       | 7.8       | 16.2      | 13.1      | 7.5       | 7.8       | 8.3       | 10.4      |
| RATIO                        |      | 0.723     | 0.685     | 0.833     | 0.485     | 0.861     | 0.775     | 0.548     | 0.722     | 0.205     | 0.841     |
| METEOROLOGICAL SITE          |      | 240       | 240       | 220       | 190       | 220       | 230       | 310       | 250       | 210       | 210       |
| BRADLEY                      |      | DIR (DEG) |
| VEL (MPH)                    |      | 5.3       | 6.0       | 4.5       | 2.7       | 8.0       | 7.0       | 5.1       | 6.0       | 1.4       | 7.3       |
| SPD (MPH)                    |      | 8.6       | 8.5       | 7.3       | 5.8       | 10.2      | 10.6      | 6.2       | 8.3       | 5.8       | 10.1      |
| RATIO                        |      | 0.613     | 0.704     | 0.614     | 0.478     | 0.781     | 0.656     | 0.831     | 0.723     | 0.248     | 0.722     |
| METEOROLOGICAL SITE          |      | 240       | 240       | 260       | 200       | 260       | 250       | 220       | 260       | 120       | 240       |
| BRIDGEPORT                   |      | DIR (DEG) |
| VEL (MPH)                    |      | 7.2       | 5.4       | 6.2       | 3.8       | 8.2       | 4.2       | 1.8       | 6.4       | 5.0       | 6.2       |
| SPD (MPH)                    |      | 7.3       | 5.6       | 6.9       | 4.0       | 8.3       | 4.6       | 4.0       | 6.5       | 6.2       | 6.6       |
| RATIO                        |      | 0.976     | 0.966     | 0.897     | 0.936     | 0.979     | 0.918     | 0.448     | 0.996     | 0.809     | 0.940     |
| METEOROLOGICAL SITE          |      | 260       | 270       | 270       | 220       | 260       | 250       | 40        | 280       | 140       | 260       |
| WORCESTER                    |      | DIR (DEG) |
| VEL (MPH)                    |      | 7.5       | 6.2       | 6.5       | 1.4       | 9.3       | 8.3       | 3.9       | 6.7       | 3.6       | 8.9       |
| SPD (MPH)                    |      | 8.2       | 6.3       | 6.8       | 3.5       | 9.3       | 8.5       | 4.3       | 6.9       | 4.0       | 9.2       |
| RATIO                        |      | 0.913     | 0.983     | 0.967     | 0.418     | 0.997     | 0.982     | 0.907     | 0.971     | 0.893     | 0.966     |
| <b>NEW HAVEN-123 (4880)</b>  |      |           |           |           |           |           |           |           |           |           |           |
| OZONE                        |      | .104      | .101      | .099      | .097      | .097      | .096      | .089      | .089      | .088      | .084      |
| DATE                         |      | 4/28/90   | 9/ 2/90   | 7/18/90   | 7/17/90   | 8/ 4/90   | 8/18/90   | 7/20/90   | 8/17/90   | 9/29/90   | 9/ 6/90   |
| METEOROLOGICAL SITE          |      | 150       | 280       | 230       | 230       | 150       | 230       | 230       | 190       | 210       | 180       |
| NEWARK                       |      | DIR (DEG) |
| VEL (MPH)                    |      | 4.7       | 4.8       | 5.2       | 7.2       | 3.8       | 7.0       | 7.3       | 5.8       | 5.0       | 4.4       |
| SPD (MPH)                    |      | 6.8       | 7.2       | 7.6       | 8.6       | 7.8       | 9.5       | 10.1      | 7.6       | 6.9       | 5.3       |
| RATIO                        |      | 0.698     | 0.670     | 0.685     | 0.833     | 0.485     | 0.734     | 0.723     | 0.757     | 0.722     | 0.820     |
| METEOROLOGICAL SITE          |      | 130       | 240       | 240       | 220       | 190       | 200       | 240       | 210       | 190       | 200       |
| BRADLEY                      |      | DIR (DEG) |
| VEL (MPH)                    |      | 1.3       | 1.4       | 6.0       | 4.5       | 2.7       | 5.9       | 5.3       | 3.1       | 5.5       | 2.9       |
| SPD (MPH)                    |      | 6.6       | 4.9       | 8.5       | 7.3       | 5.8       | 7.8       | 8.6       | 6.0       | 7.5       | 6.3       |
| RATIO                        |      | 0.190     | 0.279     | 0.704     | 0.614     | 0.478     | 0.764     | 0.613     | 0.508     | 0.734     | 0.461     |

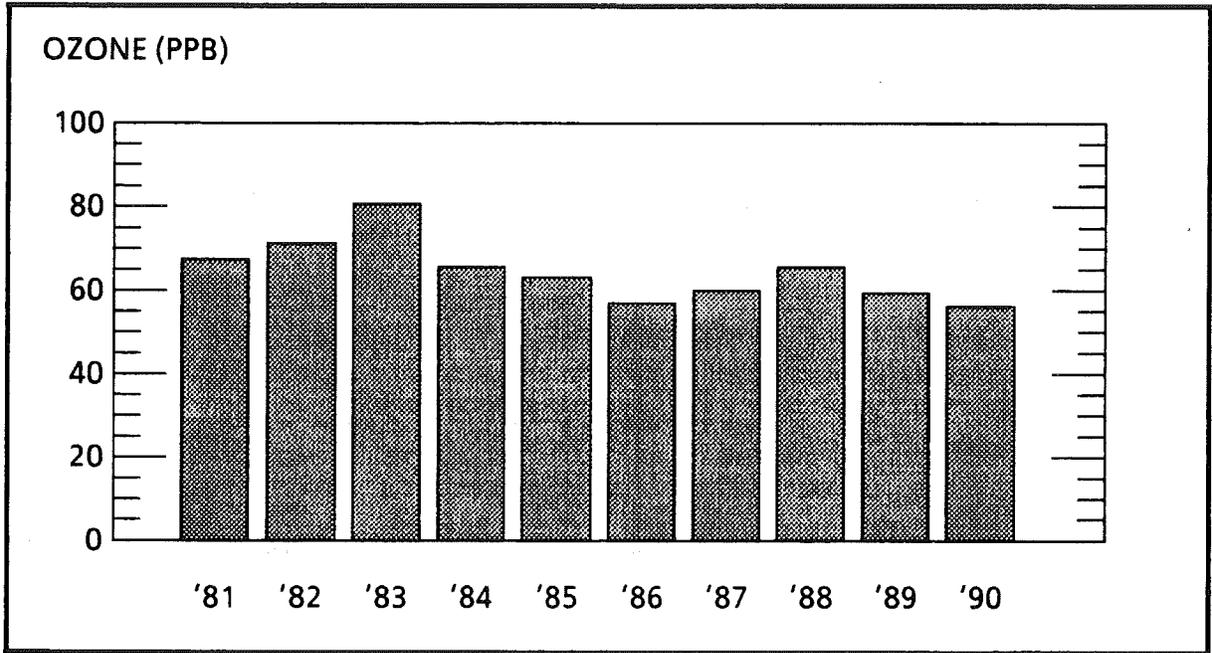
TABLE 4-3, CONTINUED

1990 TEN HIGHEST 1-HOUR AVERAGE OZONE DAYS WITH WIND DATA

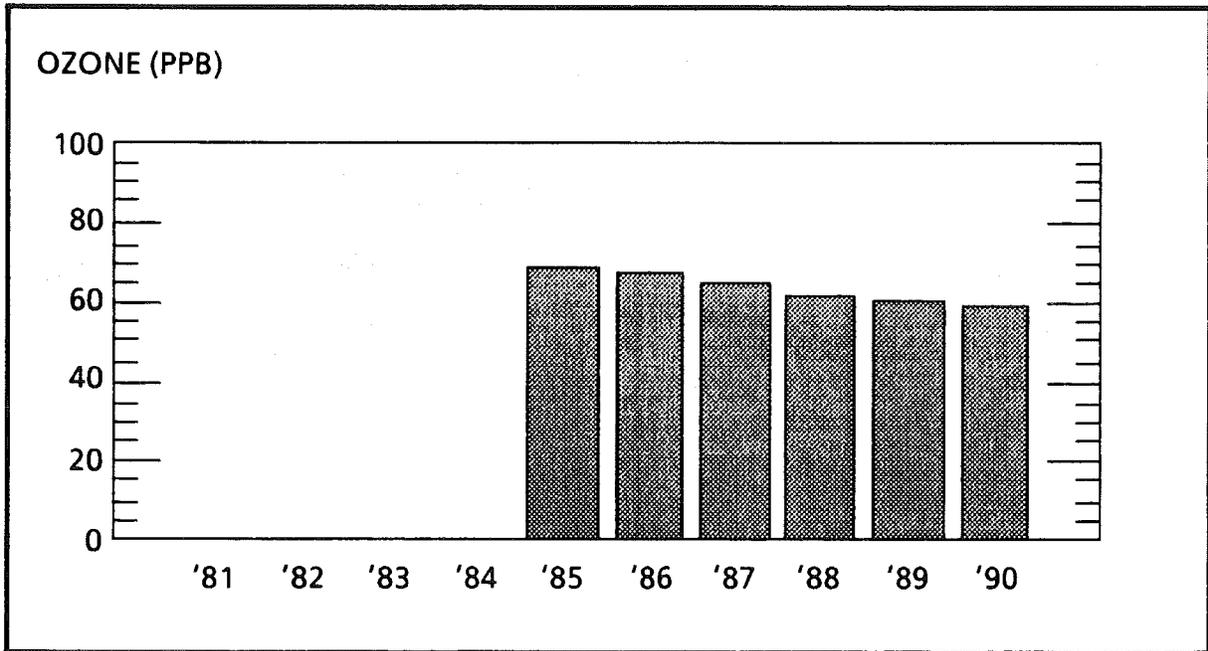
UNITS : PARTS PER MILLION

| TOWN-SITE (SAMPLES)               | RANK      | 1       | 2       | 3       | 4       | 5       | 6       | 7       | 8       | 9       | 10     |
|-----------------------------------|-----------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------|
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG) | 250     | 250     | 240     | 260     | 200     | 250     | 240     | 210     | 250     | 160    |
|                                   | VEL (MPH) | 3.3     | 6.7     | 5.4     | 6.2     | 3.8     | 7.4     | 7.2     | 3.4     | 4.8     | 3.3    |
|                                   | SPD (MPH) | 4.2     | 6.9     | 5.6     | 6.9     | 4.0     | 7.6     | 7.3     | 3.7     | 4.9     | 4.0    |
|                                   | RATIO     | 0.784   | 0.967   | 0.966   | 0.897   | 0.936   | 0.974   | 0.976   | 0.897   | 0.983   | 0.827  |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG) | 360     | 280     | 270     | 270     | 220     | 260     | 260     | 260     | 250     | 220    |
|                                   | VEL (MPH) | 2.8     | 6.6     | 6.2     | 6.5     | 1.4     | 5.7     | 7.5     | 5.0     | 5.7     | 2.6    |
|                                   | SPD (MPH) | 7.0     | 7.0     | 6.3     | 6.8     | 3.5     | 6.0     | 8.2     | 5.5     | 5.9     | 3.7    |
|                                   | RATIO     | 0.392   | 0.932   | 0.983   | 0.967   | 0.418   | 0.948   | 0.913   | 0.923   | 0.968   | 0.688  |
| STAFFORD-001 (4704)               | OZONE     | .153    | .143    | .139    | .127    | .126    | .119    | .114    | .111    | .100    | .099   |
|                                   | DATE      | 8/18/90 | 7/20/90 | 7/18/90 | 6/22/90 | 8/17/90 | 7/4/90  | 8/4/90  | 6/27/90 | 7/17/90 | 9/1/90 |
| METEOROLOGICAL SITE<br>NEWARK     | DIR (DEG) | 230     | 230     | 230     | 200     | 190     | 230     | 150     | 220     | 230     | 230    |
|                                   | VEL (MPH) | 7.0     | 7.3     | 5.2     | 6.4     | 5.8     | 14.0    | 3.8     | 5.7     | 7.2     | 2.1    |
|                                   | SPD (MPH) | 9.5     | 10.1    | 7.6     | 8.3     | 7.6     | 16.2    | 7.8     | 9.5     | 8.6     | 5.0    |
|                                   | RATIO     | 0.734   | 0.723   | 0.685   | 0.773   | 0.757   | 0.861   | 0.485   | 0.597   | 0.833   | 0.419  |
| METEOROLOGICAL SITE<br>BRADLEY    | DIR (DEG) | 200     | 240     | 240     | 210     | 210     | 220     | 190     | 200     | 220     | 190    |
|                                   | VEL (MPH) | 5.9     | 5.3     | 6.0     | 6.9     | 3.1     | 8.0     | 2.7     | 5.2     | 4.5     | 1.8    |
|                                   | SPD (MPH) | 7.8     | 8.6     | 8.5     | 8.5     | 6.0     | 10.2    | 5.8     | 8.1     | 7.3     | 5.3    |
|                                   | RATIO     | 0.764   | 0.613   | 0.704   | 0.819   | 0.508   | 0.781   | 0.478   | 0.651   | 0.614   | 0.341  |
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG) | 250     | 240     | 240     | 230     | 210     | 260     | 200     | 230     | 260     | 180    |
|                                   | VEL (MPH) | 7.4     | 7.2     | 5.4     | 5.5     | 3.4     | 8.2     | 3.8     | 6.1     | 6.2     | 2.0    |
|                                   | SPD (MPH) | 7.6     | 7.3     | 5.6     | 5.6     | 3.7     | 8.3     | 4.0     | 6.2     | 6.9     | 3.7    |
|                                   | RATIO     | 0.974   | 0.976   | 0.966   | 0.974   | 0.897   | 0.979   | 0.936   | 0.980   | 0.897   | 0.533  |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG) | 260     | 260     | 270     | 260     | 260     | 260     | 220     | 240     | 270     | 250    |
|                                   | VEL (MPH) | 5.7     | 7.5     | 6.2     | 6.3     | 5.0     | 9.3     | 1.4     | 8.5     | 6.5     | 3.3    |
|                                   | SPD (MPH) | 6.0     | 8.2     | 6.3     | 6.8     | 5.5     | 9.3     | 3.5     | 8.6     | 6.8     | 4.0    |
|                                   | RATIO     | 0.948   | 0.913   | 0.983   | 0.934   | 0.923   | 0.997   | 0.418   | 0.990   | 0.967   | 0.829  |
| STRATFORD-007 (3724)              | OZONE     | .126    | .126    | .125    | .125    | .122    | .115    | .114    | .107    | .107    | .104   |
|                                   | DATE      | 7/4/90  | 7/18/90 | 7/19/90 | 7/17/90 | 8/17/90 | 8/18/90 | 7/20/90 | 6/2/90  | 4/28/90 | 7/9/90 |
| METEOROLOGICAL SITE<br>NEWARK     | DIR (DEG) | 230     | 230     | 260     | 230     | 190     | 230     | 230     | 210     | 150     | 230    |
|                                   | VEL (MPH) | 14.0    | 5.2     | 5.6     | 7.2     | 5.8     | 7.0     | 7.3     | 8.7     | 4.7     | 10.1   |
|                                   | SPD (MPH) | 16.2    | 7.6     | 7.8     | 8.6     | 7.6     | 9.5     | 10.1    | 10.4    | 6.8     | 13.1   |
|                                   | RATIO     | 0.861   | 0.685   | 0.722   | 0.833   | 0.757   | 0.734   | 0.723   | 0.841   | 0.698   | 0.775  |
| METEOROLOGICAL SITE<br>BRADLEY    | DIR (DEG) | 220     | 240     | 250     | 220     | 210     | 200     | 240     | 210     | 130     | 230    |
|                                   | VEL (MPH) | 8.0     | 6.0     | 6.0     | 4.5     | 3.1     | 5.9     | 5.3     | 7.3     | 1.3     | 7.0    |
|                                   | SPD (MPH) | 10.2    | 8.5     | 8.3     | 7.3     | 6.0     | 7.8     | 8.6     | 10.1    | 6.6     | 10.6   |
|                                   | RATIO     | 0.781   | 0.704   | 0.723   | 0.614   | 0.508   | 0.764   | 0.613   | 0.722   | 0.190   | 0.656  |
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG) | 260     | 240     | 260     | 260     | 210     | 250     | 240     | 240     | 250     | 250    |
|                                   | VEL (MPH) | 8.2     | 5.4     | 6.4     | 6.2     | 3.4     | 7.4     | 7.2     | 6.2     | 3.3     | 4.2    |
|                                   | SPD (MPH) | 8.3     | 5.6     | 6.5     | 6.9     | 3.7     | 7.6     | 7.3     | 6.6     | 4.2     | 4.6    |
|                                   | RATIO     | 0.979   | 0.966   | 0.996   | 0.897   | 0.897   | 0.974   | 0.976   | 0.940   | 0.784   | 0.918  |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG) | 260     | 270     | 280     | 270     | 260     | 260     | 260     | 260     | 360     | 250    |
|                                   | VEL (MPH) | 9.3     | 6.2     | 6.7     | 6.5     | 5.0     | 5.7     | 7.5     | 8.9     | 2.8     | 8.3    |
|                                   | SPD (MPH) | 9.3     | 6.3     | 6.9     | 6.8     | 5.5     | 6.0     | 8.2     | 9.2     | 7.0     | 8.5    |
|                                   | RATIO     | 0.997   | 0.983   | 0.971   | 0.967   | 0.923   | 0.948   | 0.913   | 0.966   | 0.392   | 0.982  |

**FIGURE 4-5**  
**AVERAGES OF THE ANNUAL MEAN DAILY MAXIMUM**  
**OZONE CONCENTRATIONS AT TEN SITES**



**FIGURE 4-6**  
**5-YEAR AVERAGES OF THE ANNUAL MEAN DAILY MAXIMUM**  
**OZONE CONCENTRATIONS AT TEN SITES**



## V. NITROGEN DIOXIDE

### HEALTH EFFECTS

Nitrogen dioxide (NO<sub>2</sub>) is a toxic gas with a characteristic pungent odor and a reddish-orange-brown color. It is highly oxidizing and extremely corrosive.

The presence of NO<sub>2</sub> in the atmosphere is accounted for by the oxidation of nitric oxide (NO) to NO<sub>2</sub> by means of reactions with various chemical species, principally ozone, hydroperoxyl radicals and organic peroxy radicals. Large amounts of NO are emitted into the air by high temperature combustion processes. Industrial furnaces, power plants and motor vehicles are the primary sources of NO emissions.

Exposure to NO<sub>2</sub> is believed to increase the risks of acute respiratory disease and susceptibility to chronic respiratory infection. NO<sub>2</sub> also contributes to heart, lung, liver and kidney damage. At high concentrations, this pollutant can be fatal. At lower levels of 25 to 100 parts per million, it can cause acute bronchitis and pneumonia. Occasional exposure to low levels of NO<sub>2</sub> can irritate the eyes and skin.

Other effects of nitrogen dioxide are its toxicity to vegetation and its ability to combine with water vapor to form nitric acid. Furthermore, NO<sub>2</sub> is an essential ingredient, along with hydrocarbons, in the formation of ozone.

### CONCLUSIONS

Nitrogen dioxide (NO<sub>2</sub>) concentrations at all monitoring sites did not violate the NAAQS for NO<sub>2</sub> in 1990. The annual arithmetic mean NO<sub>2</sub> concentration at each site was well below the federal standard of 100 µg/m<sup>3</sup>. The highest annual mean was 51 µg/m<sup>3</sup> which occurred at the New Haven 123 site.

### SAMPLE COLLECTION AND ANALYSIS

The DEP Air Monitoring Unit used continuous electronic analyzers employing the chemiluminescent reference method to continuously monitor NO<sub>2</sub> levels.

### DISCUSSION OF DATA

**Monitoring Network** - There were three nitrogen dioxide monitoring sites in 1990 (see Figure 5-1). The sites -- Bridgeport 013, East Hartford 003 and New Haven 123 -- were located in three urban areas near major expressways in order to obtain maximum NO<sub>2</sub> readings.

**Precision and Accuracy** - Twenty precision checks were made on the NO<sub>2</sub> monitors in 1990, yielding 95% probability limits ranging from -23% to +14%. Accuracy is determined by introducing a known amount of NO<sub>2</sub> into each of the monitors. Four audits for accuracy were conducted on the monitoring network in 1990. Four different concentration levels were tested on each monitor: low, low/medium, medium/high and high. The 95% probability limits for the low level test ranged from -8% to +10%; those for the low/medium level test ranged from +3% to +5%; those for the medium/high level test ranged from -6% to +5%; and those for the high level test ranged from -3% to +1%.

**Annual Averages** - The annual average NO<sub>2</sub> standard of 100 µg/m<sup>3</sup> was not exceeded in 1990 at any site in Connecticut (see Table 5-1). In 1990, all three sites had sufficient data to compute valid

arithmetic means. This permits comparisons with the 1988 and 1989 annual averages. The annual average NO<sub>2</sub> concentrations decreased at all three sites between 1988 and 1990.

**Statistical Projections** - The format of Table 5-1 is the same as that used to present the particulate matter and sulfur dioxide data, except that for NO<sub>2</sub> there are no 24-hour standards and, therefore, no projections of violations are possible. However, Table 5-1 gives the annual arithmetic mean of the hourly NO<sub>2</sub> concentrations in order to allow direct comparison to the annual NO<sub>2</sub> standard. The 95% confidence limits about the arithmetic mean for each site demonstrate that it is unlikely that any site exceeded the primary annual standard of 100 µg/m<sup>3</sup> in 1990.

**10-High Days with Wind Data** - Table 5-2 presents for each site the ten days in 1990 when the highest hourly NO<sub>2</sub> readings occurred, along with the associated wind conditions for each day. (See the discussion of Table 2-5 in the particulate matter section for a description of the origin and use of the wind data.)

According to National Weather Service local climatological data recorded at Bradley Airport, 13 of the 17 days listed in the table had at least 50% of the possible sunshine. This is interpreted to confirm the importance of photochemical oxidation in the formation of NO<sub>2</sub>.

Using the National Weather Service data from the Bridgeport meteorological site for Bridgeport 013 and New Haven 123, and using the data from Bradley for East Hartford 003, one finds that over 76% of the days have persistent winds out of the southwest. This is not unexpected given the fact that the NO<sub>2</sub> sites were deliberately located to the north and east of major expressways and interchanges, which are major sources of nitrogen oxide emissions. Moreover, high NO<sub>2</sub> levels coincident with southwest winds confirm the importance of pollution transport into Connecticut from the southwest.

**Trends** - The weighted average of the annual NO<sub>2</sub> concentrations at the three monitoring sites is illustrated in Figure 5-2. The year-to-year trend appears to be down through 1987, up in 1988 and down thereafter.

Given the importance of meteorology -- sunlight, in general, and southwest winds in Connecticut, in particular -- on the formation of NO<sub>2</sub>, a trend might best be illustrated by the averaging of the data over multiple years. As was the case with ozone, a trend based on multiple years of data should diminish the effect of meteorology and, thereby, reveal the effect of nitrogen oxide and hydrocarbon emission controls on ambient concentrations of NO<sub>2</sub>. Figure 5-3 shows that the 3-year average NO<sub>2</sub> concentration, unlinked from meteorology, has been trending downward over the past six years.

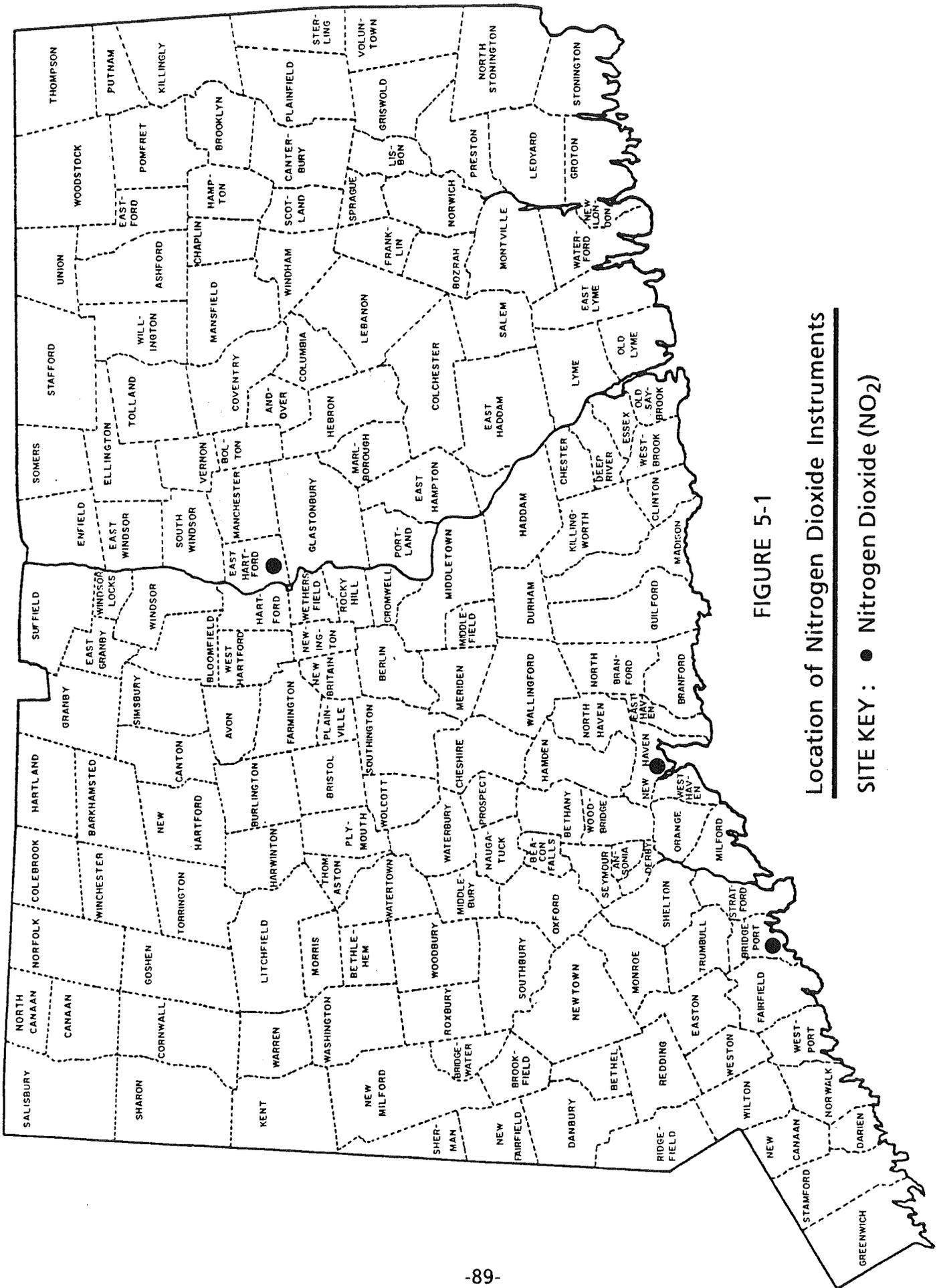


FIGURE 5-1  
 Location of Nitrogen Dioxide Instruments  
 SITE KEY : ● Nitrogen Dioxide (NO<sub>2</sub>)

**TABLE 5-1**  
**1988 -1990 NITROGEN DIOXIDE ANNUAL AVERAGES**

| <u>Town Name</u> | <u>Site</u> | <u>Year</u> | <u>Samples</u> | <u>Arithmetic Mean</u> | <u>95-Percent-Limits Lower</u> | <u>95-Percent-Limits Upper</u> | <u>Standard Deviation</u> |
|------------------|-------------|-------------|----------------|------------------------|--------------------------------|--------------------------------|---------------------------|
| Bridgeport       | 013         | 1988        | 8674           | 51.03                  | 50.97                          | 51.10                          | 27.18                     |
| Bridgeport       | 013         | 1989        | 7886           | 48.10                  | 47.92                          | 48.28                          | 25.58                     |
| Bridgeport       | 013         | 1990        | 8137           | 47.97                  | 47.82                          | 48.12                          | 25.98                     |
| East Hartford    | 003         | 1988        | 8702           | 38.42                  | 38.37                          | 38.47                          | 23.39                     |
| East Hartford    | 003         | 1989        | 8038           | 38.33                  | 38.20                          | 38.47                          | 21.79                     |
| East Hartford    | 003         | 1990        | 8287           | 35.92                  | 35.81                          | 36.03                          | 21.71                     |
| New Haven        | 123         | 1988        | 8695           | 55.26                  | 55.21                          | 55.32                          | 26.38                     |
| New Haven        | 123         | 1989        | 8221           | 53.54                  | 53.41                          | 53.66                          | 23.85                     |
| New Haven        | 123         | 1990        | 8343           | 50.73                  | 50.61                          | 50.84                          | 24.42                     |

N.B. The arithmetic mean and standard deviation have units of  $\mu\text{g}/\text{m}^3$ .

TABLE 5-2

1990 TEN HIGHEST 1-HOUR AVERAGE NO2 DAYS WITH WIND DATA

UNITS : PARTS PER MILLION

| TOWN-SITE (SAMPLES)            | RANK      | 1       | 2       | 3       | 4       | 5        | 6      | 7       | 8        | 9        | 10      |
|--------------------------------|-----------|---------|---------|---------|---------|----------|--------|---------|----------|----------|---------|
| BRIDGEPORT-013 (8137)          | NO2       | .147    | .111    | .105    | .090    | .088     | .088   | .086    | .084     | .083     | .083    |
| METEOROLOGICAL SITE NEWARK     | DATE      | 3/15/90 | 11/2/90 | 4/27/90 | 3/11/90 | 1/17/90  | 3/9/90 | 4/28/90 | 1/16/90  | 3/13/90  | 5/9/90  |
|                                | DIR (DEG) | 180     | 230     | 210     | 220     | 190      | 230    | 150     | 240      | 270      | 220     |
|                                | VEL (MPH) | 1.4     | 6.8     | 4.5     | 3.3     | 5.8      | 3.2    | 4.7     | 5.3      | 7.8      | 6.6     |
|                                | SPD (MPH) | 4.9     | 8.5     | 6.5     | 5.3     | 6.3      | 6.0    | 6.8     | 6.6      | 8.9      | 8.9     |
|                                | RATIO     | 0.284   | 0.805   | 0.692   | 0.618   | 0.912    | 0.538  | 0.698   | 0.809    | 0.873    | 0.739   |
| METEOROLOGICAL SITE BRADLEY    | DATE      | 190     | 200     | 310     | 40      | 180      | 220    | 0.912   | 180      | 350      | 190     |
|                                | DIR (DEG) | 2.2     | 4.3     | 3.5     | 2.5     | 6.2      | 1.5    | 1.3     | 4.1      | 3.7      | 8.0     |
|                                | VEL (MPH) | 5.0     | 6.3     | 6.5     | 6.8     | 8.1      | 4.5    | 6.6     | 6.5      | 6.2      | 8.1     |
|                                | SPD (MPH) | 0.444   | 0.682   | 0.543   | 0.371   | 0.772    | 0.327  | 0.190   | 0.631    | 0.596    | 0.996   |
| METEOROLOGICAL SITE BRIDGEPORT | DATE      | 250     | 260     | 260     | 260     | 170      | 180    | 250     | 260      | 280      | 230     |
|                                | DIR (DEG) | 2.9     | 4.5     | 5.8     | 5.4     | 1.4      | 1.1    | 3.3     | 4.6      | 3.4      | 3.8     |
|                                | VEL (MPH) | 4.2     | 4.6     | 6.0     | 5.5     | 4.6      | 2.3    | 4.2     | 4.7      | 5.2      | 4.2     |
|                                | SPD (MPH) | 0.686   | 0.988   | 0.967   | 0.988   | 0.306    | 0.470  | 0.784   | 0.969    | 0.657    | 0.921   |
| METEOROLOGICAL SITE WORCESTER  | DATE      | 260     | 260     | 310     | 280     | 210      | 200    | 360     | 290      | 290      | 250     |
|                                | DIR (DEG) | 2.8     | 7.6     | 6.4     | 7.2     | 5.0      | 1.1    | 2.8     | 5.9      | 7.9      | 8.0     |
|                                | VEL (MPH) | 4.2     | 8.2     | 6.6     | 7.8     | 5.8      | 3.9    | 7.0     | 6.0      | 8.3      | 8.3     |
|                                | SPD (MPH) | 0.675   | 0.926   | 0.967   | 0.928   | 0.864    | 0.293  | 0.392   | 0.980    | 0.952    | 0.959   |
| EAST HARTFORD-003 (8287)       | NO2       | .091    | .088    | .088    | .079    | .071     | .069   | .068    | .068     | .067     | .064    |
| METEOROLOGICAL SITE NEWARK     | DATE      | 3/15/90 | 1/17/90 | 11/2/90 | 1/23/90 | 11/16/90 | 5/9/90 | 11/1/90 | 3/9/90   | 11/15/90 | 4/27/90 |
|                                | DIR (DEG) | 180     | 190     | 230     | 270     | 210      | 220    | 200     | 230      | 220      | 210     |
|                                | VEL (MPH) | 1.4     | 5.8     | 6.8     | 4.8     | 6.8      | 6.6    | 2.7     | 3.2      | 8.1      | 4.5     |
|                                | SPD (MPH) | 4.9     | 6.3     | 8.5     | 8.9     | 8.5      | 8.9    | 5.5     | 6.0      | 9.5      | 6.5     |
|                                | RATIO     | 0.284   | 0.912   | 0.805   | 0.538   | 0.803    | 0.739  | 0.501   | 0.538    | 0.853    | 0.692   |
| METEOROLOGICAL SITE BRADLEY    | DATE      | 190     | 180     | 200     | 220     | 180      | 190    | 80      | 220      | 170      | 310     |
|                                | DIR (DEG) | 2.2     | 6.2     | 4.3     | 2.4     | 7.0      | 8.0    | .6      | 1.5      | 6.3      | 3.5     |
|                                | VEL (MPH) | 5.0     | 8.1     | 6.3     | 4.5     | 9.9      | 8.1    | 3.3     | 4.5      | 7.5      | 6.5     |
|                                | SPD (MPH) | 0.444   | 0.772   | 0.682   | 0.541   | 0.701    | 0.996  | 0.183   | 0.327    | 0.836    | 0.543   |
| METEOROLOGICAL SITE BRIDGEPORT | DATE      | 250     | 170     | 260     | 280     | 260      | 230    | 260     | 180      | 260      | 260     |
|                                | DIR (DEG) | 2.9     | 1.4     | 4.5     | 3.6     | 5.6      | 3.8    | 1.9     | 1.1      | 8.7      | 5.8     |
|                                | VEL (MPH) | 4.2     | 4.6     | 4.6     | 6.0     | 5.9      | 4.2    | 3.9     | 2.3      | 9.1      | 6.0     |
|                                | SPD (MPH) | 0.686   | 0.306   | 0.988   | 0.603   | 0.951    | 0.921  | 0.489   | 0.470    | 0.965    | 0.967   |
| METEOROLOGICAL SITE WORCESTER  | DATE      | 260     | 210     | 260     | 280     | 250      | 250    | 280     | 200      | 270      | 310     |
|                                | DIR (DEG) | 2.8     | 5.0     | 7.6     | 4.9     | 8.6      | 8.0    | 5.9     | 1.1      | 10.6     | 6.4     |
|                                | VEL (MPH) | 4.2     | 5.8     | 8.2     | 5.3     | 8.8      | 8.3    | 6.2     | 3.9      | 10.6     | 6.6     |
|                                | SPD (MPH) | 0.675   | 0.864   | 0.926   | 0.922   | 0.985    | 0.959  | 0.960   | 0.293    | 0.998    | 0.967   |
| NEW HAVEN-123 (8343)           | NO2       | .122    | .122    | .116    | .093    | .089     | .084   | .083    | .083     | .081     | .081    |
| METEOROLOGICAL SITE NEWARK     | DATE      | 3/15/90 | 11/2/90 | 3/13/90 | 11/3/90 | 11/1/90  | 2/8/90 | 1/17/90 | 11/16/90 | 4/27/90  | 1/9/90  |
|                                | DIR (DEG) | 180     | 230     | 270     | 240     | 200      | 180    | 190     | 210      | 210      | 200     |
|                                | VEL (MPH) | 1.4     | 6.8     | 7.8     | 5.3     | 2.7      | 3.4    | 5.8     | 6.8      | 4.5      | 5.0     |
|                                | SPD (MPH) | 4.9     | 8.5     | 8.9     | 7.6     | 5.5      | 5.3    | 6.3     | 8.5      | 6.5      | 6.2     |
|                                | RATIO     | 0.284   | 0.805   | 0.873   | 0.696   | 0.501    | 0.631  | 0.912   | 0.803    | 0.692    | 0.806   |
| METEOROLOGICAL SITE BRADLEY    | DATE      | 190     | 200     | 350     | 240     | 80       | 170    | 180     | 180      | 310      | 170     |
|                                | DIR (DEG) | 2.2     | 4.3     | 3.7     | 2.9     | .6       | 6.1    | 6.2     | 7.0      | 3.5      | 5.6     |
|                                | VEL (MPH) | 5.0     | 6.3     | 6.2     | 7.2     | 3.3      | 7.2    | 8.1     | 9.9      | 6.5      | 7.0     |
|                                | SPD (MPH) | 0.444   | 0.682   | 0.596   | 0.402   | 0.183    | 0.855  | 0.772   | 0.701    | 0.543    | 0.790   |

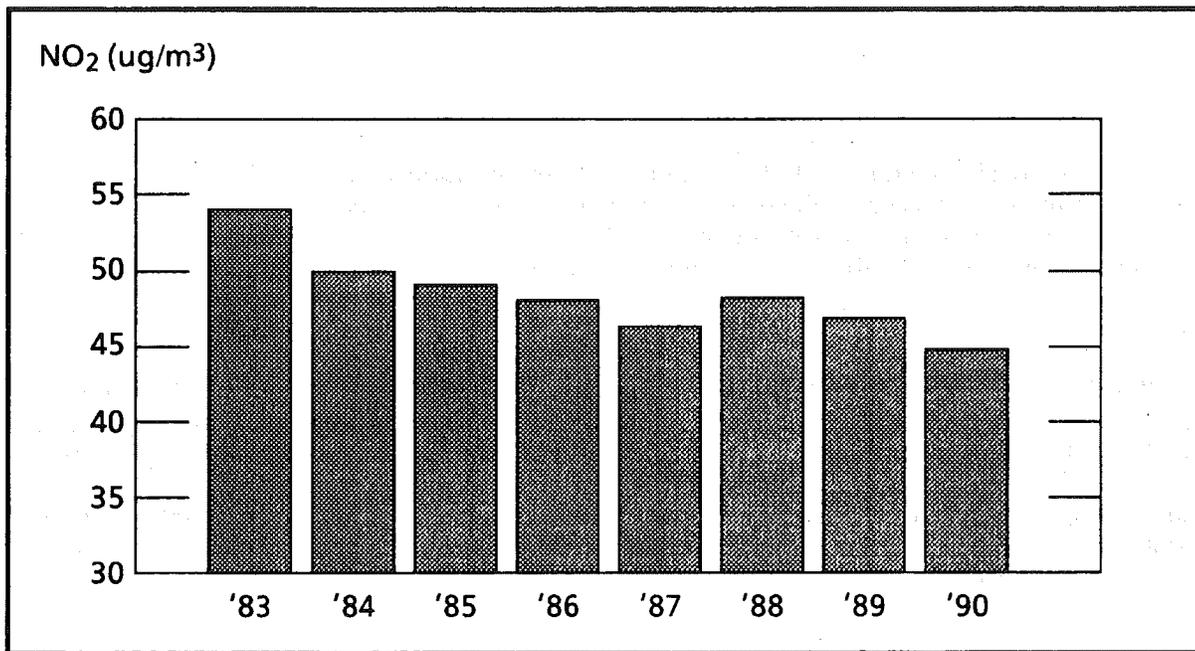
TABLE 5-2, CONTINUED

1990 TEN HIGHEST 1-HOUR AVERAGE NO2 DAYS WITH WIND DATA

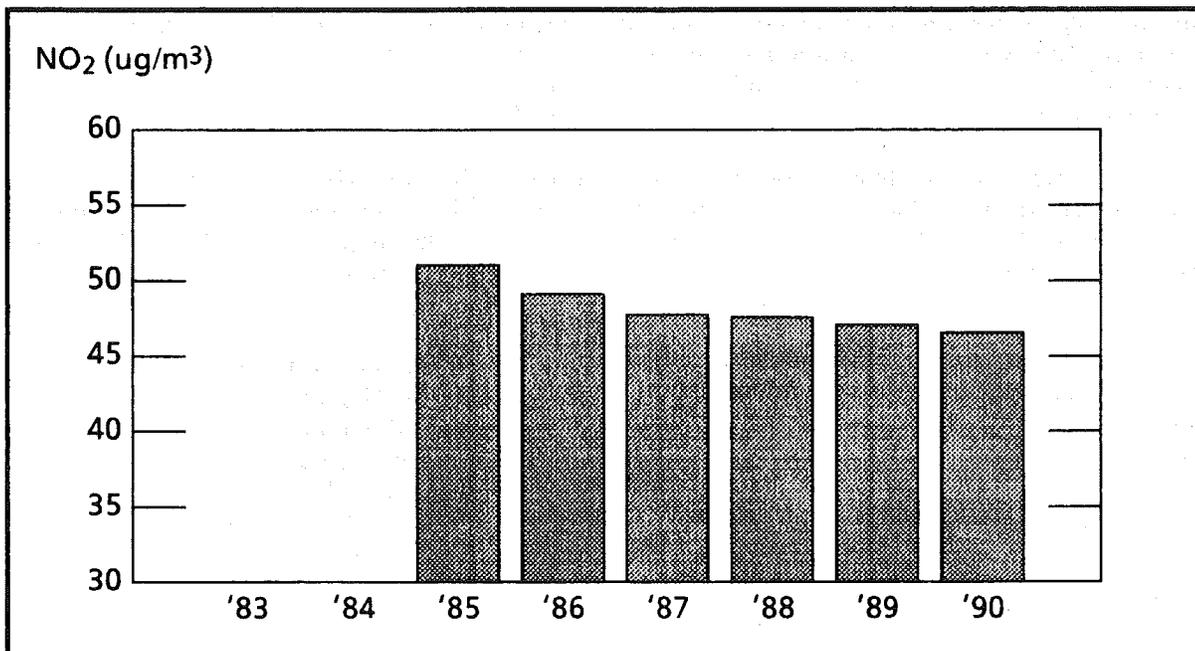
UNITS : PARTS PER MILLION

| TOWN-SITE (SAMPLES)               | RANK      | 1     | 2     | 3     | 4     | 5     | 6     | 7     | 8     | 9     | 10    |
|-----------------------------------|-----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG) | 250   | 260   | 280   | 260   | 260   | 250   | 170   | 260   | 260   | 240   |
|                                   | VEL (MPH) | 2.9   | 4.5   | 3.4   | 5.4   | 1.9   | 4.9   | 1.4   | 5.6   | 5.8   | 5.4   |
|                                   | SPD (MPH) | 4.2   | 4.6   | 5.2   | 5.5   | 3.9   | 5.6   | 4.6   | 5.9   | 6.0   | 5.9   |
|                                   | RATIO     | 0.686 | 0.988 | 0.657 | 0.989 | 0.489 | 0.875 | 0.306 | 0.951 | 0.967 | 0.909 |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG) | 260   | 260   | 290   | 300   | 280   | 250   | 210   | 250   | 310   | 230   |
|                                   | VEL (MPH) | 2.8   | 7.6   | 7.9   | 10.1  | 5.9   | 7.2   | 5.0   | 8.6   | 6.4   | 6.1   |
|                                   | SPD (MPH) | 4.2   | 8.2   | 8.3   | 10.2  | 6.2   | 7.6   | 5.8   | 8.8   | 6.6   | 6.5   |
|                                   | RATIO     | 0.675 | 0.926 | 0.952 | 0.992 | 0.960 | 0.947 | 0.864 | 0.985 | 0.967 | 0.938 |

**FIGURE 5-2**  
**AVERAGES OF THE ANNUAL NO<sub>2</sub> CONCENTRATIONS AT THREE SITES**



**FIGURE 5-3**  
**3-YEAR AVERAGES OF THE ANNUAL NO<sub>2</sub> CONCENTRATIONS AT THREE SITES**



## VI. CARBON MONOXIDE

### HEALTH EFFECTS

Carbon monoxide (CO) is a colorless, odorless, poison gas formed when carbon-containing fuel is not burned completely. It is by far the most plentiful air pollutant. Fortunately, this deadly gas does not persist in the atmosphere. It is apparently converted by natural processes to harmless carbon dioxide in ways not yet understood, and this is done quickly enough to prevent any general buildup. However, CO can reach dangerous levels in local areas, such as city-street canyons with heavy auto traffic and little wind.

Clinical experience with accidental CO poisoning has shown clearly how it affects the body. When the gas is breathed, CO replaces oxygen in the red blood cells, reducing the amount of oxygen that can reach the body cells and maintain life. Lack of oxygen affects the brain, and the first symptoms are impaired perception and thinking. Reflexes are slowed, judgement weakened, and drowsiness ensues. An auto driver breathing high levels of CO is more likely to have an accident; an athlete's performance and skill drop suddenly. Lack of oxygen then affects the heart. Death can come from heart failure or general asphyxiation if a person is exposed to very high levels of CO.

### CONCLUSIONS

The eight-hour National Ambient Air Quality Standard of 9 parts per million (ppm) was not exceeded at any of the five carbon monoxide monitoring sites in Connecticut during 1990. Nor was an exceedance of the 35 ppm one-hour standard measured at any site in 1990.

In order to put the monitoring data into proper perspective, it must be realized that carbon monoxide concentrations vary greatly from place-to-place. More than 95% of the CO emissions in Connecticut come from motor vehicles. Therefore, concentrations are greatest in areas of traffic congestion. The magnitude and frequency of high concentrations observed at any monitoring site are not necessarily indicative of widespread CO levels. In fact, CO monitors in Connecticut are sited specifically to measure CO levels in neighborhoods and at traffic intersections.

The CO standards are likely to be exceeded in any city in the state where there are areas of traffic congestion. However, as Connecticut's SIP control strategies are implemented, there should continue to be a decrease in the number of congested areas. Also, as federally - mandated controls which reduce emissions from new motor vehicles are implemented, a reduction in ambient CO levels should be achieved.

Unlike SO<sub>2</sub>, particulate matter, and O<sub>3</sub>, elevated CO levels are not often associated with southwesterly winds, indicating that this pollutant is more of a local-scale, rather than a regional-scale, problem. Moreover, high CO levels tend to occur during the colder months when there are low atmospheric mixing heights, stable conditions and high CO auto emissions due to cold engine operation. Stable conditions, which are characterized by cold temperatures at the surface and warm temperatures aloft, discourage surface mixing and result in calm surface conditions. With little or no surface winds, CO emissions can accumulate to unhealthy levels.

## METHOD OF MEASUREMENT

The DEP Air Monitoring Unit uses instruments employing a non-dispersive infrared technique to continuously measure carbon monoxide levels. The instantaneous concentrations are electronically recorded at the site, averaged for each hour, and stored for transmission to the central computer in Hartford. Due to the relative inertness of CO, a long sampling line can be used without the danger of CO being depleted by chemical reactions within the lines. The most important consideration in the measurement of CO is the placement of the sampling probe inlet -- that is, its proximity to traffic lanes.

## DISCUSSION OF DATA

**Monitoring Network** - The network in 1990 consisted of five carbon monoxide monitors: Bridgeport 004, Hartford 013, Hartford 017, New Haven 019, and Stamford 020. They are all located in urban areas. All the sites are also located west of the Connecticut River, with three of them in coastal towns (see Figure 6-1).

**Precision and Accuracy** - The carbon monoxide monitors had a total of 210 precision checks during 1990. The resulting 95% probability limits were -3% to +7%. Accuracy is determined by introducing a known amount of CO into each of the monitors. Five audits for accuracy were conducted on the monitoring network in 1990. Three different concentration levels were tested on each monitor: low, medium and high. The 95% probability limits ranged from -6% to +11% for the low level test; -4% to +3% for the medium level test; and -4% to +5% for the high level test.

**8-Hour and 1-Hour Averages** - An 8-hour concentration is said to exceed the standard of 9 ppm if it is equal to or greater than 9.5 ppm. No site had a CO concentration exceeding the 8-hour standard, which means that the standard was not violated in Connecticut in 1990 (see Table 6-1).

Regarding the maximum 8-hour running average at each site, there were increases from 1989 to 1990 at Bridgeport 004, New Haven 019 and Stamford 020, and there were decreases at Hartford 013 and Hartford 017. The second highest 8-hour running average decreased from 1989 to 1990 at Bridgeport 004 and Hartford 017, and increased at Hartford 013 and New Haven 019. There was no change at Stamford 020.

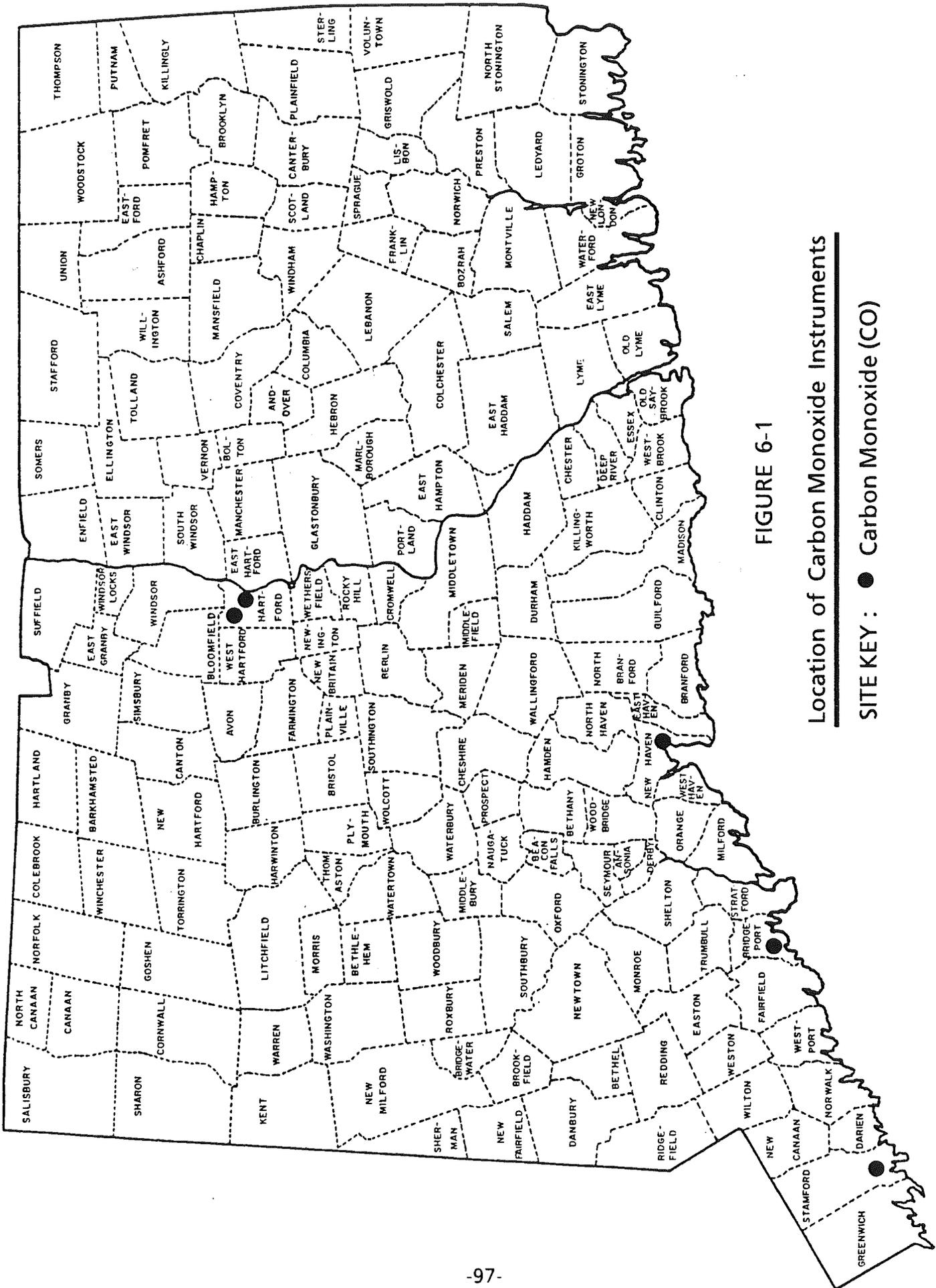
As for 1-hour averages, no site in the state recorded a value exceeding the primary 1-hour standard of 35 ppm. Bridgeport 004, New Haven 019 and Stamford 020 recorded maximum 1-hour values that were higher than the year before, while Hartford 013 and Hartford 017 had lower values. Second high 1-hour values were higher in 1990 at all the sites except Hartford 013.

The maximum and second high CO concentrations at each site are presented in Table 6-1. Table 6-2 presents monthly highs and a monthly tally of the number of times the standards were exceeded at each site. Seasonal variations in CO levels can be observed using this table.

**Trends** - Due to the local nature of CO emissions, it is not appropriate to give an estimate of widespread CO trends. However, local CO trends can be addressed in a number of ways. Exceedances of the 8-hour standard can be tracked in order to determine if a CO problem is worsening or abating at a site. This is illustrated in Table 6-3 and in Figure 6-2. One can see that over the past five years the Hartford-017 site has shown a higher frequency of exceedances relative to the other sites, with a downward trend after 1987. No exceedances are evident at Bridgeport 004, Hartford 013 or New Haven 019, and there are no exceedances at Stamford 020 after 1986. For this reason, these sites are excluded from Figure 6-2.

Another way of illustrating local CO trends is to use running averages. Running averages have the advantage of smoothing out the abrupt, transitory changes in pollutant levels that are often evident in

consecutive sampling periods and from one season to the next. Figure 6-3 shows the 36-month running averages of the hourly CO concentrations at each monitoring site. CO levels appear to be flattening out at Bridgeport 004 and Stamford 020 after trending down for some years, while they continue to trend down at Hartford 017. The Hartford 013 and New Haven 019 sites have fewer data, and CO levels at these sites appear to be either flat or rising slightly.



**FIGURE 6-1**  
**Location of Carbon Monoxide Instruments**  
**SITE KEY : ● Carbon Monoxide (CO)**

**TABLE 6-1**

**1990 CARBON MONOXIDE STANDARDS ASSESSMENT SUMMARY**

| <u>TOWN-SITE</u>          | <u>TIME OF</u>   |  | <u>2ND HIGH</u>  |  | <u>TIME OF</u>   |  | <u>2ND HIGH</u>  |  | <u>TIME OF</u>   |  | <u>2ND HIGH</u>  |  |
|---------------------------|--|--|--|--|--|--|--|--|--|--|--|--|
|                           | <u>MAXIMUM</u><br><u>8-HOUR</u><br><u>RUNNING</u><br><u>AVERAGE</u> <sup>1</sup> | <u>8-HOUR</u><br><u>RUNNING</u><br><u>AVERAGE</u> <sup>1</sup> | <u>8-HOUR</u><br><u>RUNNING</u><br><u>AVERAGE</u> <sup>1</sup> | <u>8-HOUR</u><br><u>RUNNING</u><br><u>AVERAGE</u> <sup>1</sup> | <u>MAXIMUM</u><br><u>1-HOUR</u><br><u>AVERAGE</u> <sup>2</sup> |
| Bridgeport-004            | 6.1  | 01/17/01   | 5.0  | 11/02/03   | 9.3  | 01/16/23   | 8.5  | 01/16/18   |  |  |  |  |
| Hartford-013              | 4.8  | 11/02/02   | 4.7  | 02/08/02   | 6.4  | 02/08/08   | 6.0  | 11/26/22   |  |  |  |  |
| Hartford-017 <sup>3</sup> | 9.3  | 02/07/22   | 8.6  | 01/24/20   | 19.3   | 02/07/18   | 15.8   | 02/07/17   |  |  |  |  |
| New Haven-019             | 7.2  | 01/16/24   | 6.8  | 03/11/24   | 11.8   | 01/16/18   | 9.9  | 11/02/15   |  |  |  |  |
| Stamford-020              | 7.4  | 01/24/24   | 6.0  | 01/16/24   | 10.5   | 01/24/21   | 10.0   | 02/09/09   |  |  |  |  |

<sup>1</sup> The time of the 8-hour average is reported as follows: month/day/hour (EST), specifying the end of the 8-hour period.

<sup>2</sup> The time of the 1-hour average is reported as follows: month/day/hour (EST), specifying the end of the 1-hour period.

<sup>3</sup> No data exist for April through most of October due to road construction.

N.B. The CO averages are expressed in terms of parts per million (ppm).

TABLE 6-2

1990 CARBON MONOXIDE SEASONAL FEATURES

| <u>TOWN-SITE</u> | <u>JAN</u>                | <u>FEB</u> | <u>MAR</u> | <u>APR</u> | <u>MAY</u> | <u>JUN</u> | <u>JUL</u> | <u>AUG</u> | <u>SEP</u> | <u>OCT</u> | <u>NOV</u> | <u>DEC</u> |
|------------------|---------------------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| Bridgeport-004   | Max. 1-Hour               | 9.3        | 6.6        | 6.1        | 4.2        | 2.7        | 2.5        | 2.9        | 6.7        | 3.6        | 5.3        | 7.6        |
|                  | Max. Running 8-Hour       | 6.1        | 4.0        | 3.8        | 3.2        | 2.3        | 2.0        | 2.0        | 3.5        | 2.8        | 3.0        | 4.9        |
|                  | No. of 8-Hour Exceedances | 0          | 0          | 0          | 0          | 0          | 0          | 0          | 0          | 0          | 0          | 0          |
| Hartford-013     | Max. 1-Hour               | 5.5        | 6.4        | 3.1        | 3.5        | 2.0        | 2.7        | 2.2        | 2.3        | 3.5        | 4.0        | 3.4        |
|                  | Max. Running 8-Hour       | 4.0        | 4.7        | 2.2        | 1.8        | 1.1        | 2.1        | 1.2        | 1.7        | 1.9        | 2.7        | 2.7        |
|                  | No. of 8-Hour Exceedances | 0          | 0          | 0          | 0          | 0          | 0          | 0          | 0          | 0          | 0          | 0          |
| Hartford-017*    | Max. 1-Hour               | 15.4       | 19.3       | 11.6       |            |            |            |            |            | 8.0        | 10.5       | 8.9        |
|                  | Max. Running 8-Hour       | 8.6        | 9.3        | 6.2        |            |            |            |            |            | 4.4        | 6.9        | 5.3        |
|                  | No. of 8-Hour Exceedances | 0          | 0          | 0          | 0          | 0          | 0          | 0          | 0          | 0          | 0          | 0          |
| New Haven-019    | Max. 1-Hour               | 11.8       | 7.0        | 9.5        | 6.1        | 4.2        | 4.3        | 4.0        | 4.3        | 4.4        | 9.9        | 6.7        |
|                  | Max. Running 8-Hour       | 7.2        | 4.6        | 6.8        | 4.7        | 3.2        | 3.3        | 3.3        | 3.2        | 3.5        | 6.7        | 5.2        |
|                  | No. of 8-Hour Exceedances | 0          | 0          | 0          | 0          | 0          | 0          | 0          | 0          | 0          | 0          | 0          |
| Stamford-020     | Max. 1-Hour               | 10.5       | 10.0       | 6.1        | 4.8        | 4.7        | 4.3        | 4.3        | 4.0        | 5.6        | 7.4        | 9.3        |
|                  | Max. Running 8-Hour       | 7.4        | 6.0        | 4.6        | 3.2        | 3.5        | 3.1        | 3.0        | 3.3        | 3.2        | 3.9        | 5.9        |
|                  | No. of 8-Hour Exceedances | 0          | 0          | 0          | 0          | 0          | 0          | 0          | 0          | 0          | 0          | 0          |

\* No data exist for April through most of October due to road construction.

N.B. The CO concentrations are in terms of parts per million (ppm).

## TABLE 6-3

### EXCEEDANCES OF THE 8-HOUR CO STANDARD FOR 1986 -1990

| <u>SITE</u>    | <u>1986</u>    | <u>1987</u>    | <u>1988</u> | <u>1989</u> | <u>1990</u>    |
|----------------|----------------|----------------|-------------|-------------|----------------|
| Bridgeport-004 | 0              | 0              | 0           | 0           | 0              |
| Hartford-013   | -              | 0 <sup>a</sup> | 0           | 0           | 0 <sup>b</sup> |
| Hartford-017   | 3              | 8              | 3           | 1           | 0              |
| New Haven-019  | 0 <sup>c</sup> | 0              | 0           | 0           | 0              |
| Stamford-020   | 1              | 0              | 0           | 0           | 0              |

<sup>a</sup> Data are missing for January and February.

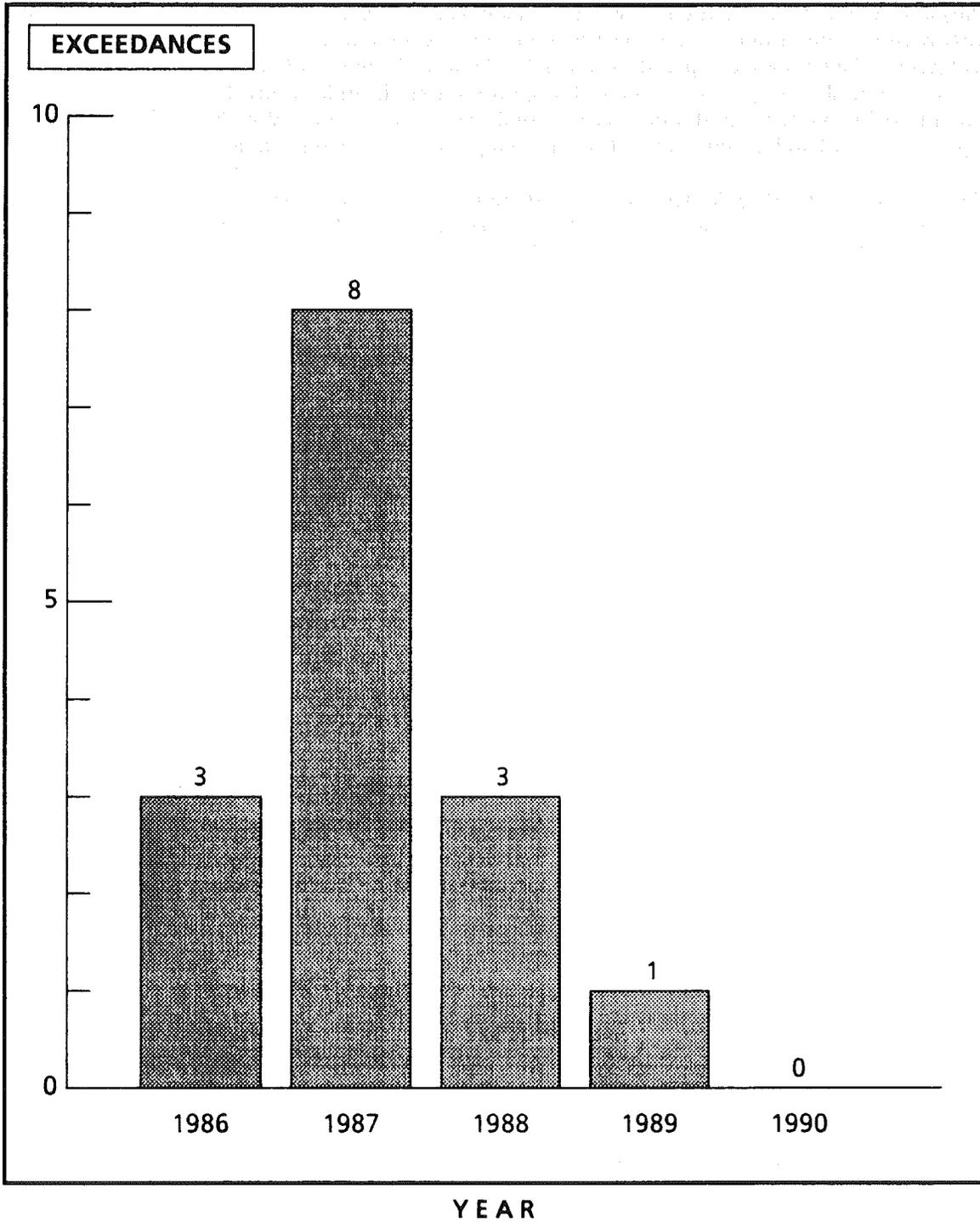
<sup>b</sup> Data are missing for April through most of October due to road construction.

<sup>c</sup> Data are missing for January through March.

**FIGURE 6-2**

**EXCEEDANCES OF THE 8-HOUR CO STANDARD FOR 1986-1990**

**SITE: HARTFORD-017**



## IX. CLIMATOLOGICAL DATA

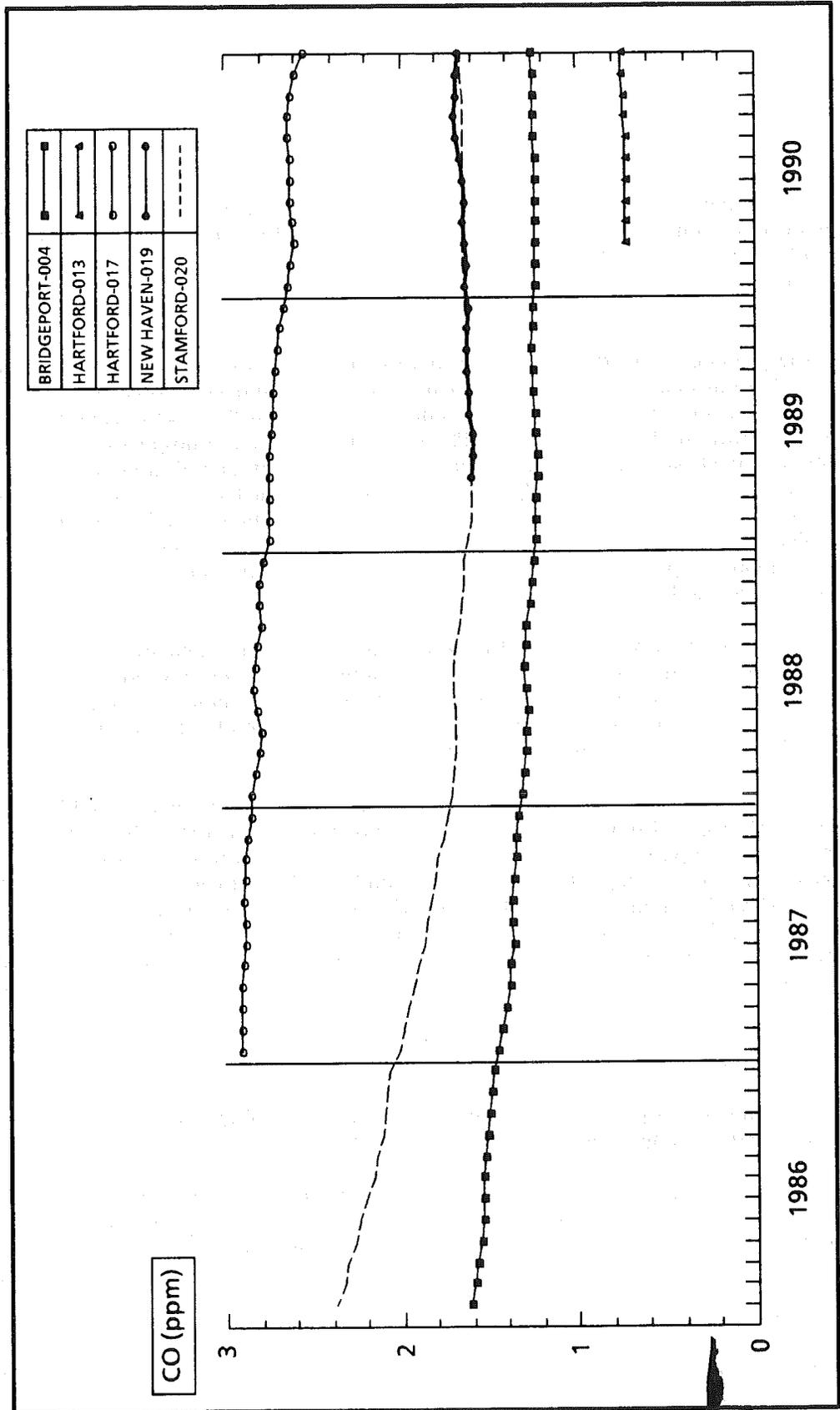
Weather is often the most significant factor influencing short-term changes in air quality. It also has an affect on long-term trends. Climatological information from the National Weather Service station at Bradley International Airport in Windsor Locks is shown in Table 9-1 for the years 1989 and 1990. Table 9-2 contains information from the National Weather Service station located at Sikorsky Memorial Airport near Bridgeport. All data are compared to "mean" or "normal" values. Wind speeds<sup>1</sup> and temperatures are shown as monthly and yearly averages. Precipitation data includes both the number of days with more than 0.01 inches of precipitation and the total water equivalent. Also shown are degree days<sup>2</sup> (heating requirement) and the number of days with temperatures exceeding 90°F.

Wind roses for Bradley Airport and Newark Airport have been developed from 1990 National Weather Service surface observations and are shown in Figures 9-2 and 9-4, respectively. Wind roses from these stations for 1989 are shown in Figures 9-1 and 9-3, respectively.

<sup>1</sup> The mean wind speed for a month or year is calculated from all the hourly wind speeds, regardless of the wind directions.

<sup>2</sup> The degree day value for each day is arrived at by subtracting the average temperature of the day from 65°F. This number (65) is used as a base value because it is assumed that there is no heating requirement when the outside temperature is 65°F.

**FIGURE 6-3**  
**36-MONTH RUNNING AVERAGES OF THE HOURLY CO CONCENTRATIONS**



## VII. LEAD

### HEALTH EFFECTS

Lead (Pb) is a soft, dull gray, odorless and tasteless heavy metal. It is a ubiquitous element that is widely distributed in small amounts, particularly in soil and in all living things. Although the metallic form of lead is reactive and rarely occurs in nature, lead is prevalent in the environment in the form of various inorganic compounds, and occasional concentrated deposits of lead compounds occur in the earth's crust.

The presence of lead in the atmosphere is primarily accounted for by the emissions of lead compounds from man-made processes, such as the extraction and processing of metallic ores, the incineration of solid wastes, and the operation of motor vehicles. Nationally, in 1990, these source categories contributed 31%, 31% and 31%, respectively, of the atmospheric lead. The motor vehicle contribution, while still a large source of airborne lead emissions, has decreased significantly from a 71% share in 1985 to its current 31% and, since 1989, is no longer the largest source of airborne lead emissions. These emissions are in the form of fine-to-course particulate matter and are comprised of lead sulfate, ammonium lead halides, and lead halides, of which the chief component is lead bromochloride. The halide compounds appear to undergo chemical changes over a period of hours and are converted to lead carbonate, oxide and oxycarbonate.

The most important sources of lead in humans and other animals are ingestion of foods and beverages, inhalation of airborne lead, and the eating of non-food substances. From the standpoint of the general population, the intake of lead into the body is primarily through ingestion. The airborne lead settles out on crops and water supplies and is then ingested by the general population. The direct intake of lead from the ambient air is relatively small.

Overexposure to lead in the United States is primarily a problem in children. Age, pica, diet, nutritional status, and multiple sources of exposure serve to increase the risk of lead poisoning in children. This is especially true in the inner cities where the prevalence of lead poisoning is greatest. Overexposure to lead compounds may result in undesirable biologic effects. These effects range from reversible clinical or metabolic symptoms, which disappear after cessation of exposure, to permanent damage or death from a single extreme dose or prolonged overexposure. Clinical lead poisoning is accompanied by symptoms of intestinal cramps, peripheral nerve paralysis, anemia, and severe fatigue. Very severe exposure results in permanent neurological, renal, or cardiovascular damage or death.

### CONCLUSIONS

The Connecticut primary and secondary ambient air quality standard for lead and its compounds was not exceeded at any site in Connecticut during 1990.

The monitoring sites where the lead levels were highest were generally in urban locations with moderate to heavy traffic. In Connecticut, this is due to the fact that the primary source of lead to the atmosphere is the combustion of gasoline, which still contains trace amounts of lead.

### SAMPLE COLLECTION AND ANALYSIS

The Air Monitoring Unit used lo-vol samplers in 1990 to obtain ambient concentrations of lead. These samplers are used to collect particulate matter onto fiberglass filters. Compared to hi-vol samplers,

lo-vols operate continuously at reduced flow rates, for an entire month. This results in a one month integrated sample. The particulate matter collected on the filters is subsequently analyzed for its chemical composition. Wet chemistry techniques are used to separate the particulate matter into various components. The lead content of the particulate matter is determined using an atomic absorption spectrophotometer.

## DISCUSSION OF DATA

**Monitoring Network** - In 1990, only lo-vol samplers were operated in Connecticut to monitor lead levels (see Figure 7-1). There were 5 such samplers operated throughout the state by the DEP in areas with populations of 200,000 or more: Bridgeport, Hartford (2), New Haven and Waterbury. The samplers are situated near some of the busiest city streets and highways in order to monitor "worst-case" lead concentrations. EPA approval for lo-vol samplers was granted in February 1984.

Much of the lead monitoring network was dismantled in 1988 due to the changeover from hi-vol to PM<sub>10</sub> monitoring in the particulate matter network. By the end of that year, all but two of the hi-vol lead samplers were terminated: Hartford 013 and New Haven 013. By the end of 1989 all of the hi-vol samplers were terminated.

**Precision and Accuracy** - Due to the very low airborne lead concentrations, precision checks yield 95% probability limits that are too low to calculate. Accuracy for lead can be assessed in two ways. One is by auditing the air flow through the monitors. No audits for flow accuracy were conducted on the monitoring network in 1990. Accuracy can also be defined as the accuracy of the analysis method. This is determined by the chemical analysis of known lead samples. On this basis, 12 audits were performed on the network. Two different concentration levels were tested: high and low. The 95% probability limits for the low level ranged from -7% to +7%; those for the high level ranged from -7% to +3%.

**NAAQS** - Connecticut's ambient air quality standard for lead and its compounds, measured as elemental lead, is: 1.5 micrograms per cubic meter ( $\mu\text{g}/\text{m}^3$ ), maximum arithmetic mean averaged over three consecutive calendar months. This standard was enacted on November 2, 1981. Previously, Connecticut's lead standard was substantially identical to the national standard: 1.5  $\mu\text{g}/\text{m}^3$  for a calendar quarter-year average. The change to a 3-month running average means that a more stringent standard applies in Connecticut, since there are three times as many data blocks within a calendar year which must be below the limiting concentration of 1.5  $\mu\text{g}/\text{m}^3$ .

**3-Month Running Averages** - Three-month running average lead concentrations for 1990 are given in Table 7-1. All are significantly below the primary and secondary standard of 1.5  $\mu\text{g}/\text{m}^3$ .

**Trends** - A downward trend in measured concentrations of lead has been observed since 1977. This is due to the increasing use of unleaded gasoline. Figure 7-2 shows that the decrease in statewide ambient average lead concentrations has been commensurate with a decrease in lead emissions from gasoline combustion from 1982 to 1989. In fact, this relationship is so close it has a correlation coefficient of 0.987 (see Figure 7-3). Reliable data on the sales of leaded gasoline in Connecticut are no longer available; so lead emissions will no longer be updated in Figure 7-2. And Figure 7-3 will contain only pre-1990 data.

The downward trend in airborne lead concentrations can be expected to level off at some point in the near future, when the use of leaded gasoline is finally phased out or minimized. Lead emissions will then rise and fall with the number of vehicle miles travelled (VMT's) by the population. This is due to the fact that so-called unleaded gasoline still contains a small proportion of lead.

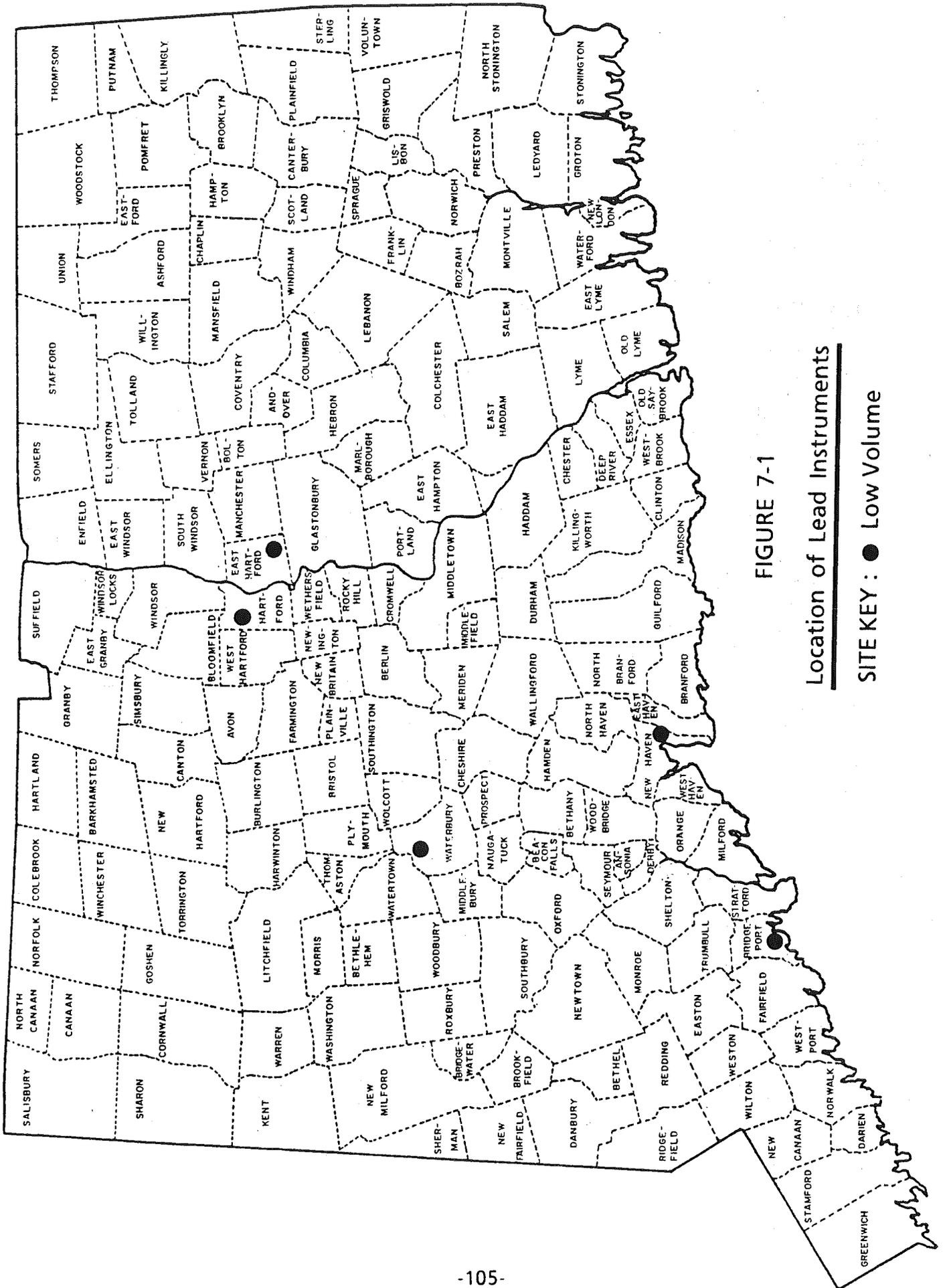


FIGURE 7-1

Location of Lead Instruments

SITE KEY : ● Low Volume

**TABLE 7-1**

**1990 3-MONTH RUNNING AVERAGE LEAD CONCENTRATIONS<sup>a</sup>**

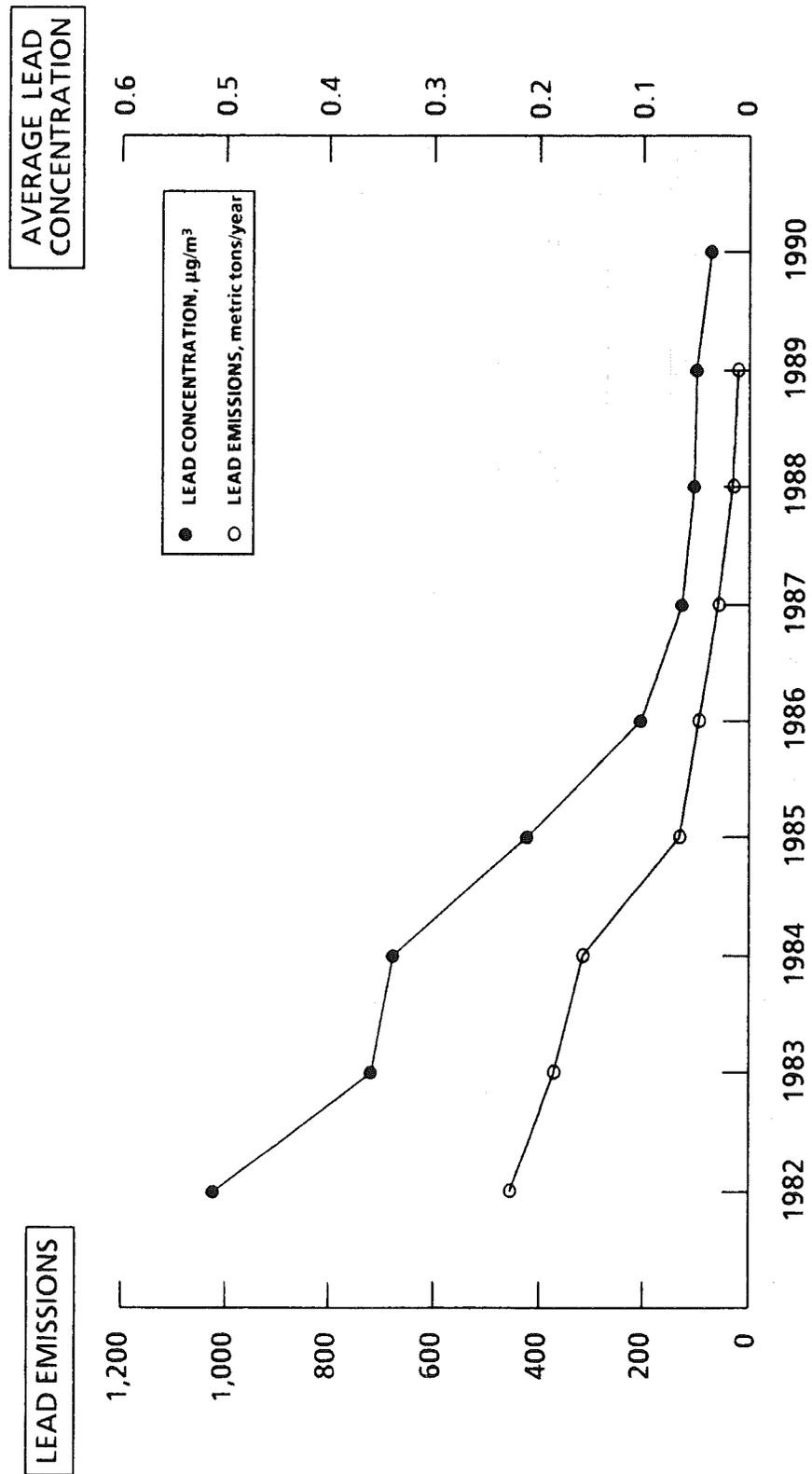
| <u>TOWN-SITE</u>           | <u>JAN</u> | <u>FEB</u> | <u>MAR</u> | <u>APR</u> | <u>MAY</u> | <u>JUN</u> | <u>JUL</u> | <u>AUG</u> | <u>SEP</u> | <u>OCT</u> | <u>NOV</u> | <u>DEC</u> |
|----------------------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| Bridgeport-010             | 0.033      | 0.033      | 0.037      | 0.033      | 0.030      | 0.027      | -----      | -----      | -----      | 0.023      | 0.023      | 0.020      |
| East Hartford-004          | 0.013      | 0.017      | -----      | -----      | -----      | -----      | 0.013      | 0.013      | 0.013      | 0.017      | 0.013      | -----      |
| Hartford-016               | 0.033      | 0.037      | 0.037      | 0.033      | 0.027      | 0.027      | 0.030      | 0.030      | 0.023      | -----      | -----      | -----      |
| New Haven-018              | -----      | -----      | 0.073      | 0.067      | 0.057      | 0.047      | 0.053      | 0.057      | 0.060      | 0.060      | 0.063      | 0.077      |
| Waterbury-123 <sup>b</sup> | 0.040      | 0.040      | 0.043      | 0.043      | -----      | -----      | -----      | -----      | -----      | 0.053      | 0.043      | -----      |

<sup>a</sup> The lead concentrations are in terms of micrograms per cubic meter ( $\mu\text{g}/\text{m}^3$ )

<sup>b</sup> The averages for August and September were omitted because they were affected by sandblasting on a local bridge

N.B. A blank area in the table indicates that a lead sampler was not in operation during the month at that site. Dashes indicate insufficient data for a 3-month average.

**FIGURE 7-2**  
STATEWIDE ANNUAL LEAD EMISSIONS FROM GASOLINE  
AND  
STATEWIDE ANNUAL AVERAGE LEAD CONCENTRATIONS

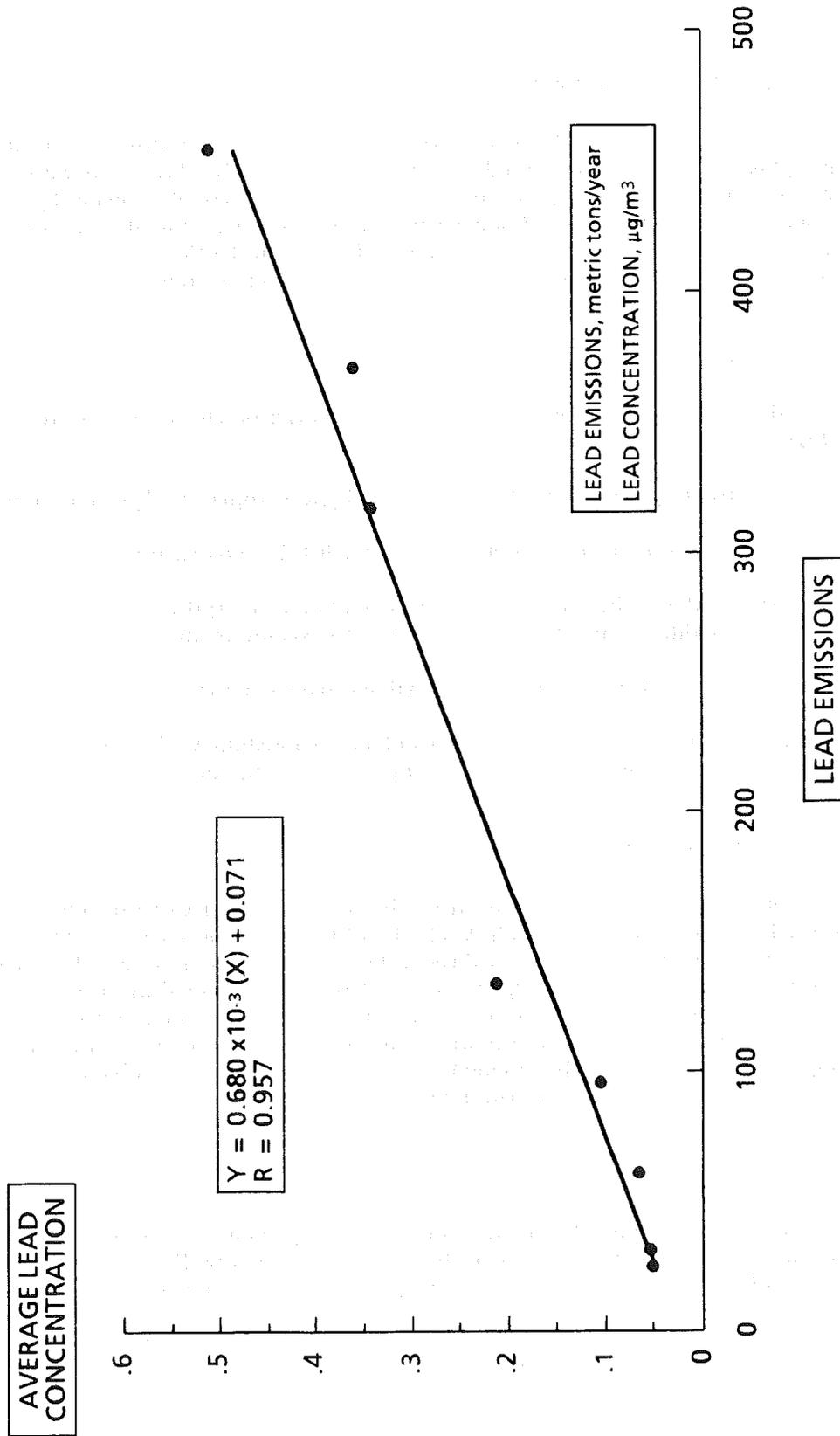


**FIGURE 7-3**

**STATEWIDE ANNUAL AVERAGE LEAD CONCENTRATIONS**

**VS.**

**STATEWIDE ANNUAL LEAD EMISSIONS FROM GASOLINE**



## VIII. ACID PRECIPITATION

### MONITORING PROGRAM

Recently, there has been a growing public concern about the occurrence and effects of atmospheric deposition, most notably acid precipitation or "acid rain." It has become apparent that, in order to address this concern, basic data need to be collected on the chemical properties of precipitation. Recognizing this, the State of Connecticut, through the Department of Environmental Protection, has agreed to cooperate with the Water Resources Division of the United States Geological Survey (USGS) to establish the Connecticut Atmospheric Deposition Monitoring Program.

### PROGRAM OBJECTIVES

The program is designed to collect and analyze precipitation on an event basis and has the following objectives:

- (1) to determine selected chemical and physical properties of precipitation in Connecticut;
- (2) to determine the spatial and temporal distribution of precipitation chemistry in the State;
- (3) to determine the relationships between precipitation chemistry and meteorological conditions, such as storm track and air mass movement;
- (4) to provide baseline information that can be used to determine trends and estimate loads; and
- (5) to use techniques and methodologies consistent with those of the national monitoring networks in order to provide comparative information.

### DATA COLLECTION SITES

Data collection sites have been established according to siting criteria used in the National Atmospheric Deposition Program (NADP). Use of these criteria ensures the validity of comparisons made between data which are collected through Connecticut's program and data from other atmospheric deposition programs. Other objectives considered during the siting process were the collection of samples representative of different geographic areas of the State, and the sampling of precipitation representative of long-range transport and not merely local sources. Using these criteria, precipitation sampling sites were established in the towns of Plainfield, Marlborough and Litchfield (Morris Dam). The locations of these sites are shown in Figure 8-1.

### EQUIPMENT

Each site is equipped with an automatic wet-dry sensing type of precipitation collector -- the same type used by the NADP and the National Trends Network (NTN). The collector operates when precipitation wets an electronic sensor, completing an electrical circuit. This activates a motor that opens a lid over the sample container when the precipitation event begins and closes the lid when the precipitation ceases. The purpose of the lid is to retard the loss of samples through evaporation and to prevent contamination by dry fallout.

Each site is also equipped with an automatic rain gage which provides a record of the quantity of rain at 15-minute intervals.

### **DATA COLLECTION**

Samples of precipitation are gathered from the automatic collectors as soon as possible following the end of a precipitation event, in most cases within 24 hours. The samples are immediately tested for acidity through pH measurements. The samples are also tested for specific conductance. This is a measure of the ions (i.e., the dissolved solids) in solution and, therefore, of the pollutant load.

Samples from selected precipitation events are also sent to a USGS laboratory for further analyses to determine the concentrations of additional chemical constituents, including major anions, cations, nutrients and trace metals.

Through the Connecticut Atmospheric Deposition Monitoring Program, a network capable of providing uninterrupted baseline data on precipitation quality within the State has been developed. Data collected through the program is currently being published monthly by the USGS in its report, Water Resources Conditions in Connecticut. Historical data are available from the Water Resources Division of the USGS or from the Natural Resources Center of the DEP at the addresses provided below. When using the data, one should note that they are specific only to the time and place of their collection.

### **DISCUSSION OF DATA**

Presently, the data that have been collected in the initial stages of the study are being analyzed to determine, on a preliminary basis, the distribution and magnitude of atmospheric deposition in Connecticut. Because precipitation chemistry is a function of air quality and climate, both of which fluctuate over time and space, several more years of continuous data collection will be necessary to develop an adequate baseline to determine trends accurately and to more fully define the controlling processes. However, a preliminary evaluation of the data indicates that the precipitation occurring within Connecticut has been chemically affected by man-made contaminants. Normal rain has a pH of 5.6, which already places it in the acidic range. The current data show that the annual mean pH of the precipitation at the 3 data collection sites has varied between 4.1 and 4.4 from 1984 through 1990. The annualized data are presented in Table 8-1 and illustrated in Figure 8-2. Further evaluation of the data may provide more information on the source of the contaminants and the effects upon the environment.

It is important to stress that it is presently difficult to forecast statewide trends in the chemical properties of precipitation, or to perform comparative analyses, because of a lack of a large long-term data base. Generally, a 20-year or greater period of record is an acceptable statistical data base. When performing comparative analyses, some hydrologic data bases use 60 years or more of record keeping. Therefore, it should be apparent that data collection under the Connecticut Atmospheric Deposition Monitoring Program must continue until a sufficient period of record has been obtained.

Further information is available from the Water Resources Division, United States Geological Survey, 450 Main Street, Hartford, Connecticut 06103 at (203) 240-3060, or from the Natural Resources Center, Department of Environmental Protection, 165 Capitol Avenue, Hartford, Connecticut 06106 at (203) 566-3540.

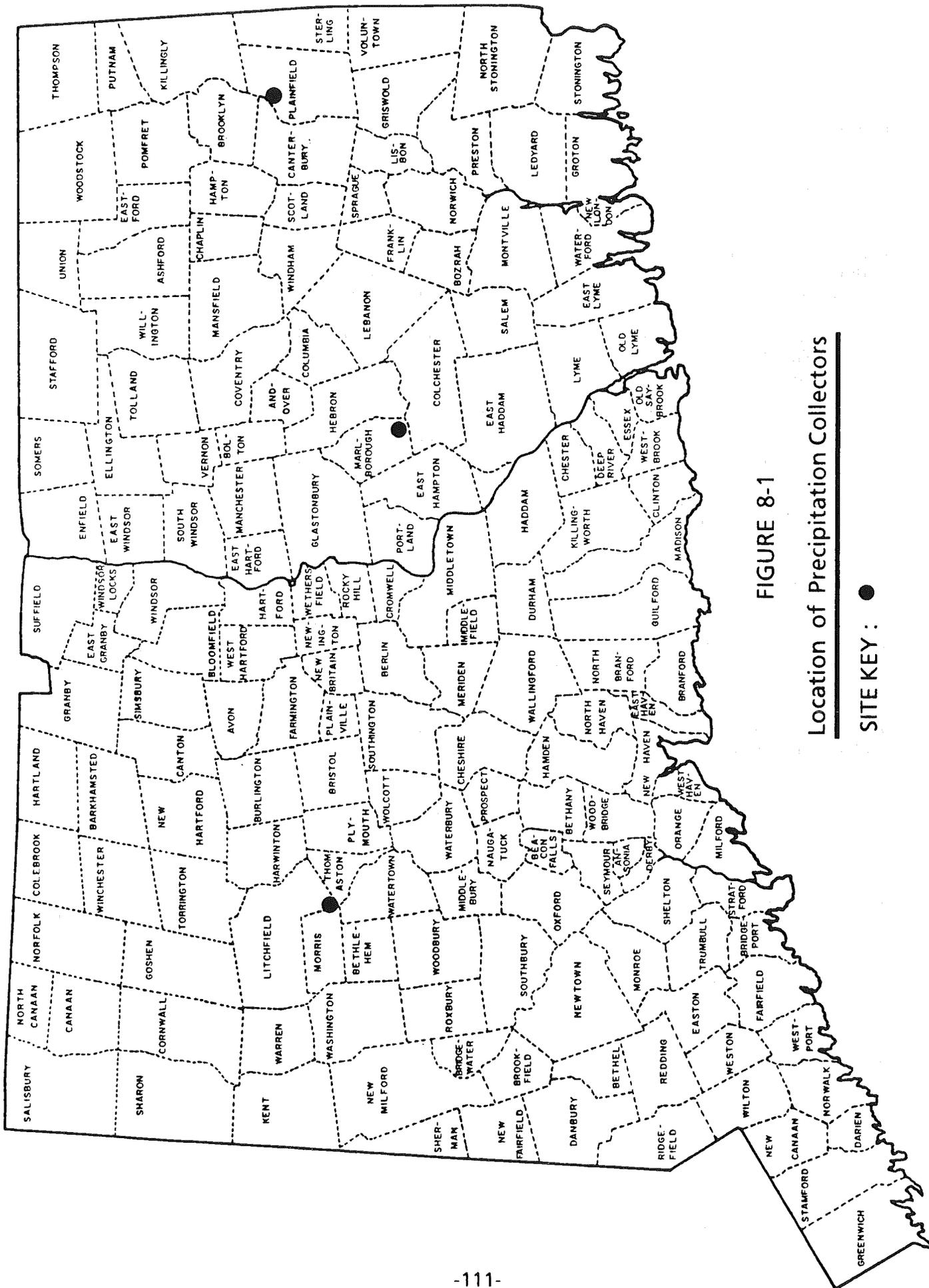


FIGURE 8-1  
 Location of Precipitation Collectors

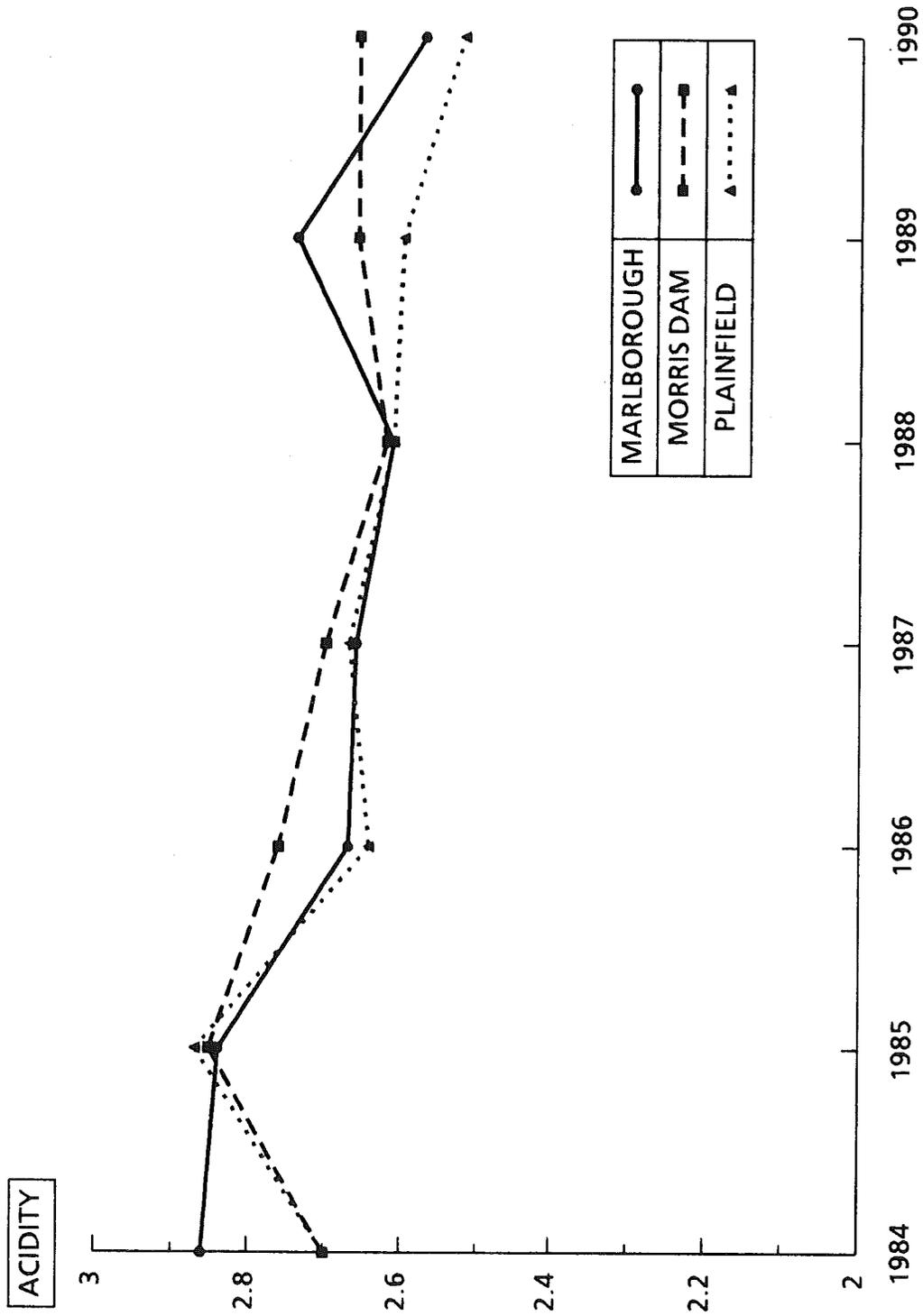
SITE KEY : ●

**TABLE 8-1**  
**ANNUAL MEAN ACIDITY OF PRECIPITATION AT 3 SITES<sup>1</sup>**

|      | Marlborough | Morris Dam | Plainfield |
|------|-------------|------------|------------|
| 1984 | 2.86        | 2.70       | 2.70       |
| 1985 | 2.84        | 2.85       | 2.87       |
| 1986 | 2.67        | 2.76       | 2.64       |
| 1987 | 2.66        | 2.70       | 2.67       |
| 1988 | 2.61        | 2.62       | 2.61       |
| 1989 | 2.74        | 2.66       | 2.60       |
| 1990 | 2.57        | 2.66       | 2.52       |

<sup>1</sup> Acidity = 7 - pH

**FIGURE 8-2**  
**ANNUAL MEAN ACIDITY OF PRECIPITATION AT 3 SITES<sup>1</sup>**



<sup>1</sup> ACIDITY = 7 - pH

TABLE 9-1

1989 AND 1990 CLIMATOLOGICAL DATA  
BRADLEY INTERNATIONAL AIRPORT, WINDSOR LOCKS

|      | AVERAGE TEMPERATURE °F |      | NO. OF DAYS WHEN MAX. TEMP. EXCEEDED 90 °F |      | DEGREE DAYS |                     | PRECIPITATION IN EQUIVALENT INCHES OF WATER |      | NO. OF DAYS WITH MORE THAN 0.01 INCHES OF PRECIPITATION |       | AVERAGE WIND SPEED (MPH) |                   |     |       |      |      |      |
|------|------------------------|------|--|------|-------------|---------------------|---|------|---|-------|--------------------------|-------------------|-----|-------|------|------|------|
|      | 1989                   | 1990 | Mean <sup>a</sup>                          | 1989 | 1990        | Normal <sup>c</sup> | 1989  | 1990 | Mean <sup>d</sup>                                       | 1989  | 1990                     | Mean <sup>d</sup> |     |       |      |      |      |
| Jan  | 30.8                   | 34.7 | 26.6                                       | 0    | 0           | 1054                | 935   | 1234 | 0.88  | 4.03  | 3.53                     | 10                | 13  | 10.7  | 9.4  | 8.7  | 9.0  |
| Feb  | 28.6                   | 33.0 | 27.8                                       | 0    | 0           | 1012                | 890   | 1047 | 1.85  | 3.37  | 3.20                     | 11                | 10  | 10.2  | 9.4  | 10.1 | 9.4  |
| Mar  | 37.4                   | 40.2 | 37.2                                       | 0    | 0           | 847                 | 763   | 874  | 3.02  | 2.46  | 3.69                     | 12                | 9   | 11.3  | 10.0 | 9.1  | 9.9  |
| Apr  | 46.5                   | 49.2 | 48.2                                       | 0    | 2           | 553                 | 478   | 486  | 3.33  | 4.55  | 3.75                     | 13                | 13  | 11.2  | 8.6  | 9.6  | 10.0 |
| May  | 60.4                   | 56.7 | 59.1                                       | 0    | 0           | 175                 | 251   | 197  | 12.00   | 6.38  | 3.72                     | 16                | 15  | 11.9  | 8.0  | 9.5  | 8.9  |
| Jun  | 68.3                   | 69.0 | 67.8                                       | 1    | 1           | 31                  | 21  | 20   | 6.65  | 3.59  | 3.59                     | 16                | 10  | 11.4  | 6.8  | 9.0  | 8.1  |
| Jul  | 72.6                   | 74.4 | 73.2                                       | 6    | 6           | 0                   | 5   | 0    | 3.40  | 2.09  | 3.55                     | 9                 | 8   | 9.7   | 6.6  | 8.1  | 7.5  |
| Aug  | 71.4                   | 73.3 | 71.0                                       | 3    | 5           | 22                  | 0   | 8    | 6.81  | 8.32  | 3.88                     | 10                | 12  | 9.9   | 6.9  | 7.6  | 7.2  |
| Sep  | 63.9                   | 64.0 | 63.5                                       | 1    | 0           | 103                 | 112   | 102  | 4.67  | 2.13  | 3.59                     | 11                | 9   | 9.4   | 7.2  | 7.7  | 7.3  |
| Oct  | 53.4                   | 57.4 | 53.0                                       | 0    | 0           | 354                 | 276   | 391  | 7.62  | 7.63  | 3.25                     | 10                | 12  | 8.4   | 8.2  | 9.3  | 7.8  |
| Nov  | 40.9                   | 44.5 | 42.1                                       | 0    | 0           | 715                 | 608   | 702  | 2.89  | 3.76  | 3.83                     | 12                | 8   | 11.1  | 10.5 | 10.2 | 8.5  |
| Dec  | 18.1                   | 36.7 | 30.3                                       | 0    | 0           | 1444                | 873   | 1113 | 1.49  | 4.86  | 3.70                     | 8                 | 12  | 11.9  | 8.8  | 9.8  | 8.7  |
| YEAR | 49.4                   | 52.8 | 50.0                                       | 11   | 14          | 6310                | 5212  | 6174 | 54.61   | 53.17 | 43.30                    | 138               | 131 | 126.9 | 8.4  | 9.1  | 8.5  |

\* Less than 0.05      Extracted From: Local Climatological Data Charts

<sup>a</sup> 1905-1990

<sup>b</sup> 1960-1990

<sup>c</sup> 1951-1980

<sup>d</sup> 1955-1990

U.S. Department of Commerce  
National Oceanic and Atmospheric Administration  
Environmental Data Service

TABLE 9-2

1989 AND 1990 CLIMATOLOGICAL DATA  
SIKORSKY INTERNATIONAL AIRPORT, STRATFORD

|      | AVERAGE TEMPERATURE °F |      | NO. OF DAYS WHEN MAX. TEMP. EXCEEDED 90 °F |      | DEGREE DAYS |      | PRECIPITATION IN EQUIVALENT INCHES OF WATER |       | NO. OF DAYS WITH MORE THAN 0.01 INCHES OF PRECIPITATION |      | AVERAGE WIND SPEED (MPH) |      |
|------|------------------------|------|--|------|-------------|------|---|-------|---|------|--------------------------|------|
|      | 1989                   | 1990 | 1989                                       | 1990 | 1989        | 1990 | 1989  | 1990  | 1989  | 1990 | 1989                     | 1990 |
| Jan  | 33.8                   | 36.7 | 0  | 0    | 958         | 869  | 1.44  | 4.01  | 9   | 11   | ---                      | ---  |
| Feb  | 31.0                   | 35.0 | 0  | 0    | 945         | 836  | 2.40  | 1.94  | 12  | 11   | ---                      | ---  |
| Mar  | 38.8                   | 40.1 | 0  | 0    | 804         | 766  | 4.06  | 2.10  | 10  | 8    | ---                      | ---  |
| Apr  | 47.9                   | 49.2 | 0  | 1    | 505         | 476  | 3.15  | 4.87  | 12  | 12   | ---                      | ---  |
| May  | 59.6                   | 56.9 | 0  | 0    | 180         | 243  | 9.53  | 6.89  | 13  | 15   | ---                      | ---  |
| Jun  | 68.5                   | 69.1 | 0  | 0    | 19          | 12   | 5.60  | 1.91  | 18  | 10   | ---                      | ---  |
| Jul  | 71.8                   | 73.9 | 0  | 2    | 0           | 5    | 3.44  | 2.83  | 9   | 8    | ---                      | ---  |
| Aug  | 71.6                   | 73.9 | 3  | 1    | 7           | 1    | 6.57  | 6.47  | 7   | 14   | ---                      | ---  |
| Sep  | 65.2                   | 65.6 | 0  | 0    | 88          | 77   | 3.21  | 1.75  | 7   | 8    | ---                      | ---  |
| Oct  | 54.9                   | 59.6 | 0  | 0    | 305         | 208  | 7.02  | 5.72  | 10  | 8    | ---                      | ---  |
| Nov  | 43.2                   | 46.6 | 0  | 0    | 648         | 546  | 3.27  | 1.89  | 13  | 9    | ---                      | ---  |
| Dec  | 23.3                   | 40.0 | 0  | 0    | 1285        | 771  | 0.83  | 3.53  | 9   | 13   | ---                      | ---  |
| YEAR | 50.8                   | 53.9 | 3  | 4    | 5744        | 4810 | 50.52                                       | 43.91 | 131   | 127  | ---                      | ---  |

\* Less than 0.05

a 1903-1990

b 1966-1990

c 1951-1980

d 1894-1990

e 1949-1990

f 1958-1980

Extracted From: Local Climatological Data Charts

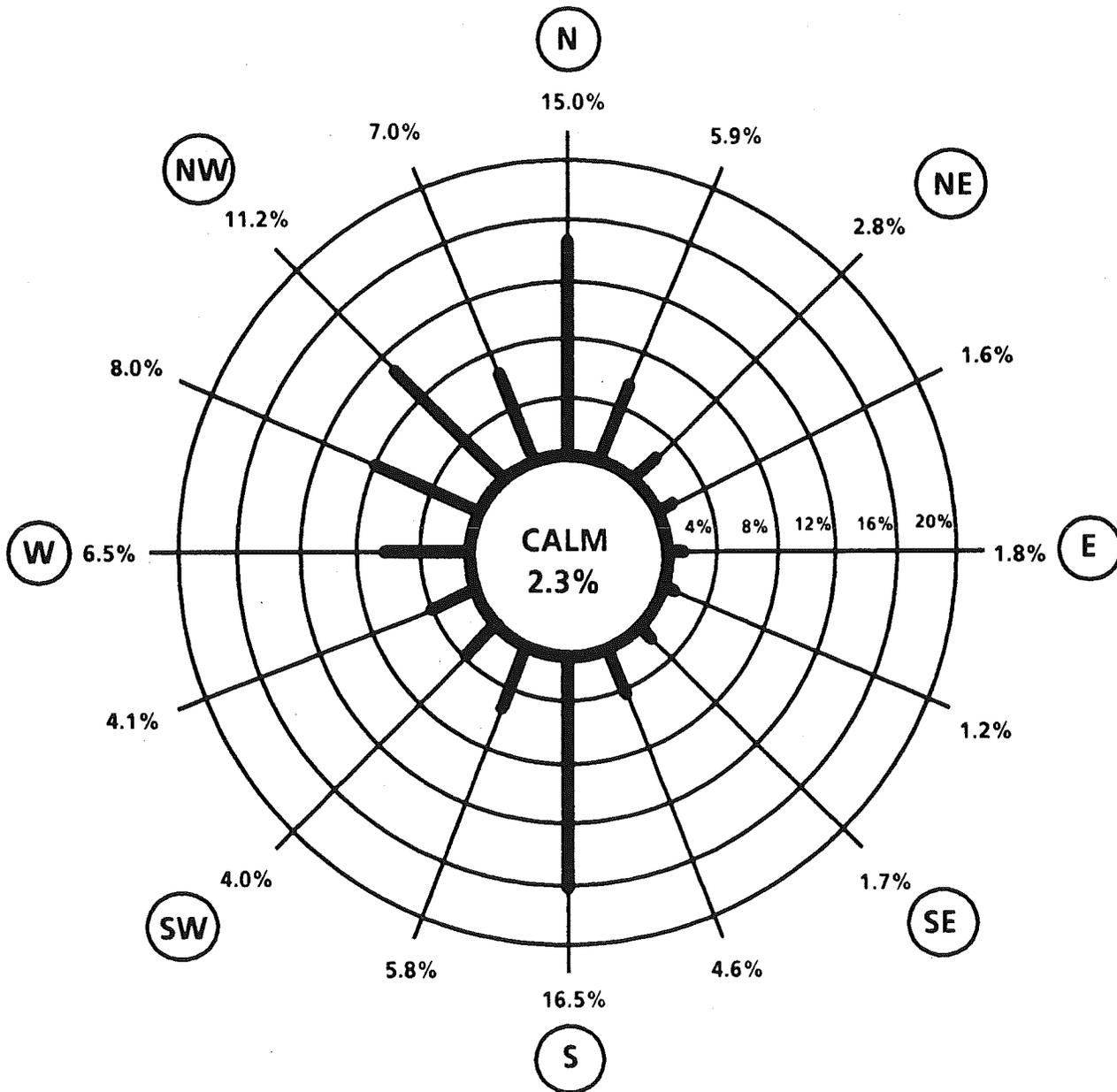
U.S. Department of Commerce

National Oceanic and Atmospheric Administration

Environmental Data Service

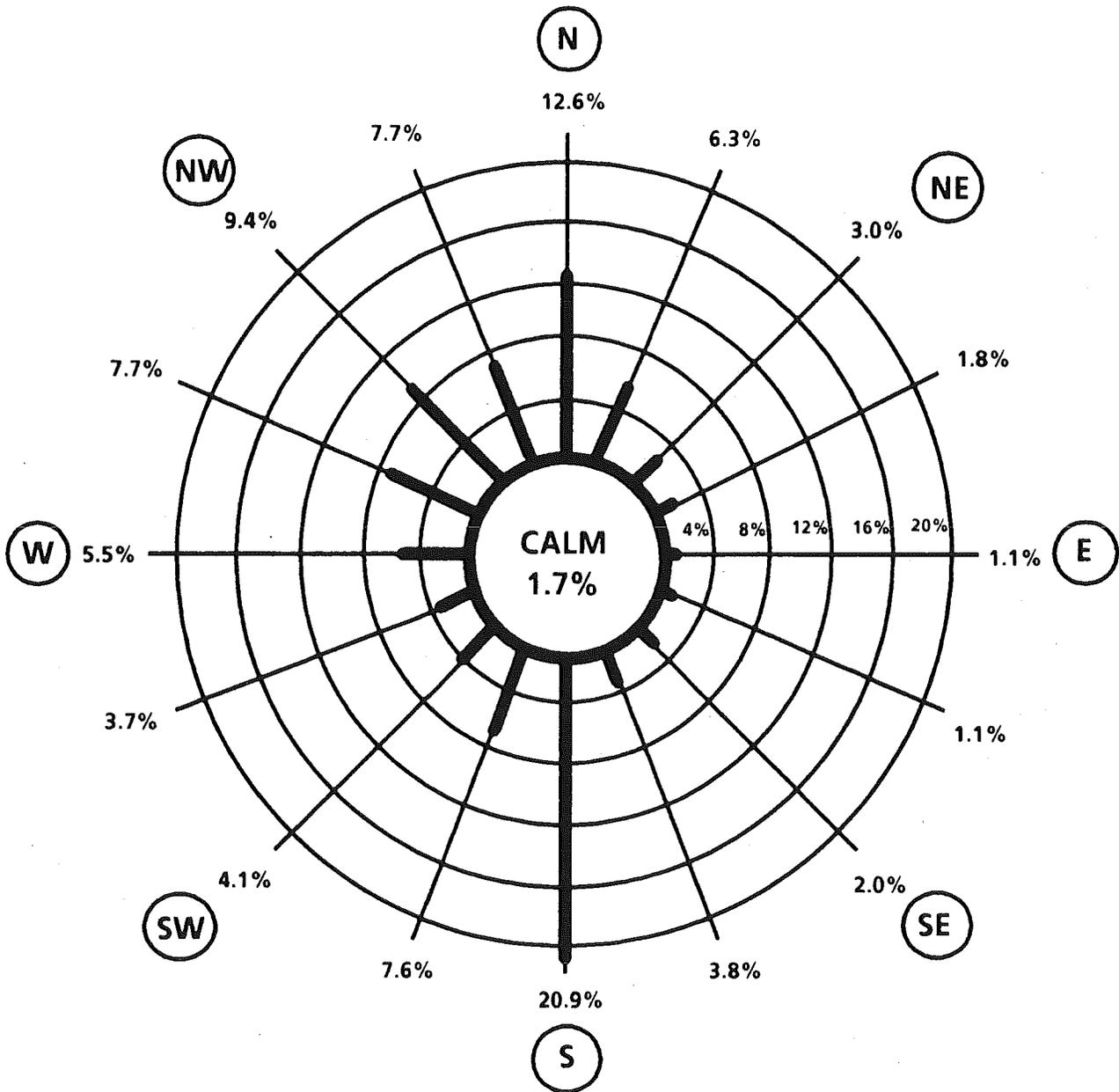
**FIGURE 9-1**

**ANNUAL WIND ROSE FOR 1989**  
**BRADLEY INTERNATIONAL AIRPORT**  
**WINDSOR LOCKS, CONNECTICUT**

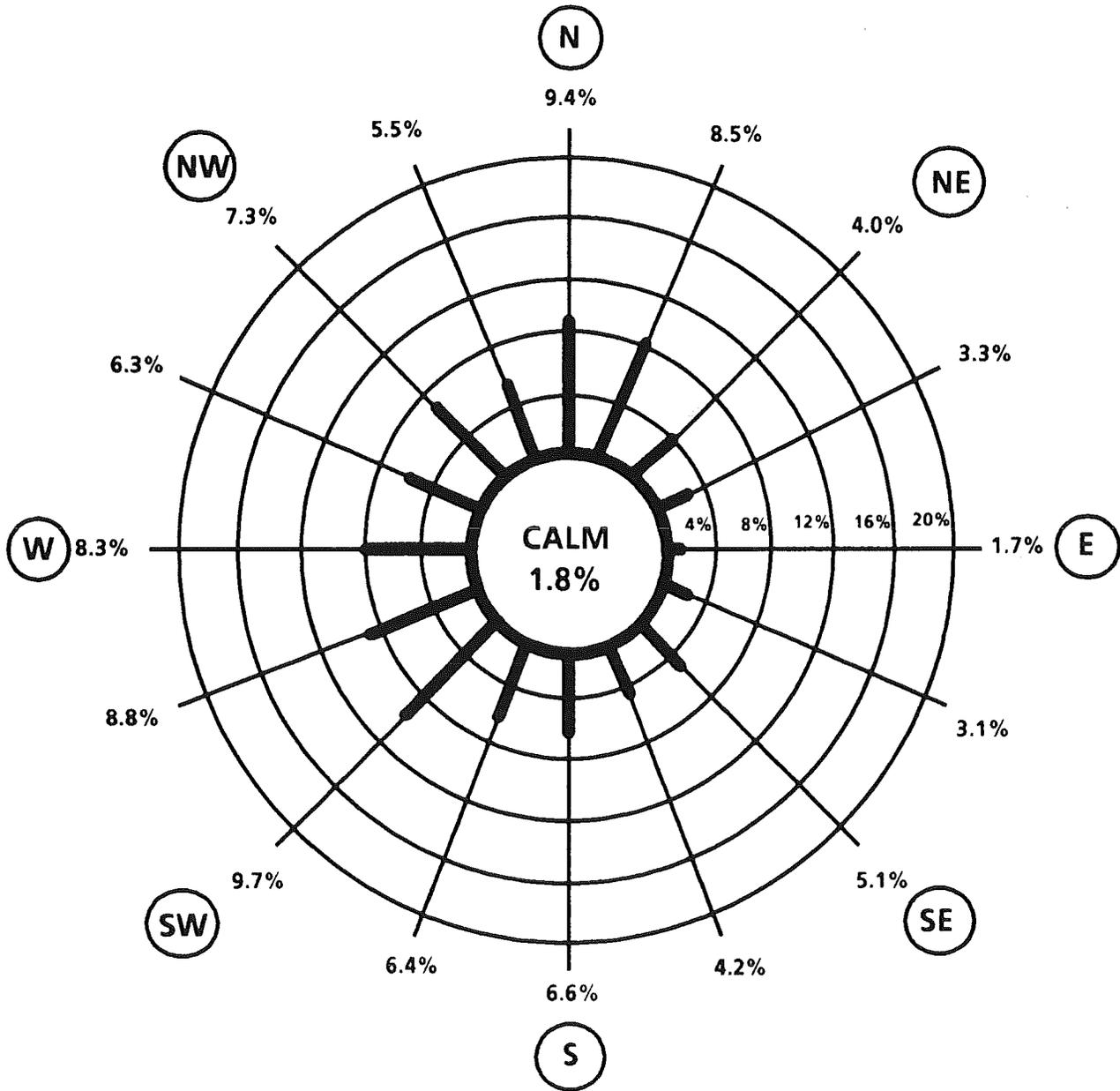


**FIGURE 9-2**

**ANNUAL WIND ROSE FOR 1990**  
**BRADLEY INTERNATIONAL AIRPORT**  
**WINDSOR LOCKS, CONNECTICUT**

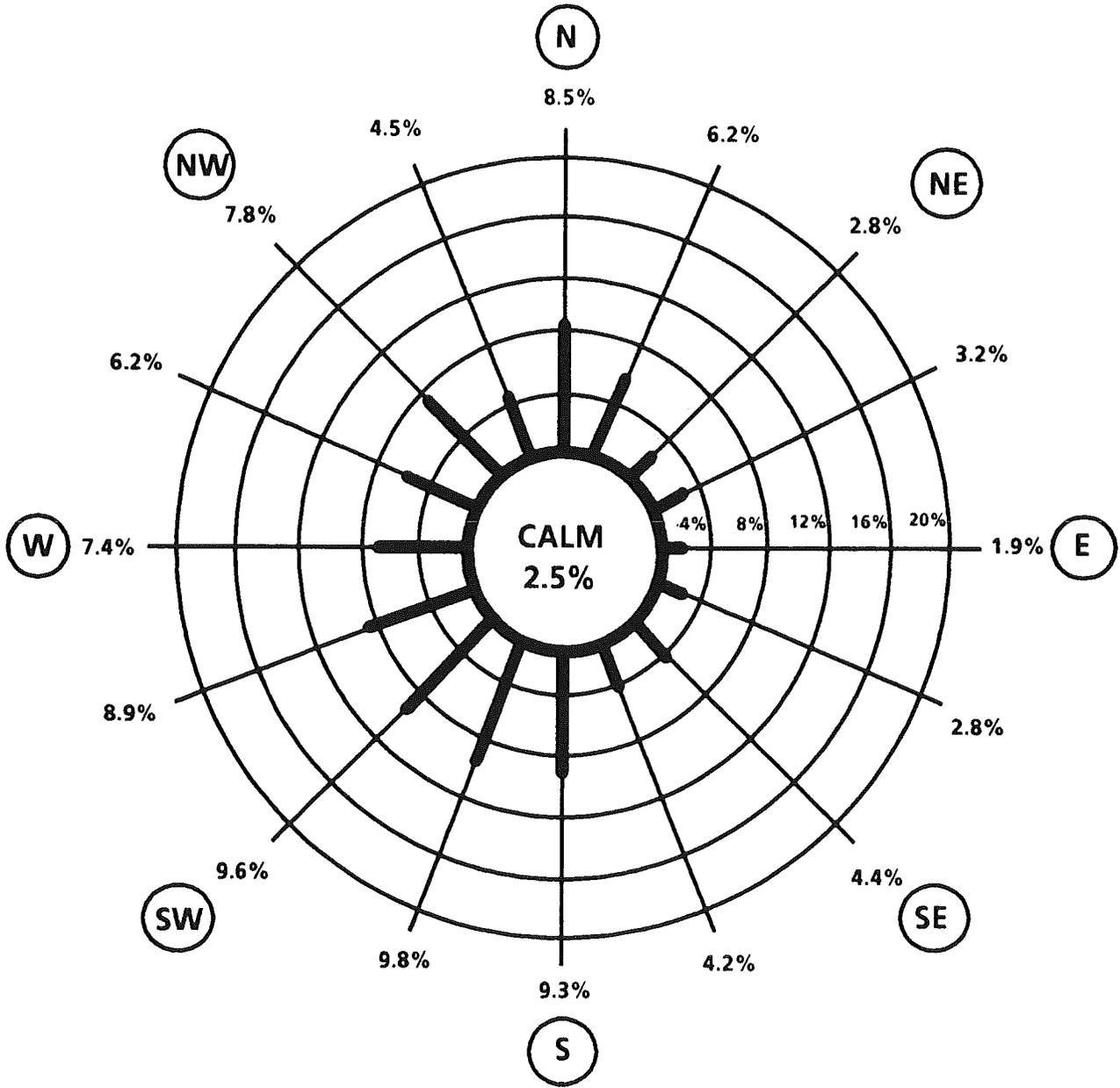


**FIGURE 9-3**  
**ANNUAL WIND ROSE FOR 1989**  
**NEWARK INTERNATIONAL AIRPORT**  
**NEWARK, NEW JERSEY**



**FIGURE 9-4**

**ANNUAL WIND ROSE FOR 1990**  
**NEWARK INTERNATIONAL AIRPORT**  
**NEWARK, NEW JERSEY**



## X. ATTAINMENT AND NON-ATTAINMENT OF NAAQS IN CONNECTICUT'S AQCR'S

The attainment status designations for Connecticut's four Air Quality Control Regions (AQCR's, see Figure 10-1) with regard to the National Ambient Air Quality Standards (NAAQS) have been determined for 1990 for the following pollutants: particulate matter no greater than 10 micrometers in diameter ( $PM_{10}$ ); sulfur dioxide ( $SO_2$ ); ozone ( $O_3$ ); nitrogen dioxide ( $NO_2$ ); carbon monoxide (CO); and lead (Pb). Table 10-1 shows the attainment status of each AQCR by pollutant. The AQCR's are classified as attainment, nonattainment or unclassifiable. These classifications conform to federal EPA guidelines and were applied in each case only after federal approval was granted. The federal EPA classifies an AQCR as attainment for a particular pollutant when all standards for the pollutant are attained (i.e., short term, long term, primary and secondary, wherever applicable). This notwithstanding, Table 10-1 contains the AQCR classifications with respect to each relevant short-term and long-term standard.

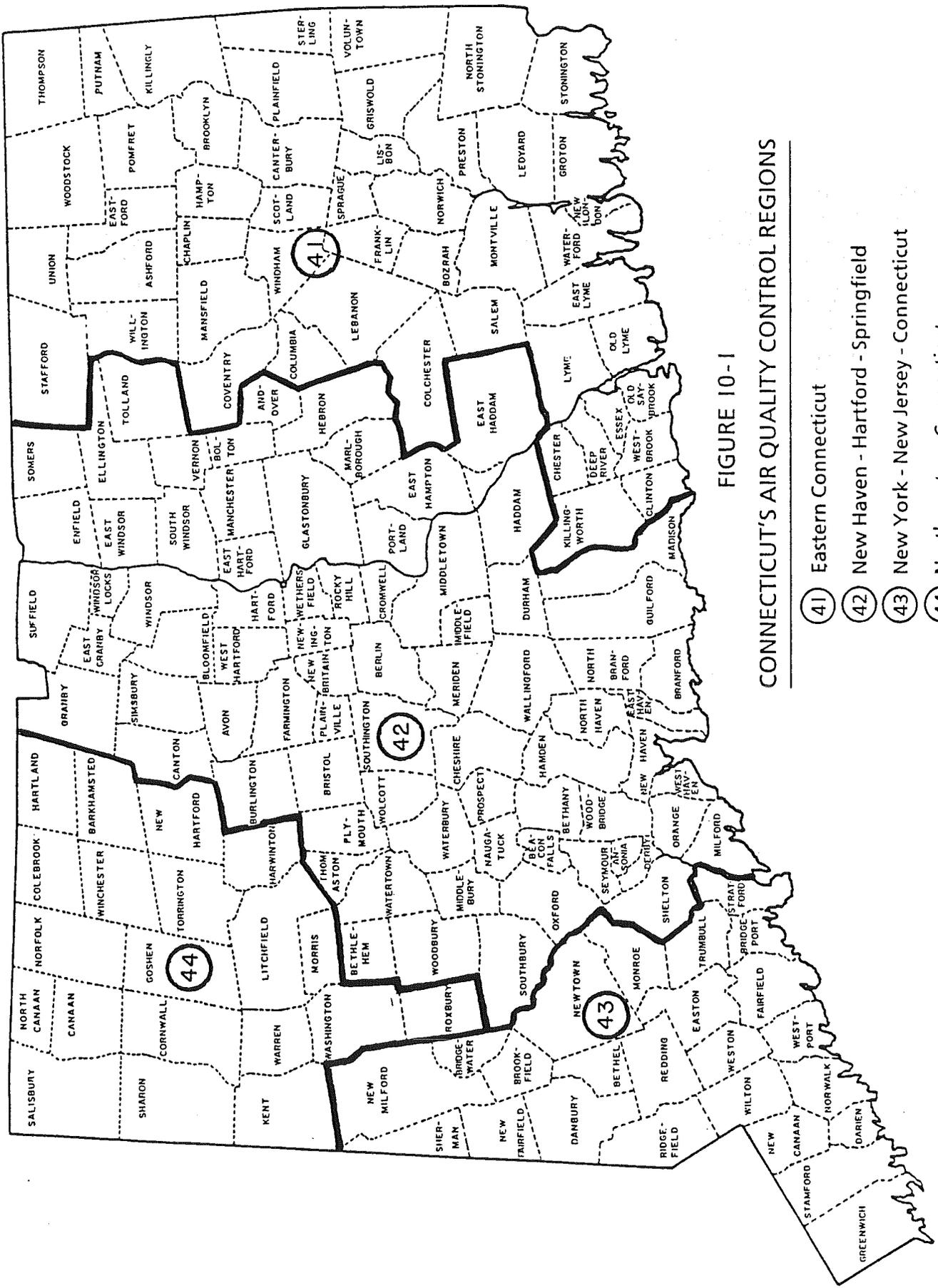


FIGURE 10-1  
CONNECTICUT'S AIR QUALITY CONTROL REGIONS

- ④1 Eastern Connecticut
- ④2 New Haven - Hartford - Springfield
- ④3 New York - New Jersey - Connecticut
- ④4 Northwestern Connecticut

## TABLE 10-1

### CONNECTICUT'S COMPLIANCE BY AQCR WITH THE NAAQS IN 1990

| <u>Pollutant</u> | <u>Primary<br/>or<br/>Secondary</u> | <u>NAAQS</u> | <u>AQCR<br/>41</u> | <u>AQCR<br/>42</u> | <u>AQCR<br/>43</u> | <u>AQCR<br/>44</u> |
|------------------|-------------------------------------|--------------|--------------------|--------------------|--------------------|--------------------|
| PM <sub>10</sub> | Both                                | Annual       | A                  | X                  | A                  | A                  |
|                  | Both                                | 24-Hour      | A                  | X                  | A                  | A                  |
| SO <sub>2</sub>  | Primary                             | Annual       | A                  | A                  | A                  | A                  |
|                  |                                     | 24-Hour      | A                  | A                  | A                  | A                  |
|                  | Secondary                           | 3-Hour       | A                  | A                  | A                  | A                  |
| Ozone            | Both                                | 1-Hour       | X                  | X                  | X                  | X                  |
| NO <sub>2</sub>  | Both                                | Annual       | A                  | A                  | A                  | A                  |
| CO               | Both                                | 1-Hour       | A                  | A                  | A                  | A                  |
|                  |                                     | 8-Hour       | U                  | X                  | X                  | U                  |
| Lead             | Both                                | 3-Month      | A                  | A                  | A                  | A                  |

X = Nonattainment

U = Unclassifiable

A = Attainment

## XI. CONNECTICUT SLAMS AND NAMS NETWORK

On May 10, 1979, the U.S. Environmental Protection Agency made public its final rulemaking for ambient air monitoring and data reporting requirements in the "Federal Register" (Vol. 44, No. 92). These regulations are meant to ensure the acceptability of air measurement data, the comparability of data from all monitoring stations, the cost-effectiveness of monitoring networks, and timely data submission for assessment purposes. The regulations address a number of key areas including quality assurance, monitoring methodologies, network design and probe siting. Detailed requirements and specific criteria are provided which form the framework for ambient air quality monitoring. These regulations apply to all parties conducting ambient air quality monitoring for the purpose of supporting or complying with environmental regulations. In particular, state/local control agencies and industrial/private concerns involved in air monitoring are directly influenced by specific requirements, compliance dates and recommended guidelines.

### QUALITY ASSURANCE

The regulations specify the minimum quality assurance requirements for State and Local Air Monitoring Stations (SLAMS) networks and National Air Monitoring Stations (NAMS) networks. Two distinct and equally important functions make up the quality assurance program: assessment of the quality of monitoring data by estimating their precision and accuracy, and control of the quality of the data by implementation of quality control policies, procedures, and corrective actions. (See Part D of Section I, Quality Assurance).

The data assessment requirements entail the determination of precision and accuracy for both continuous and manual methods. A one-point precision check must be carried out at least once every other week on each automated analyzer used to measure SO<sub>2</sub>, NO<sub>2</sub>, CO and O<sub>3</sub>. Standards from which the precision check test data are derived must meet specifications detailed in the regulations. For manual methods, precision checks are to be accomplished by operating co-located duplicate samplers. In 1990, Connecticut maintained two co-located PM<sub>10</sub> monitors (New Haven 123 and Waterbury 123) and one co-located lead monitor (New Haven 018).

Accuracy determinations for automated analyzers (SO<sub>2</sub>, NO<sub>2</sub>, CO, O<sub>3</sub>) are accomplished by audits performed by an independent auditor utilizing equipment and gases which are disassociated from the normal network operations. Accuracy determinations are accomplished via traceable standard flow devices for hi-vols and via spiked strip analyses for lead. For SLAMS analyzers, accuracy audits must be performed on each analyzer at least once per calendar year.

All precision and accuracy data are statistics derived through calculation methods specified by the regulations, with the data and results reported quarterly on personal computer floppy disks. The NAMS network is actually part of the SLAMS network; so the SLAMS accuracy determinations also apply to the NAMS network. The distinguishing characteristics of NAMS are: 1) the sites are located in high population, high pollution areas (i.e., urban areas); 2) only continuous instruments are used to monitor gaseous pollutants; 3) the regulations specify a minimum number and locations for them; and 4) the data, in addition to being included in the annual report, are required to be reported quarterly to EPA.

In order to control the quality of data, the monitoring program must have operational procedures for each of the following activities:

1. Selection of methods, analyzers, and samplers,
2. Site selection and probe siting,

3. Equipment purchase, check-out and installation,
4. Instrument calibration,
5. Control checks and their frequency,
6. Control limits for control checks, and corrective actions when such limits are exceeded,
7. Preventive and remedial maintenance,
8. Documentation of quality control information, and
9. Data recording, reduction, validation and reporting.

### **MONITORING METHODOLOGIES**

Except as otherwise stated within the regulations, the monitoring methods used must be "reference" or "equivalent," as designated by the EPA. Table 11-1 lists methods used in Connecticut's network in 1990 which were on the EPA-approved list as of December 12, 1989. Additional updates to these approved methods are provided through the "Federal Register."

### **NETWORK DESIGN**

The regulations also describe monitoring objectives and general criteria to be applied in establishing the SLAMS and NAMS networks and for choosing general locations for new monitors. Criteria are also presented for determining the location and number of monitors. Since January 1, 1984, these criteria have served as the framework for all State Implementation Plan (SIP) monitoring networks.

The SLAMS and NAMS networks are designed to meet four basic monitoring objectives: (1) to determine the highest pollutant concentration in the area; (2) to determine representative concentrations in areas of high population density; (3) to determine the ambient impact of significant sources or source categories; and (4) to determine general background concentration levels. Proper siting of a monitor requires precise specification of the monitoring objectives, which usually includes a desired spatial scale of representativeness. The spatial scales of representativeness are specified in the regulations for all pollutants and monitoring objectives. The 1990 SLAMS and NAMS networks in Connecticut are presented and described in Table 11-2.

### **PROBE SITING**

Location and exposure of monitoring probes are described in Title 40 of the Code of Federal Regulations, Part 58, Appendix E. The probe siting criteria promulgated in the regulations are specific. They are also sufficiently comprehensive to define the requirements for ensuring the uniform collection of compatible and comparable air quality data.

These criteria are detailed by pollutant and include vertical and horizontal probe placement, spacing from obstructions and trees, spacing from roadways, probe material and sample residence time, and various other considerations. A summary of the probe siting criteria is presented in Table 11-3. The siting criteria generally apply to all spatial scales except where noted. The most notable exception is spacing from roadways which is dependent on traffic volume.

For the chemically reactive gases SO<sub>2</sub>, NO<sub>2</sub>, and O<sub>3</sub>, the regulations specify borosilicate glass, FEP teflon or their equivalent as the only acceptable sample train materials. Additionally, in order to minimize the effects of particulate deposition on probe walls, sample trains for reactive gases must have residence times of less than 20 seconds.

**TABLE 11-1**

U. S. EPA-APPROVED MONITORING METHODS USED IN CONNECTICUT IN 1990

| <u>Pollutant</u> | <u>Monitoring Methods</u>                    |                              |                          |
|------------------|--|------------------------------|--------------------------|
|                  | Reference Manual                             | Reference Automated          | Equivalent Automated     |
| PM <sub>10</sub> | Wedding & Associates<br>Critical Flow Hi-vol |                              |                          |
| SO <sub>2</sub>  |  |                              | Thermo Electron 43 (0.5) |
| O <sub>3</sub>   |  |                              | DASIBI 1008-RS (0.5)     |
| CO               |  | Thermo Electron 48 (50)      |                          |
| NO <sub>2</sub>  |  | Thermo Electron 14 B/E (0.5) |                          |
| Lead             | High Volume Method<br>Low Volume Method*     |                              |                          |

\* This is a modified reference method approved by EPA on 2/29/84.

( ) = Approved range in ppm

**TABLE 11-2**  
**1990 SLAMS AND NAMS SITES IN CONNECTICUT**

| <u>Town</u>  | <u>Urban Area</u>      | <u>Site</u> | <u>SLAMS<br/>or<br/>NAMS</u> | <u>Sampling<br/>Method</u> | <u>Analytic<br/>Method</u> | <u>Operating<br/>Schedule</u> | <u>Monitoring Objective</u> | <u>Spatial Scale of<br/>Representativeness</u> |
|--|------------------------|-------------|------------------------------|----------------------------|----------------------------|-------------------------------|-----------------------------|--|
| <b><u>PARTICULATE MATTER (PM<sub>10</sub>)</u></b> |                        |             |                              |                            |                            |                               |                             |  |
| Ansonia  | Bridgeport             | 004         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | Population                  | Urban  |
| Berlin   | New Britain            | 002         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | Population                  | Neighborhood                                   |
| Bridgeport   | Bridgeport             | 010         | N                            | Hi-Vol                     | Gravimetric                | 6th day                       | Population                  | Neighborhood                                   |
| Bridgeport   | Bridgeport             | 013         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | Population                  | Neighborhood                                   |
| Bridgeport   | Bridgeport             | 014         | N                            | Hi-Vol                     | Gravimetric                | 6th day                       | High Concentration          | Micro  |
| Bristol  | Bristol                | 001         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | High Concentration          | Neighborhood                                   |
| Burlington   | NONE                   | 001         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | Background                  | Regional                                       |
| Cornwall   | NONE                   | 005         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | Background                  | Regional                                       |
| Danbury  | Danbury                | 123         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | Population                  | Neighborhood                                   |
| Darien   | Stamford               | 001         | N                            | Hi-Vol                     | Gravimetric                | 6th day                       | High Concentration          | Micro  |
| E. Hartford  | Hartford               | 004         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | High Concentration          | Neighborhood                                   |
| Enfield  | MA-CT*                 | 005         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | Population                  | Regional                                       |
| Greenwich  | Stamford               | 017         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | Population                  | Neighborhood                                   |
| Groton   | New London/<br>Norwich | 006         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | High Concentration          | Neighborhood                                   |
| Haddam   | NONE                   | 002         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | Population                  | Regional                                       |
| Hartford   | Hartford               | 013         | N                            | Hi-Vol                     | Gravimetric                | 6th day                       | Population                  | Neighborhood                                   |
| Hartford   | Hartford               | 014         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | Population                  | Neighborhood                                   |
| Hartford   | Hartford               | 015         | N                            | Hi-Vol                     | Gravimetric                | 6th day                       | High Concentration          | Micro  |
| Hartford   | Hartford               | 018         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | Population                  | Micro  |
| Manchester   | Hartford               | 001         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | High Concentration          | Neighborhood                                   |
| Meriden  | Meriden                | 002         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | High Concentration          | Neighborhood                                   |

\* Includes Springfield, Chicheopee, Holyoke in MA; East Windsor, Enfield, Suffield, Windsor Locks in CT.

**TABLE 11-2, CONTINUED**  
**1990 SLAMS AND NAMS SITES IN CONNECTICUT**

| <u>Town</u>                                 | <u>Urban Area</u>      | <u>Site</u> | <u>SLAMS<br/>or<br/>NAMS</u> | <u>Sampling<br/>Method</u> | <u>Analytic<br/>Method</u> | <u>Operating<br/>Schedule</u> | <u>Monitoring Objective</u> | <u>Spatial Scale of<br/>Representativeness</u> |
|---|------------------------|-------------|------------------------------|----------------------------|----------------------------|-------------------------------|-----------------------------|--|
| <b>PARTICULATE MATTER (PM<sub>10</sub>)</b> |                        |             |                              |                            |                            |                               |                             |  |
| Middletown                                  | Hartford               | 003         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | High Concentration          | Neighborhood                                   |
| Milford                                     | Bridgeport             | 010         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | Population                  | Neighborhood                                   |
| Naugatuck                                   | Waterbury              | 001         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | High Concentration          | Neighborhood                                   |
| New Britain                                 | New Britain            | 012         | N                            | Hi-Vol                     | Gravimetric                | 6th day                       | High Concentration          | Middle   |
| New Haven                                   | New Haven              | 013         | N                            | Hi-Vol                     | Gravimetric                | 6th day                       | Population                  | Neighborhood                                   |
| New Haven                                   | New Haven              | 018         | N                            | Hi-Vol                     | Gravimetric                | 6th day                       | High Concentration          | Middle   |
| New Haven                                   | New Haven              | 020         | N                            | Hi-Vol                     | Gravimetric                | 6th day                       | High Concentration          | Middle   |
| New Haven                                   | New Haven              | 123         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | Population                  | Neighborhood                                   |
| New London                                  | New London/<br>Norwich | 004         | N                            | Hi-Vol                     | Gravimetric                | 6th day                       | High Concentration          | Middle   |
| Norwalk                                     | Norwalk                | 014         | N                            | Hi-Vol                     | Gravimetric                | 6th day                       | High Concentration          | Micro  |
| Norwich                                     | New London/<br>Norwich | 002         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | Population                  | Neighborhood                                   |
| Putnam                                      | NONE                   | 002         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | Population                  | Neighborhood                                   |
| Stamford                                    | Stamford               | 001         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | High Concentration          | Neighborhood                                   |
| Stratford                                   | Bridgeport             | 005         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | High Concentration          | Neighborhood                                   |
| Torrington                                  | NONE                   | 001         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | Population                  | Neighborhood                                   |
| Voluntown                                   | NONE                   | 001         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | Background                  | Regional                                       |
| Wallingford                                 | New Haven              | 006         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | Population                  | Neighborhood                                   |
| Waterbury                                   | Waterbury              | 007         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | Population                  | Neighborhood                                   |
| Waterbury                                   | Waterbury              | 123         | N                            | Hi-Vol                     | Gravimetric                | 6th day                       | High Concentration          | Middle   |
| Waterford                                   | New London/<br>Norwich | 001         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | Population                  | Neighborhood                                   |
| West Haven                                  | New Haven              | 003         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | High Concentration          | Middle   |
| Willimantic                                 | NONE                   | 002         | S                            | Hi-Vol                     | Gravimetric                | 6th day                       | High Concentration          | Neighborhood                                   |

**TABLE 11-2, CONTINUED**  
**1990 SLAMS AND NAMS SITES IN CONNECTICUT**

| <u>Town</u>                  | <u>Urban Area</u>      | <u>Site</u> | <u>SLAMS<br/>or<br/>NAMS</u> | <u>Sampling &amp; Analytic<br/>Method</u> | <u>Operating<br/>Schedule</u> | <u>Monitoring Objective</u> | <u>Spatial Scale of<br/>Representativeness</u> |
|------------------------------|------------------------|-------------|------------------------------|---|-------------------------------|-----------------------------|--|
| <b><u>SULFUR DIOXIDE</u></b> |                        |             |                              |   |                               |                             |  |
| Bridgeport                   | Bridgeport             | 012         | S                            | Pulsed Fluorescence                       | Continuous                    | High Concentration          | Neighborhood                                   |
| Bridgeport                   | Bridgeport             | 013         | N                            | Pulsed Fluorescence                       | Continuous                    | High Concentration          | Neighborhood                                   |
| Danbury                      | Danbury                | 123         | S                            | Pulsed Fluorescence                       | Continuous                    | Population                  | Neighborhood                                   |
| E. Hartford                  | Hartford               | 006         | N                            | Pulsed Fluorescence                       | Continuous                    | High Concentration          | Neighborhood                                   |
| East Haven                   | New Haven              | 003         | S                            | Pulsed Fluorescence                       | Continuous                    | Population                  | Neighborhood                                   |
| Enfield                      | MA - CT*               | 005         | S                            | Pulsed Fluorescence                       | Continuous                    | Background                  | Regional                                       |
| Greenwich                    | Stamford               | 017         | S                            | Pulsed Fluorescence                       | Continuous                    | Background                  | Urban  |
| Groton                       | New London/<br>Norwich | 007         | S                            | Pulsed Fluorescence                       | Continuous                    | Population                  | Neighborhood                                   |
| Hartford                     | Hartford               | 018         | N                            | Pulsed Fluorescence                       | Continuous                    | Population                  | Neighborhood                                   |
| Milford                      | Bridgeport             | 010         | S                            | Pulsed Fluorescence                       | Continuous                    | High Concentration          | Neighborhood                                   |
| New Britain                  | New Britain            | 011         | S                            | Pulsed Fluorescence                       | Continuous                    | High Concentration          | Neighborhood                                   |
| New Haven                    | New Haven              | 123         | N                            | Pulsed Fluorescence                       | Continuous                    | High Concentration          | Neighborhood                                   |
| Stamford                     | Stamford               | 025         | S                            | Pulsed Fluorescence                       | Continuous                    | Population                  | Neighborhood                                   |
| Stamford                     | Stamford               | 123         | S                            | Pulsed Fluorescence                       | Continuous                    | High Concentration          | Neighborhood                                   |
| Waterbury                    | Waterbury              | 008         | S                            | Pulsed Fluorescence                       | Continuous                    | High Concentration          | Neighborhood                                   |
| Waterbury                    | Waterbury              | 123         | S                            | Pulsed Fluorescence                       | Continuous                    | Population                  | Neighborhood                                   |

\* Includes Springfield, Chicopee, Holyoke in MA; East Windsor, Enfield, Suffield, Windsor Locks in CT.

**TABLE 11-2, CONTINUED**  
**1990 SLAMS AND NAMS SITES IN CONNECTICUT**

| <u>Town</u>                   | <u>Urban Area</u>      | <u>Site</u> | <u>SLAMS<br/>or<br/>NAMS</u> | <u>Sampling &amp; Analytic<br/>Method</u> | <u>Operating<br/>Schedule</u> | <u>Monitoring Objective</u> | <u>Spatial Scale of<br/>Representativeness</u> |
|-------------------------------|------------------------|-------------|------------------------------|---|-------------------------------|-----------------------------|--|
| <b><u>NITROGEN OXIDES</u></b> |                        |             |                              |   |                               |                             |  |
| Bridgeport                    | Bridgeport             | 013         | S                            | Chemiluminescent                          | Continuous                    | High Concentration          | Neighborhood                                   |
| E. Hartford                   | Hartford               | 003         | S                            | Chemiluminescent                          | Continuous                    | High Concentration          | Neighborhood                                   |
| New Haven                     | New Haven              | 123         | S                            | Chemiluminescent                          | Continuous                    | High Concentration          | Neighborhood                                   |
| <b><u>OZONE</u></b>           |                        |             |                              |   |                               |                             |  |
| Bridgeport                    | Bridgeport             | 013         | N                            | Chemiluminescent                          | Continuous                    | Population                  | Neighborhood                                   |
| Danbury                       | Danbury                | 123         | S                            | Chemiluminescent                          | Continuous                    | High Concentration          | Urban  |
| E. Hartford                   | Hartford               | 003         | N                            | Chemiluminescent                          | Continuous                    | Population                  | Neighborhood                                   |
| Greenwich                     | Stamford               | 017         | S                            | Chemiluminescent                          | Continuous                    | High Concentration          | Urban  |
| Groton                        | New London/<br>Norwich | 008         | S                            | Chemiluminescent                          | Continuous                    | High Concentration          | Urban  |
| Madison                       | NONE                   | 002         | S                            | Chemiluminescent                          | Continuous                    | High Concentration          | Urban  |
| Middletown                    | Hartford               | 007         | N                            | Chemiluminescent                          | Continuous                    | High Concentration          | Urban  |
| New Haven                     | New Haven              | 123         | N                            | Chemiluminescent                          | Continuous                    | Population                  | Neighborhood                                   |
| Stafford                      | NONE                   | 001         | N                            | Chemiluminescent                          | Continuous                    | High Concentration          | Urban  |
| Stratford                     | Bridgeport             | 007         | N                            | Chemiluminescent                          | Continuous                    | High Concentration          | Urban  |
| <b><u>CARBON MONOXIDE</u></b> |                        |             |                              |   |                               |                             |  |
| Bridgeport                    | Bridgeport             | 004         | S                            | NDIR                                      | Continuous                    | High Concentration          | Micro  |
| Hartford                      | Hartford               | 013         | N                            | NDIR                                      | Continuous                    | Population                  | Neighborhood                                   |
| Hartford                      | Hartford               | 017         | N                            | NDIR                                      | Continuous                    | High Concentration          | Micro  |
| New Haven                     | New Haven              | 019         | S                            | NDIR                                      | Continuous                    | High Concentration          | Micro  |
| Stamford                      | Stamford               | 020         | S                            | NDIR                                      | Continuous                    | High Concentration          | Micro  |

**TABLE 11-2, CONTINUED**  
**1990 SLAMS AND NAMS SITES IN CONNECTICUT**

| <u>Town</u> | <u>Urban Area</u> | <u>Site</u> | <u>SLAMS<br/>or<br/>NAMS</u> | <u>Sampling<br/>Method</u> | <u>Analytic<br/>Method</u> | <u>Operating<br/>Schedule</u> | <u>Monitoring Objective</u> | <u>Spatial Scale of<br/>Representativeness</u> |
|-------------|-------------------|-------------|------------------------------|----------------------------|----------------------------|-------------------------------|-----------------------------|--|
|             |                   |             |                              |                            | <u>LEAD</u>                |                               |                             |  |
| Bridgeport  | Bridgeport        | 010         | S                            | Lo-Vol                     | Atomic Abs.                | 1 month                       | High Concentration          | Middle   |
| E. Hartford | Hartford          | 004         | N                            | Lo-Vol                     | Atomic Abs.                | 1 month                       | Population                  | Neighborhood                                   |
| Hartford    | Hartford          | 016         | N                            | Lo-Vol                     | Atomic Abs.                | 1 month                       | High Concentration          | Micro  |
| New Haven   | New Haven         | 018         | S                            | Lo-Vol                     | Atomic Abs.                | 1 month                       | High Concentration          | Middle   |
| Waterbury   | Waterbury         | 123         | S                            | Lo-Vol                     | Atomic Abs.                | 1 month                       | High Concentration          | Middle   |

**TABLE 11-3**

**SUMMARY OF PROBE SITING CRITERIA**

| Pollutant        | Spatial Scale                            | Distance from Supporting Structure (meters) |                         | Height Above Ground (meters) | Other Spacing Criteria   |
|------------------|--|---|-------------------------|------------------------------|--|
|                  |  | Vertical                                    | Horizontal <sup>a</sup> |                              |  |
| PM <sub>10</sub> | Micro                                    |   | > 2                     | 2 - 7                        | <ol style="list-style-type: none"> <li>1. The sampler should be &gt; 20 meters from the dripline and must be 10 meters from the dripline when any tree acts as an obstruction.</li> <li>2. The distance from the sampler to an obstacle, such as a building, must be at least twice the height the obstacle protrudes above the sampler, except for street canyon sites.<sup>b</sup></li> <li>3. There must be unrestricted air flow 270 degrees around the sampler, except for street canyon sites.</li> <li>4. No furnace or incineration flues should be nearby.<sup>c</sup></li> <li>5. The spacing from roads varies with traffic<sup>d</sup>, except for street canyon sites which must be from 2 to 10 meters from the edge of the nearest traffic lane.</li> </ol> |
|                  | Middle, neighborhood, urban and regional |   | > 2                     | 2 - 15                       | <ol style="list-style-type: none"> <li>1. The sampler should be &gt; 20 meters from the dripline and must be 10 meters from the dripline when any tree acts as an obstruction.</li> <li>2. The distance from the sampler to an obstacle, such as a building, must be at least twice the height the obstacle protrudes above the sampler.<sup>b</sup></li> <li>3. There must be unrestricted air flow 270 degrees around the sampler.</li> <li>4. No furnace or incineration flues should be nearby.<sup>c</sup></li> <li>5. The spacing from roads varies with traffic.<sup>d</sup></li> </ol>   |

# TABLE 11-3, CONTINUED

## SUMMARY OF PROBE SITING CRITERIA

| Pollutant | Spatial Scale                            | Distance from Supporting Structure (meters) |                         | Height Above Ground (meters) | Other Spacing Criteria  |
|-----------|--|---|-------------------------|------------------------------|---|
|           |  | Vertical                                    | Horizontal <sup>a</sup> |                              |   |
| Pb        | Micro                                    |   | >2                      | 2 - 7                        | <ol style="list-style-type: none"> <li>1. The sampler should be &gt; 20 meters from the dripline and must be 10 meters from the dripline when any tree acts as an obstruction.</li> <li>2. The distance from the sampler to an obstacle, such as a building, must be at least twice the height the obstacle protrudes above the sampler.<sup>b</sup></li> <li>3. There must be unrestricted air flow 270 degrees around the sampler, except for street canyon sites.<sup>c</sup></li> <li>4. No furnace or incineration flues should be nearby.<sup>c</sup></li> <li>5. The sampler must be 5 to 15 meters from a major roadway.</li> </ol> |
|           | Middle, neighborhood, urban and regional |   | >2                      | 2 - 15                       | <ol style="list-style-type: none"> <li>1. The sampler should be &gt; 20 meters from the dripline and must be 10 meters from the dripline when any tree acts as an obstruction.</li> <li>2. The distance from the sampler to an obstacle, such as a building, must be at least twice the height the obstacle protrudes above the sampler.<sup>b</sup></li> <li>3. There must be unrestricted air flow 270 degrees around the sampler.</li> <li>4. No furnace or incineration flues should be nearby.<sup>c</sup></li> <li>5. The spacing from roads varies with traffic.<sup>d</sup></li> </ol>  |

**TABLE 11-3, CONTINUED**  
**SUMMARY OF PROBE SITING CRITERIA**

| Pollutant       | Spatial Scale | Distance from Supporting Structure (meters) |                         | Height Above Ground (meters) | Other Spacing Criteria  |
|-----------------|---------------|---|-------------------------|------------------------------|---|
|                 |               | Vertical                                    | Horizontal <sup>a</sup> |                              |   |
| SO <sub>2</sub> | All           | 3 - 15                                      | > 1                     | > 1                          | <ol style="list-style-type: none"> <li>1. The probe should be &gt; 20 meters from the dripline and must be 10 from the dripline when a tree acts as an obstruction.</li> <li>2. The distance from the inlet probe to an obstacle, such as a building, must be at least twice the height the obstacle protrudes above the inlet probe.<sup>b</sup></li> <li>3. There must be unrestricted air flow 270 degrees around the inlet probe, or 180 degrees if the probe is on the side of a building.</li> <li>4. No furnace or incineration flues should be nearby.<sup>c</sup></li> </ol> |
| O <sub>3</sub>  | All           | > 1   | > 1                     | 3 - 15                       | <ol style="list-style-type: none"> <li>1. The probe should be &gt; 20 meters from the dripline and must be 10 from the dripline when a tree acts as an obstruction.</li> <li>2. The distance from the inlet probe to an obstacle, such as a building, must be at least twice the height the obstacle protrudes above the inlet probe.</li> <li>3. There must be unrestricted air flow 270 degrees around the inlet probe, or 180 degrees if the probe is on the side of a building.</li> <li>4. The spacing from roads varies with traffic.<sup>d</sup></li> </ol>                    |

# TABLE 11-3, CONTINUED

## SUMMARY OF PROBE SITING CRITERIA

| Pollutant       | Spatial Scale       | Distance from Supporting Structure (meters) |                         | Height Above Ground (meters) | Other Spacing Criteria   |
|-----------------|---------------------|---|-------------------------|------------------------------|--|
|                 |                     | Vertical                                    | Horizontal <sup>a</sup> |                              |  |
| CO              | Micro               | 3 + or - 1/2                                | > 1                     | > 1                          | <ol style="list-style-type: none"> <li>The probe must be &gt; 10 meters from the street intersection and should be at a midblock location.</li> <li>The probe must be 2 to 10 meters from the edge of the nearest traffic lane.</li> <li>There must be unrestricted airflow 180 degrees around the inlet probe.</li> </ol>   |
|                 | Middle neighborhood | 3 - 15                                      | > 1                     | > 1                          | <ol style="list-style-type: none"> <li>There must be unrestricted airflow 270 degrees around the inlet probe, or 180 degrees if the probe is on the side of a building.</li> <li>The spacing from roads varies with traffic.<sup>d</sup></li> </ol>  |
| NO <sub>2</sub> | All                 | 3 - 15                                      | > 1                     | > 1                          | <ol style="list-style-type: none"> <li>The probe should be &gt; 20 meters from the dripline and must be 10 from the dripline when a tree acts as an obstruction.</li> <li>The distance from the inlet probe to an obstacle, such as a building, must be at least twice the height the obstacle protrudes above the inlet probe.<sup>b</sup></li> <li>There must be unrestricted air flow 270 degrees around the inlet probe, or 180 degrees if the probe is on the side of a building.</li> <li>The spacing from roads varies with traffic.<sup>d</sup></li> </ol> |

<sup>a</sup> When the probe is located on a rooftop, this separation distance is in reference to walls, parapets, or penthouses located on the roof.

<sup>b</sup> Sites not meeting this criterion would be classified as middle scale.

<sup>c</sup> Distance is dependent upon height of furnace or incineration flue, type of fuel or waste burned, and quality of fuel (sulfur and ash content). This is to avoid undue influences from minor pollutant sources.

<sup>d</sup> Distance is dependent upon traffic ADT, pollutant, and spatial scale.

## XII. PUBLICATIONS

The following is a partial listing of technical papers and study reports dealing with various aspects of Connecticut air pollutant levels and air quality data.

1. Bruckman, L., *Asbestos: An Evaluation of Its Environmental Impact in Connecticut*, internal report issued by the Connecticut Department of Environmental Protection, Hartford, Connecticut, March 12, 1976.
2. Lepow, M. L., L. Bruckman, R.A. Rubino, S. Markowitz, M. Gillette and J. Kapish, *"Role of Airborne Lead in Increased Body Burden of Lead in Hartford Children,"* Environ. Health Perspect., May, 1974, pp. 99-102.
3. Bruckman, L. and R.A. Rubino, *"Rationale Behind a Proposed Asbestos Air Quality Standard,"* paper presented at the 67th Annual Meeting of the Air Pollution Control Association, Denver, Colorado, June 9-11, 1974, J. Air Pollut. Cntr. Assoc., 25: 1207-15 (1975).
4. Rubino, R.A., L. Bruckman and J. Magyar, *"Ozone Transport,"* paper presented at the 68th Annual Meeting of the Air Pollution Control Association, Boston, Massachusetts, June 15-20, 1975, J. Air Pollut. Cntr. Assoc.: 26, 972-5 (1976).
5. Bruckman, L., R.A. Rubino and T. Helfgott, *"Rationale Behind a Proposed Cadmium Air Quality Standard,"* paper presented at the 68th Annual Meeting of the Air Pollution Control Association, Boston, Massachusetts, June 15-20, 1975.
6. Rubino, R.A., L. Bruckman, A. Kramar, W. Keever and P. Sullivan, *"Population Density and Its Relationship to Airborne Pollutant Concentrations and Lung Cancer Incidence in Connecticut,"* paper presented at the 68th Annual Meeting of the Air Pollution Control Association, Boston, Massachusetts, June 15-20, 1975.
7. Lepow, M.L., L. Bruckman, M. Gillette, R.A. Rubino and J. Kapish, *"Investigations into Sources of Lead in the Environment of Urban Children,"* Environ. Res., 10: 415-26 (1975).
8. Bruckman, L., E. Hyne and P. Norton, *"A Low Volume Particulate Ambient Air Sampler,"* paper presented at the APCA Specialty Conference entitled "Measurement Accuracy as it Relates to Regulation Compliance," New Orleans, Louisiana, October 26-28, 1975, APCA publication SP-16, Air Pollution Control Association, Pittsburgh, Pennsylvania, 1976.
9. Bruckman, L. and R.A. Rubino, *"High Volume Sampling Errors Incurred During Passive Sample Exposure Periods,"* J. Air Pollut. Cntr. Assoc., 26: 881-3 (1976).
10. Bruckman, L., R.A. Rubino and B. Christine, *"Asbestos and Mesothelioma Incidence in Connecticut,"* J. Air Pollut. Cntr. Assoc., 27: 121-6 (1977).
11. Bruckman, L., *Suspended Particulate Transport in Connecticut: An Investigation Into the Relationship Between TSP Concentrations and Wind Direction in Connecticut*, internal report issued by the Connecticut Department of Environmental Protection, Hartford, Connecticut, December 24, 1976.

12. Bruckman, L. and R.A. Rubino, "**Monitored Asbestos Concentrations in Connecticut,**" paper presented at the 70th Annual Meeting of the Air Pollution Control Association, Toronto, Ontario, June 20-24, 1977.
13. Bruckman, L., "**Suspended Particulate Transport,**" paper presented at the 70th Annual Meeting of the Air Pollution Control Association, Toronto, Ontario, June 20-24, 1977.
14. Bruckman, L., "**A Study of Airborne Asbestos Fibers in Connecticut,**" paper presented at the "Workshop in Asbestos: Definitions and Measurement Methods" sponsored by the National Bureau of Standards/U.S. Department of Commerce, July 18-20, 1977.
15. Bruckman, L., "**Monitored Asbestos Concentrations Indoors,**" paper presented at The Fourth Joint Conference of Sensing Environmental Pollutants, New Orleans, Louisiana, November 6-11, 1977.
16. Bruckman, L., paper presented at the Joint Conference on Applications of Air Pollution Meteorology, Salt Lake City, Utah, November 28 - December 2, 1977.
17. Bruckman, L., E. Hyne, W. Keever, "**A Comparison of Low Volume and High Volume Particulate Sampling,**" internal report issued by the Connecticut Department of Environmental Protection, Hartford, Connecticut, 1976.
18. "**Data Validation and Monitoring Site Review,**" (part of the Air Quality Maintenance Planning Process), internal report issued by the Connecticut Department of Environmental Protection, Hartford, Connecticut, June 15, 1976.
19. "**Air Quality Data Analysis,**" (part of the Air Quality Maintenance Planning Process), internal report issued by the Connecticut Department of Environmental Protection, Hartford, Connecticut, August 16, 1976.
20. Bruckman, L., "**Investigation into the Causes of Elevated SO<sub>2</sub> Concentrations Prevalent Across Connecticut During Periods of SW Wind Flow,**" paper presented at the 71st Annual Meeting of the Air Pollution Control Association, Paper #78-16.4, Houston, Texas, June 25-29, 1978.
21. Anderson, M.K., "**Power Plant Impact on Ambient Air: Coal vs. Oil Combustion,**" paper presented at the 68th Annual Meeting of the Air Pollution Control Association, Paper #75-33.5, Boston, MA, June 15-20, 1975.
22. Anderson, M.K., G. D. Wight, "**New Source Review: An Ambient Assessment Technique,**" paper presented at the 71st Annual Meeting of the Air Pollution Control Association, Paper #78-2.4, Houston, TX, June 25-29, 1978.
23. Wolff, G.T., P.J. Liroy, G.D. Wight, R.E. Pasceri, "**Aerial Investigation of the Ozone Plume Phenomenon,**" J. Air Pollut. Control Association, 27: 460-3 (1977).
24. Wolff, G.T., P.J. Liroy, R.E. Meyers, R.T. Cederwall, G.D. Wight, R.E. Pasceri, R.S. Taylor, "**Anatomy of Two Ozone Transport Episodes in the Washington, D.C., to Boston, Mass., Corridor,**" Environ. Sci. Technol., 11-506-10 (1977).
25. Wolff, G.T., P.J. Liroy, G.D. Wight, R.E. Meyers, and R.T. Cederwall, "**Transport of Ozone Associated With an Air Mass,**" In: Proceed. 70 Annual Meeting APCA, Paper 377-20.3, Toronto, Canada, June, 1977.

26. Wight, G.D., G.T. Wolff, P.J. Lioy, R.E. Meyers, and R.T.Cederwall, "**Formation and Transport of Ozone in the Northeast Quadrant of the U.S.,**" In: Proceed. ASTM Sym. Air Quality and Atmos. Ozone, Boulder, Colo., Aug. 1977.
27. Wolff, G.T., P.J. Lioy, and G.D. Wight, "**An Overview of the Current Ozone Problem in the Northeastern and Midwestern U.S.,**" In: Proceed. Mid-Atlantic States APCA Conf. on Hydrocarbon Control Feasibility, p. 98, New York, N.Y., April, 1977.
28. Wolff, G.T., P.J. Lioy, G.D. Wight, R.E. Meyers, and R.T.Cederwall, "**An Investigation of Long-Range Transport of Ozone Across the Midwestern and Eastern U.S.,**" Atmos. Environ. 11:797 (1977).
29. Bruckman, L., R.A. Rubino, and J. Gove, "**Connecticut's Approach to Controlling Toxic Air Pollutants,**" paper presented at the STAPPA / ALAPCO Air Toxics Conference, Air Toxics Control: An Environmental Challenge, Washington, D. C., October 15-17, 1986.
30. Wackter, D.J., and P.V. Bayly, "**The Effectiveness of Emission Controls on Reducing Ozone Levels in Connecticut from 1976 through 1987,**" paper presented at the APCA Specialty Conference on: The Scientific and Technical Issues Facing Post-1987 Ozone Control Strategies, Hartford, Connecticut, November 17-19, 1987.
31. Wackter, D.J., "**Sensitivity Analysis of Ozone Predictions by the Urban Airshed Model in the Northeast,**" paper presented at the Air Pollution Control Association Conference on VOC and Ozone, Northampton, MA, November 1-2, 1988.

### XIII. ERRATA

During the preparation of this Air Quality Summary, a number of errors were discovered in previous editions of this document. For the benefit of the reader, the corrections are presented below:

- Regarding the 1989 Air Quality Summary,
  1. In Section II, on page 11, the third sentence in the first paragraph under **Annual Averages** should end with the year 1989 (not 1988).
  2. In Section II, on page 12, the second sentence in the second paragraph under **Statistical Projections** should read: "...more frequent PM<sub>10</sub> sampling in 1987, 1988 and 1989..."
  3. In Section II, on page 32, Table 2-4 should show that the annual average for ammonium is 330 ng/m<sup>3</sup> (not 3260 ng/m<sup>3</sup>).
  4. In Section III, on page 57, in Table 3-1, the site name for Hartford 018 should be changed from "State Office Building" to "Sheldon Street."
  5. In Section IV, due to last-minute changes, the deletion or renumbering of some figures was not reflected in the text:
    - a. On page 76, under **Monitoring Network**, the reference to Figure 4-5 should be changed to Figure 4-3.
    - b. On page 76, under **1-Hour Average**, the reference in the second paragraph to Figure 4-6 should be changed to Figure 4-4.
    - c. On pages 76 and 77, under **Trends**, the two references in the second paragraph and the single reference in the third paragraph to Figure 4-7 should be changed to Figure 4-5. In addition, the reference in the third paragraph to Figure 4-8 should be changed to Figure 4-6.
  6. In Section VII, on page 108, miscalculated emissions from solid waste incineration led to erroneous conclusions regarding the trend of airborne lead concentrations. Consequently, the two paragraphs under **Trends** should be deleted and replaced by the following:

*The downward trend in airborne lead concentrations can be expected to level off at some point in the near future, when the use of leaded gasoline is finally phased out or minimized. Lead emissions will then rise and fall with the number of vehicle miles traveled by the population. This is due to the fact that so-called unleaded gasoline still contains a small proportion of lead.*
  7. In Section XI, on page 128, the parenthetical sentence at the end of the first paragraph under **Quality Assurance** should reference Part D (not Part E).
- Regarding the 1988 Air Quality Summary,
  1. In Section VII, on page 88, for reasons explained in item 5 above, the last two paragraphs under **Trends** should be deleted and replaced by the paragraph in item 5.

2. In Section XI, on page 108, the parenthetical phrase at the end of the first paragraph under Quality Assurance should reference Part D.(not Part E).